

APPENDIX B

A Finite Element Solution Technique
for a Diagnostic Circulation Model

by

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A FINITE ELEMENT SOLUTION TECHNIQUE
FOR A DIAGNOSTIC SHELF CIRCULATION MODEL

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ABSTRACT. A linear diagnostic shelf circulation model developed by Galt (1975) is implemented using the Finite Element Method. The model solves a second-order non-homogeneous elliptic vorticity equation for the surface elevation within the region of interest. Solutions are obtained using finite element techniques, with elemental areas determined by available **STD** station spacing. After obtaining the surface elevations, velocities are calculated.

The model was initially tested on several simple contrived cases to help demonstrate the physics and the numerical techniques involved. Results from these tests indicate that, physically, the model generates a **barotropic** flow within the region of interest such that water and vorticity are conserved through the bottom Ekman layer. Numerically, the model approximates the analytical solution by **piecewise** linear functions. Therefore, if the **analytical** solution is not linear numerical errors occur which depend upon the mesh size.

The computer model has been written up in Standard Fortran and requires a set of STD station data and wind-stress data. The model is configured so that it can be economically run on intermediate size computers (100-150K core).

1. INTRODUCTION

The purpose of this study is to develop an economic and easily used flow model for continental shelf areas to help study the distribution of offshore pollutants. This report documents the program and demonstrates its use for simple test cases. A **geostrophic** model appropriately formulated for time scales of a few days is attempted. Most **geostrophic** flow models in the past have been developed for flow in deep water where a **level** of no motion is **specified**. At this reference **level** the net horizontal pressure gradient is assumed

to be zero (Sverdrup et al., 1942; **Formin, 1964**). From this hypothesized level, the relative **isopycnal** slopes can be calculated **from STD** observations. Over shelf areas, however, a level of no motion is improbable, and a different kind of model is needed.

The model developed here for shelf areas is a linear steady-state model requiring a set of STD and wind-stress data. The model incorporates **baroclinic** contributions, a variable depth, a wind-driven surface Ekman layer, and a **geostrophically** driven bottom Ekman layer into a **vertically integrated vorticity equation**. **Continuity is invoked**; the **coriolis** parameter is taken to be a constant, and **the** final result is a nonhomogeneous elliptic equation for the surface elevation. (A similar formulation for the homogeneous case is presented by Welander, 1957.) This equation is solved using a finite element technique with a triangular mesh system which **can** be adjusted to a region of arbitrarily located stations. Once the surface elevations are obtained, estimates of surface and bottom velocities are computed.

The actual computer model calls a set of subroutines which can easily be bypassed, altered, or used elsewhere. For example, the model has a **subroutine to convert geographic coordinates into a nondimensional x, y Cartesian grid, and another** to normalize the raw station data in terms of arbitrary dimensions read in by the user.

This report will concentrate on the finite element **technique** used, the development of the mathematics and physics of the model has been published by **Galt** (1975). A companion report will discuss the details of the boundary conditions formulation and suggest strategies for model use.

2. THE FINITE ELEMENT TECHNIQUE

We now turn our attention to solving the elliptic model equation for the surface elevation. This equation is solved numerically using a finite element technique. The finite element approach copes with randomly spaced discrete data within a region, and the finite element grid fits **odd-shaped** regions well.

The finite element approach approximates the solution as a linear combination of "shape functions". These functions are inserted into the differential equation and **the residual, or error, is** minimized. For example, the equation to be solved is

$$N_2 \nabla^2 \xi - J(\xi, d) - N_1 J(\alpha, d) + N_1 N_2 \nabla^2 \alpha - \nabla x \vec{\tau} = 0 . \quad (1)$$

This can be written in the following operator form

$$L(E) = F , \quad (2)$$

where

$$L(\xi) = N_2 \nabla^2 \xi - J(\xi, d) , \quad (3)$$

$$F = N_1 J(\alpha, d) - N_1 N_2 \nabla^2 \alpha + \nabla x \vec{\tau} . \quad (4)$$

The solution, ξ , can be approximated in the following way:

$$\xi = \sum_{i=1}^{NVRTX} \psi_i C_i , \quad (5)$$

where

NVRTX = number of points at which the equation will be solved
(No. of stations);

$\psi_i = \psi_i(x, Y)$, "shape function";

c_i = value of solution at specified locations,

The shape functions used here will be **piecewise** continuous and take on the value of one at node "i", and zero at neighboring nodes. The exact nature of the shape functions and the strategy behind them is **explained** in the following section. At this point, the ψ 's are a linearly independent bases set of functions used to approximate the solution.

The next step is to substitute the approximate solution into equation (2) to give

$$L \left(\sum_{i=1}^{NVRTX} \psi_i c_i \right) - F = E, \quad (6)$$

where

E = error introduced due to approximation.

The error is minimized by the **Galerkin** technique (Zienkiewicz, 1971).

The method requires that the error be orthogonal to the space spanned by the bases set of functions. This is expressed by the following equation:

$$\iint_D E \cdot \psi_j dx dy = 0 \text{ for } j = 1, 2, \dots, NVRTX, \quad (7)$$

where

D = domain of interest.

Writing this as a system of NVRTX equations and substituting the expression for E from (6) into the above gives

$$\sum_{j=1}^{NVRTX} \iint_D \left(L \left(\sum_{i=1}^{NVRTX} \psi_i C_i \right) - F \right) \psi_j dx dy = 0 . \quad (8)$$

Since the operator, L, is linear, and the C_i 's are constants, this can be written as

$$\sum_{j=1}^{NVRTX} \sum_{i=1}^{NVRTX} C_i \iint_D L(\psi_i) \psi_j dx dy = \sum_{j=1}^{NVRTX} \iint_D F \psi_j dx dy . \quad (9)$$

This can be written in matrix form as

$$AC = R , \quad (10)$$

where

$$A_{ij} = \iint_D \psi_j L(\psi_i) dx dy , \quad (11)$$

$$R_j = \iint_D F \psi_j dx dy . \quad (12)$$

Substituting the operator from (3) into (11) gives

$$A_{ij} = \iint_D \left[N_2 \psi_j \left(\frac{\partial^2 \psi_i}{\partial x^2} + \frac{\partial^2 \psi_i}{\partial y^2} \right) - \psi_j \left(\frac{\partial \psi_i}{\partial y} \frac{\partial d}{\partial x} - \frac{\partial \psi_i}{\partial x} \frac{\partial d}{\partial y} \right) \right] dx dy . \quad (13)$$

The shape functions, ψ , will be made up of linear functions of x and y , and are piecewise continuous across element boundaries. Thus the second derivative terms are not well-defined along the boundaries and the integration shown in equation (13) cannot be completed. To avoid this problem, the second derivative terms are integrated by parts (for details, see Appendix V), giving

$$A_{ij} = -N \iint_D \left(\frac{\partial \psi_i}{\partial x} \frac{\partial \psi_j}{\partial x} + \frac{\partial \psi_i}{\partial y} \frac{\partial \psi_j}{\partial y} \right) dx dy \quad (14)$$

$$- \iint_D \psi_j \left(\frac{\partial \psi_i}{\partial y} \frac{\partial d}{\partial x} - \frac{\partial \psi_i}{\partial x} \frac{\partial d}{\partial y} \right) dx dy + \int_s \psi_j \left(\frac{\partial \psi_i}{\partial x} \ell_y + \frac{\partial \psi_i}{\partial y} \ell_x \right) ds ,$$

where

s = boundary of the domain,

ℓ_x, ℓ_y = directional cosines along the boundary.

Similarly, R_j may be obtained by substituting from (4) into (12):

$$R_j = \iint_D N_1 \psi_j \left(\frac{\partial \alpha}{\partial y} \frac{\partial d}{\partial x} - \frac{\partial \alpha}{\partial x} \frac{\partial d}{\partial y} \right) - N_1 N_2 \psi_j \left(\frac{\partial^2 \alpha}{\partial x^2} + \frac{\partial^2 \alpha}{\partial y^2} \right) \quad (15)$$

$$+ \psi_j \left(\frac{\partial \tau_y}{\partial x} - \frac{\partial \tau_x}{\partial y} \right) dx dy .$$

Once again integrating the second derivative term by parts gives

$$R_j = N \iint_D \psi_i \left(\frac{\partial \alpha}{\partial y} \frac{\partial d}{\partial x} - \frac{\partial \alpha}{\partial x} \frac{\partial d}{\partial y} \right) dx dy + N_1 N_2 \iint_D \left(\frac{\partial \psi_j}{\partial x} \frac{\partial \alpha}{\partial x} + \frac{\partial \psi_j}{\partial y} \frac{\partial \alpha}{\partial y} \right) dx dy \quad (16)$$

$$+ \iint_D \psi_j \left(\frac{\partial \tau_y}{\partial x} - \frac{\partial \tau_x}{\partial y} \right) dx dy - N_1 N_2 \int_s \psi_j \left(\frac{\partial \alpha}{\partial x} \ell_y + \frac{\partial \alpha}{\partial y} \ell_x \right) ds .$$

Equations (14) and (16) now define the **matrix** equations which must be solved.

Now consider the geometrical problem of calculating A_{ij} and R_j . First the domain is divided into triangular vertices. The five-station case is an example in figure 1. At each station, the position, depth, a , A , and wind stress components are given as

$s(N)$, $Y(N)$, $depth(N)$, $alpha(N)$, $delta(N)$, $taux(N)$, **tauy(N)**, where N refers to the **global** label of the station,

Within each triangle, the **bases** functions and independent variables are all assumed to be **linear** functions of x and y . This means that within each triangle the independent variables are represented as

$$\begin{aligned} depth_{TN} &= D_x \cdot x + D_y \cdot y + D_0, \\ alpha_{TN} &= \alpha_x \cdot x + \alpha_y \cdot y + 0, \\ \tau_{x,TN} &= \tau_x \cdot x + \tau_x \cdot y + \tau_{x0}, \\ \tau_{y,TN} &= \tau_y \cdot x + \tau_y \cdot y + \tau_{y0}. \end{aligned}$$

The coefficients are determined by matching values at the vertices.

For example, to **solve** for D_x , D_y , and D_0 in **triangle T1**, we solve the following set of equations:

$$\begin{aligned} depth(I) &= D_x \cdot x(I) + D_y \cdot y(I) + D_0, \\ depth(III) &= D_x \cdot x(III) + D_y \cdot y(III) + D_0, \\ depth(V) &= D_x \cdot x(V) + D_y \cdot y(V) + D_0. \end{aligned}$$

Each triangle contributes to the value of the **shape function at** each of its vertices. For example, triangle **T1** contributes to the value of the shape function of points I, 111, and V. The contributing elements to the shape functions are defined as follows:

$$\begin{aligned}\psi_I^{TN} &= \psi_x(1) \cdot x + \psi_y(1) \cdot y + \psi_0(1) , \\ \psi_J^{TN} &= \psi_x(2) \cdot x + \psi_y(2) \cdot y + \psi_0(2) , \\ \psi_K^{TN} &= \psi_x(3) \cdot x + \psi_y(3) \cdot y + \psi_0(3) ?\end{aligned}\tag{17}$$

where

TN = triangle number,

I, J, K = vertex number.

The coefficients, ψ_x , ψ_y , and ψ_0 are determined in such a way that $\psi_I^{TN} = 1$ at I and zero at vertices J and K. As an example, in triangle T1, to obtain $\psi_x(1)$, $\psi_y(1)$, and $\psi_0(1)$, the following set of equations is solved:

$$\begin{aligned}1 &= \psi_x(1) \cdot x(1) + \psi_y(1) \cdot y(1) + \psi_0(1), \\ 0 &= \psi_x(1) \cdot x(2) + \psi_y(1) \cdot y(2) + \psi_0(1), \\ 0 &= \psi_x(1) \cdot x(3) + \psi_y(1) \cdot y(3) + \psi_0(1).\end{aligned}\tag{18}$$

Within each triangle the shape functions and independent variables are planar segments. Over the entire region, the shape functions and independent variables are piecewise continuous.

The next step is to assemble the **matrix** and right-hand side of equation (10) one triangle at a time. Since the independent variables and shape function are linear, all the first derivatives are constants. Therefore, A_{ij} can be rewritten as

$$A_{ij} = - N_2 \iint_{DTN} (\psi_x(K_i) \cdot \psi_x(K_j) + \psi_y(K_i) \cdot \psi_y(K_j)) dx dy \quad (19)$$

$$- \iint_{DTN} (\psi_i(\psi_y(K_i) \cdot D_x - \psi_x(K_i) \cdot D_y) + \oint \psi_j(\frac{\partial \xi_j}{\partial x} \ell_y + \frac{\partial \xi_j}{\partial y} \ell_x)) ds ,$$

where

DTN = Domain of triangle TN ,

K_i, K_j = refers to the global coefficient associated with points i and j .

R_j becomes

$$N_1 \iint_j (\alpha_y D_x - \alpha_x \cdot D_y) dx dy + N_1 N_2 \iint_{DTN} ((\psi_x)_i \alpha_x + (\psi_y)_j \alpha_y) dx dy$$

$$+ \iint_{DTN} (\psi_j (\tau_y)_x - (\tau_x)_y) dx dy - N_1 N_2 \oint \psi_j (\alpha_x \cdot \ell_y + \alpha_y \ell_x) ds. \quad (20)$$

Notice that the line integrals contribute **only** to the points which lie on the boundary of the entire domain. **In the five-point example,** the line integrals are zero unless both i and j do not **equal** V .

To evaluate A_{ij} and R_j , three types of integrals have to be evaluated for each triangle:

$$\begin{aligned}
& \text{(a) } \int_{DN} dx dy , \\
& \text{(b) } \int_{DTN} \psi dx dy , \\
& \text{(c) } \int_S \psi ds .
\end{aligned}$$

The first is simply the area of the triangle. The second is one-third the area of the triangle (see Appendix VI), and the third equals the length of the triangle sides adjacent to the boundary point divided by two. A_{ij} and R_j can now be rewritten as:

$$\begin{aligned}
A_{ij} = & -N_2(\psi_x(K_i) - \psi_x(K_j) + \psi_y(K_i) \cdot \psi_y(K_j)) \cdot \text{Area} \\
& - (\psi_y(K_i) \cdot D_x - \psi_x(K_i) \cdot D_y) \cdot 1/3 \text{ Area} \\
& + (\psi_x(K_i) - \alpha_y + \psi_y(K_i) \cdot \alpha_x) \cdot \int \psi_j ds ,
\end{aligned} \tag{21}$$

$$\begin{aligned}
R_j = & N_1(\alpha_y \cdot D_x - \alpha_x \cdot D_y) \cdot 1/3 \text{ Area} + N_1 N_2(\psi_x(K_j) \cdot \alpha_x \\
& + N_1 N_2(\alpha_x \cdot \alpha_y + \alpha_y \cdot \alpha_x) \int \psi_j ds .
\end{aligned} \tag{22}$$

The matrix and right-hand side are now ready to be assembled by adding the contributions from each triangle. In our test case, we begin with triangle T1. All the gradients are calculated along with the area of the triangle. Then the contributions to R_j and A_{ij} are calculated and placed in their appropriate locations. For T1, $i = 1, III, V$, and $j = I, III, V$; the contributions to A_{ij} would be at $A_{11}, A_{13}, A_{15}, A_{31}, A_{33}, A_{35}, A_{51}, A_{53}$, and A_{55} , while the contributions

to R_j would be to $R_1, R_3,$ and R_5 . The line integral terms contribute only when i and j are boundary points. After T1 is completed, the system is repeated for T2. For the second triangle A_{15} and A_{51} already have values from the previous triangle, so we add on to the existing values.

After all the triangles are covered, the boundary conditions are considered. The solution vector components c_i are the surface elevations at the triangle vertices which are known along the boundary. To incorporate the boundary conditions where the elevation is given, the rows associated with the boundary points are set to zero except for the diagonal element which is set to 1. Then the element of the right-hand side associated with this row is set to the boundary value. Along island or coastline boundaries a no net transport condition is added on to the assembled matrix. Along these boundaries we require:

$$-d \frac{\partial \xi}{\partial s} + N_2 \left(\frac{\partial \xi}{\partial n} - \frac{\partial \xi}{\partial s} \right) = -N_1 \left(\frac{\partial \Delta}{\partial s} + \alpha \frac{\partial d}{\partial s} \right) + \tau_s - N_1 N_2 \left(\frac{\partial \alpha}{\partial n} - \frac{\partial \alpha}{\partial s} \right) \quad (23)$$

Where \bar{n} is a unit vector normal to the coast pointing offshore and \bar{s} is a unit vector given by $\bar{k} \times \bar{n} = \bar{s}$, where \bar{k} is positive up. To see how this is incorporated into the assembled matrix consider the following triangle with a coastal boundary (figure 3)

We see:

$$\bar{n} = n_x \bar{z} + n_y \bar{y} \quad (24)$$

$$= \frac{(Y_m - y_\ell)}{[(X_m - x_\ell)^2 + (Y_m - y_\ell)^2]^{1/2}} \bar{z} + \frac{-(x_m - x_\ell)}{[(x_m - x_\ell)^2 + (y_m - y_\ell)^2]^{1/2}} \bar{y}$$

$$\bar{s} = s_x \bar{z} + s_y \bar{y} \quad (25)$$

$$= \left[\frac{(x_m - x_\ell)}{(X_m - x_\ell)^2 + (Y_m - y_\ell)^2} \right] \bar{z} + \left[\frac{(Y_m - y_\ell)}{(X_m - x_\ell)^2 + (Y_m - y_\ell)^2} \right] \bar{y}$$

Within this triangle all variables are expressed in terms of the three shape functions, **i.e.**,

$$\xi = C_\ell \psi_\ell + C_m \psi_m + C_n \psi_n$$

$$d = d_\ell \psi_\ell + d_m \psi_m + d_n \psi_n$$

$$a = \alpha_\ell \psi_\ell + \alpha_m \psi_m + \alpha_n \psi_n$$

$$A = \Delta_\ell \psi_\ell + \Delta_m \psi_m + \Delta_n \psi_n$$

And the shape functions are defined by

$$\psi_\ell = (\psi_\ell)_x x + (\psi_\ell)_y y + (\psi_\ell)_o$$

$$\psi_m = (\psi_m)_x x + (\psi_m)_y y + (\psi_m)_o$$

$$\psi_n = (\psi_n)_x x + (\psi_n)_y y + (\psi_n)_o$$

With these normal and tangential derivatives can be defined by

$$\begin{aligned} \frac{\partial \xi}{\partial n} = & (C_{\ell}(\psi_{\ell})_x + C_m(\psi_m)_x + C_n(\psi_n)_x) n_x \\ & + (C_{\ell}(\psi_{\ell})_y + C_m(\psi_m)_y + C_n(\psi_n)_y) n_y \end{aligned} \quad (26)$$

Using these forms we can substitute into equation (23) to get a relationship between known triangle parameters and the nodal values of the dependent variable. The error in this equation is then required to be orthogonal to the bases set of functions integrated **along** the coastal or island boundary. These constraints are added on to **the matrix** which has already been assembled using the differential equation.

Details are shown in the program listing given in Appendix II.

3. THE PROGRAM

The FORTRAN program making up the model satisfies several specifications. First and foremost, the program can be easily utilized by anyone who has a set of standard STD station data and an available computer. Second, the program has several options as to what is read, computed, and printed. Third, parts of the program are easily changeable, bypassed, or omitted without affecting other parts of the program. The program is basically written as a collection of overlays and subroutines. In the main program, the user specifies what type of data is to be read, what is to be computed, and what is to be printed. The main program subsequently activates the appropriate set of overlays and subroutines.

Before dealing with the program in detail, it would be **helpful** to briefly **summarize** the program. It begins by reading in several control parameters which dictate what is to be computed, listed, punched, and plotted. The program has the option to list whatever is read and computed, and to punch whatever is computed. This allows data to be easily echo-checked, and computed values **need not be recomputed** for future runs using the same source deck. The first set of control parameters deals with normalizing the station data. **If** raw station data is read in with corresponding geographic coordinates, the program will transform the positions onto a scaled x-y Mercator grid and normalize the station data according to scale parameters which are also read in. The normalized data can be punched onto cards for later **runs**. The next set of options concerns the triangular mesh used for interpolation and as the finite element mesh. The user has the option of either reading in the triangular mesh or using a set of subroutines in the program to create the triangles. Then the boundary values are read in. If the triangles are internally generated, the triangles external to the region are eliminated. The program proceeds to generate and solve the finite element matrix and right-hand side **vector** subject to the boundary conditions. The solution yields the surface elevation at each station, and with this information, the transport, mean velocity, surface slope velocity, wind-driven surface velocity, **and the geostrophic** velocity at the bottom for each triangle are calculated. Finally, **there** is a set of plotting option which will draw and contour the **results**.

Appendix I is a flow chart of the main program and overlay structure with explanations of the key routines. A listing of the complete program is given in Appendix II.

3. Documentation

3.1 Section I

The program begins by reading the control parameters. These parameters determine what the program will do and how it will function. There are three types of control parameters. The first allows the user to bypass an option. For **example**, if **NOGRID** is **set to 0**, the program will not generate a Mercator grid; instead, it will read the grid. The second type of control parameter allows one to list whatever is read or calculated. These parameters all begin with the letter L. For example, if **LTRI** is set to 1, the program will **list** the triangle vertices. The third type of control parameter begins with the letters 1P and determines if the program will punch the results on cards. For example, if **IPNORM** is set to 1, the program will punch the normalized station data. A detailed explanation of each option is given in the program itself (see Appendix II). If any control parameter is set to 1, the option **will** be executed and, if it is 0, the option **will** be bypassed. In addition to the list, punch, and bypass options, there are parameters which allow the user to alter the boundary conditions during the given run, store the decomposed matrix on a file for later *use*, and smooth the alpha and delta field to a least squares fit over the data.

3.2 Section 11

This section deals with the input of station data. There are several options available. The first is to set **NORMAL** and **NOGRID** to 1 and **read** the raw station data. The program **will** then generate a Mercator grid and normalize the station data. Another choice is to read in normalized station data with geographic **coordinates**, or raw station data with Mercator coordinates. In the last two cases, either **NOGRID** or **NORMAL** is set to 0. The last option is to read normalized station data with Cartesian coordinates for the **station locations**. In this case, both **NOGRID** and **NORMAL** are set to 0. If more than one run is made on the same set of data, the last option should be exercised after generating a data deck of the normalized data and Mercator grid from the initial run.

Raw station data is read using format 10. An example is given **in** Appendix 121.

3.4 Section 111

The scale parameters which control the scaling and nondimensional **izing** are read in here, they are as follows:

USCALE: Velocity scale in meters per second;

DSCALE : Depth scale in meters;

ALSCALE: Horizontal length scale in meters;

G : Gravity in meters per second squared;

E : Perturbation density in grams per centimeter cubed;

Q : Constant density in grams per centimeter cubed;

GAMMA : Bottom friction coefficient in grams per **centimeter** squared.

3.5 Section IV

In this section, geographic coordinates are transformed into Mercator x-y grid. Notice that the routine works **only** for the northern hemisphere and west longitude. The subroutine finds the maximum and minimum **values** of latitude and longitude. The minimum latitude becomes the y = 0 axis. The y coordinate **value of each station is obtained by calculating its distance from the y = 0 axis and scaling the distance by the horizontal length scale.** For example, if a station is 100 km north of the y = 0 line and the length scale is 100 km, the y coordinate value of the station is one unit. The x coordinate is computed in a slightly different manner because the distance between a station and the x = 0 line is a function of its longitude and latitude. The program finds the mean latitude and calculates the distance in the x direction that the station is from the x = 0 longitude and the longitude of the station at the mean latitude.

The Mercator grid can be scaled so the output **overlays** standard hydrographic charts. The transformations are as follows:

$$X(I) = -(R * \lambda - \lambda_{min})$$

$$Y(I) = R * ALOG(TAN(\theta/2. + \pi/4) - TAN(\frac{\theta_{min}}{2} + \pi/4))$$

where:

R = Radius of Earth + (ALSCALE * COS (θ average)) this makes each nondimensional unit in the horizontal direction one scale (ALSCALE) **length** at the mean latitude.

λ = Longitude

λ_{\min} = Western most longitude to become $x = 0$ line

θ = Latitude

θ_{\min} = minimum latitude to become $y = 0$ line

The radius, R, is listed by the routine and if a plot is to be made to fit another Mercator projection, the x and y axis can be scaled appropriately. For example on a typical Mercator chart there will be a statement **that** the scale of the projection is **1:N** on reference latitude θ ref. Then if R is entered as:

$$R = \frac{\text{Radius of the earth (meters)}}{\cos(\theta_{\text{REF}})}$$

The plots will be correctly scaled to overlay the chart.

The data for this routine is read with the raw station data. The degrees of latitude and longitude are read into two integer arrays and the minutes of latitude and longitude into two decimal places are read into two **real** arrays. The x and y coordinates returned from this subroutine are stored into the real arrays, and the original **latitude** and longitude of the stations are lost.

3.6 Section V

This routine calculates the mean **coriolis value**, F0, by averaging the maximum and minimum **coriolis** values of the region.

3.7 Section VI

The raw station data is normalized according to the scale parameters read in by Section III. In the following, the primed values are the

normalized, nondimensional values:

$$\begin{aligned} \text{ALPHA}' &= (\text{ALPHA} - Q * \text{DEPTH}) / (E * \text{DSCALE}); \\ \text{DELTA}' &= (\text{DELTA} - Q * \text{DEPTH} * \text{DEPTH} / 2) / (E * \text{DSCALE} * \text{DSCALE}); \\ \text{DEPTH}' &= \text{DEPTH} / \text{DSCALE} \\ \text{TAUX}' &= (1 / (\text{FO} * \text{USCALE} * Q * \text{DSCALE})) * \text{TAUX}; \\ \text{TAUY}' &= (1 / (\text{FO} * \text{USCALE} * Q * \text{DSCALE})) * \text{TAUY}; \\ \text{CURL}' &= (1 / (\text{FO} * \text{USCALE} * Q * \text{DSCALE} * \text{ALSCALE})) * \text{CURL}, \end{aligned}$$

The normalized values are stored in the arrays where the raw data was stored.

3.8 Section VII

In this section, a least squares fit is made over the alpha and delta fields. A third-order polynomial in the z direction is fit to both the alpha and delta data.

$$\begin{aligned} \text{ALPHA} &= A_0 + A_1 * Z + A_2 * Z * Z + A_3 * Z * Z * Z \\ \text{DELTA} &= D_0 + D_1 * Z + D_2 * Z * Z + D_3 * Z * Z * Z \end{aligned}$$

The coefficients are returned by the subroutine to be used later to calculate the alpha and delta gradients. The subroutine is a general least squares fit program, and the basis set of functions used for the least squares interpolation can be changed. The user also has the option of smoothing the alpha and delta fields. For example, if the parameter "SMOOTH" is set to 1.5, the program will smooth data over 1.5 standard deviations away from the least squares fit back to 1.5 standard deviations.

3.9 Section VIII

In this section, the nondimensionalized run parameters are either read in or calculated:

$$\text{CONST1} = (G * E * H)/(Q * FO * USCALE * ALSCALE);$$

$$\text{CONST2} = \text{GAMMA}/(Q * DSCALE).$$

3.10 Section IX

Here the program either reads in the triangles or generates them. The triangle information is stored in an array, $1P(I, N)$, where N is the number of the triangle and I is the local vertex number (1, 2, or 3). The value of 1P is the global number of the particular point. See figure 4 for an example.

If the triangles are to be read in, integer format 5 is used (see Appendix III for an example). A brief explanation of how the triangles are generated is given in Appendix IV.

3.11 Section X

The boundary values are read in this section. If the triangles are generated internally, the external boundary values must be read in counter-clockwise order. This will allow the program to determine what triangles are inside or outside of the domain. The boundary values needed are the surface elevations of the boundary stations in centimeters. Coastal and island boundary points must be identified. A discussion of the strategy used to obtain boundary values is given in the comparison report in this series. See Appendix 111 for an example of how the boundary values should be read.

3.12 Section XI

This section is used only if the **triangles** are generated internally. The subroutine **FINDBP** stores the number of boundary points that each triangle has, rearranges the local vertex numbers of the boundary **triangles** so the boundary points are the lead vertices in counterclockwise order, and finally checks to see that the boundary points are ordered consistently. This section sets up the boundary triangles for the next routine which eliminates the triangles external to the region (see figure 5).

3.13 Section XII

Again, this option is needed only if the triangles are generated internally. Subroutine **ELIM** is used to eliminate the triangles external to the region. This will be the case for concave domains (see figure 6) and islands. Each triangle with three boundary points is tested to see if it is external or internal to the region (see figure 6).

The final mesh of the triangles to be used for the finite element technique and the number of triangles, **NTRI**, are products of this section.

3.14 Section XIII

Subroutine **SETMAT** zeros the global matrix and right-hand side. The subroutine also has the option of eliminating the **triangles** with three boundary points from the finite element mesh. If the second option is activated, the **last** parameter in the call, **IELI**, is set to **1**.

3.15 Section XIV

The assembly of the **global** matrix starts here. **K** is the number of the triangle being operated on.

3.16 Section XV

The triangle vertices are **identified** in terms of their global labels. The first vertex of triangle K has **global label J**, the second, **L**, and the third, **M**.

3.17 Section XVI

The three-by-three location matrix is set and used to **calculate the area of the triangle and all the gradients within the triangle**. For example, the first row of the matrix contains the x and y coordinates of the first local vertex of triangle K.

3.18 Section XVII

Now the area of the triangle is calculated. Subroutine **TRIAREA** calculates the determinant **of** the location matrix **A**, and multiplies it by a half. The absolute value of this quantity becomes the area of the triangle.

3.19 Section XVIII

The gradients needed for the triangle are calculated with the exception of the alpha gradients. The alpha gradients are calculated in the next section. The other forcing function gradients are obtained here using the position matrix as a coefficient matrix and setting the **right-hand side vector**, **B(1)**, **B(2)**, **B(3)**, equal to the particular values of the forcing function at vertices 1, 2, **and** 3. For example, for the depth we have:

$$\begin{bmatrix} A \end{bmatrix} \begin{bmatrix} \frac{d}{x} \\ \frac{d}{y} \\ d_0 \end{bmatrix} = \begin{bmatrix} B(1) \\ B(2) \\ B(3) \end{bmatrix} = \begin{bmatrix} \text{Depth at vertex 1} \\ \text{Depth at vertex 2} \\ \text{Depth at vertex 3} \end{bmatrix}$$

The three-by-three system is solved by Kramer's Rule in subroutine SOLVE which calls TRIAREA to compute the determinants.

The shape function gradients are also calculated in the same manner by solving the following set of equations:

$$\begin{bmatrix} \cdot \\ \cdot \\ \cdot \end{bmatrix} \begin{bmatrix} \frac{d \text{ shape } (I)}{dx} \\ \frac{d \text{ shape } (I)}{dy} \\ c \text{ shape } (I) \end{bmatrix} = \begin{bmatrix} B(1) \\ B(2) \\ B(3) \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ I=1 \end{bmatrix} \quad \text{or} \quad \begin{bmatrix} 0 \\ 1 \\ 0 \\ I=2 \end{bmatrix} \quad \text{or} \quad \begin{bmatrix} 0 \\ 0 \\ 1 \\ I=3 \end{bmatrix}$$

The subscript **I** tells you which vertex the particular gradient is associated with.

3.20 Section XIX

The alpha gradients are calculated differently than the other gradients. A simple linearization of the **alpha field** introduces errors which are unacceptably large, so a more detailed description of the density **field** is needed than the bottom alpha values at the triangle vertices. Therefore, a third-order least squares fit to the alpha field is generated (see Section VII) and used to obtain alpha values at the triangle vertices for the centroid depth.

$$\begin{aligned}
 \text{Alpha (at centroid depth)} &= \text{alpha (at bottom)} + \frac{\partial(\text{alpha})}{\partial z} \delta z \\
 &+ \frac{\partial^2(\text{alpha})}{\partial z^2} \frac{\delta z^2}{2} + \frac{\partial^3(\text{alpha})}{\partial z^3} \frac{\delta z^3}{6}
 \end{aligned}$$

In the above calculations, the **alpha** gradients are obtained by differentiating the least squares function of alpha. Once the alpha values

at the **centroid** depth are obtained over each vertex, subroutine GRAD is **called** to calculate the horizontal alpha gradients. The delta gradients needed for the transports are calculated in the **same** manner,

3.21 Section XX

The triangle's contribution to the global matrix and right-hand side is added in here. Each triangle contributes to particular rows and **columns of the global** matrix determined by the **global** label of the triangle **vertices (figure 7)**.

$$\begin{array}{ccc}
 & 3 & 4 & 5 \\
 3 & \begin{bmatrix} x \\ x \\ x \end{bmatrix} & \begin{bmatrix} x \\ x \\ x \end{bmatrix} & \begin{bmatrix} x \\ x \\ x \end{bmatrix} \\
 4 & & & \\
 5 & & &
 \end{array}
 \begin{bmatrix} \\ \\ \\ \end{bmatrix}
 \begin{matrix} \\ \\ \\ \end{matrix}
 =
 \begin{bmatrix} x \\ x \\ x \end{bmatrix}
 \begin{matrix} 3 \\ 4 \\ 5 \end{matrix}$$

Then the second triangle would contribute to

$$\begin{array}{c}
 3 \quad 5 \quad 6 \\
 \mathbf{3} \quad \begin{bmatrix} + & + & + \\ + & + & + \\ + & + & + \end{bmatrix} \quad \begin{bmatrix} \\ \\ \mathbf{C} \end{bmatrix} = \begin{bmatrix} + \\ + \\ + \end{bmatrix} \quad \begin{array}{c} \mathbf{3} \\ \mathbf{5} \\ \mathbf{6} \end{array}
 \end{array}$$

Since we want the final global matrix to represent equation 36 **integrated** over the entire domain, we add **all** the contributions from each triangle. When contributions from triangles I and II in the example above are added, the resultant matrix looks like:

$$\begin{array}{c}
 1 \quad 2 \quad 3 \quad 4 \quad 5 \quad 6 \\
 \mathbf{1} \quad \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & ** & ** & * & + \\ 0 & 0 & x & x & x & 0 \\ 0 & 0 & * & x & * & + \\ 0 & 0 & + & 0 & + & + \end{bmatrix} \quad \begin{bmatrix} \\ \\ \mathbf{C} \\ \\ \\ \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ * \\ \mathbf{x} \\ * \\ + \end{bmatrix} \quad \begin{array}{c} \mathbf{1} \\ \mathbf{2} \\ \mathbf{3} \\ \mathbf{4} \\ \mathbf{5} \\ \mathbf{6} \end{array}
 \end{array}$$

As the integration is done triangle by triangle, contributions to the matrix are accumulated in the appropriate locations of the global matrix and right-hand side.

3.22 Section XXI

The boundary conditions are imposed upon the solution in this **section**.
Each row in the global matrix that is associated with a boundary point

is zeroed. Then the diagonal element of that **row** is set to 1, and the element in the right-hand side associated with that row is set equal to the boundary value. For example, suppose a four-by-four system of **equations** was assembled as shown:

$$\begin{array}{cccc|c} \mathbf{GM(1,1)} & \mathbf{GM(1,2)} & \mathbf{GM(1,3)} & \mathbf{GM(1,4)} & \mathbf{C(1)} \\ \mathbf{GM(2,1)} & \mathbf{GM(2,2)} & \mathbf{GM(2,3)} & \mathbf{GM(2,4)} & \mathbf{C(2)} \\ \mathbf{GM(3,1)} & \mathbf{GM(3,2)} & \mathbf{GM(3,3)} & \mathbf{GM(3,4)} & \mathbf{C(3)} \\ \mathbf{GM(4,1)} & \mathbf{GM(4,2)} & \mathbf{GM(4,3)} & \mathbf{GM(4,4)} & \mathbf{C(4)} \end{array} = \begin{array}{c} \mathbf{RHS(1)} \\ \mathbf{RHS(2)} \\ \mathbf{RHS(3)} \\ \mathbf{RHS(4)} \end{array}$$

Then suppose that C(1) and C(2) are known boundary values. Subroutine **BC** alters the system into the following:

$$\begin{array}{cccc|c} \mathbf{1} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{C(1)} \\ \mathbf{0} & \mathbf{1} & \mathbf{0} & \mathbf{0} & \mathbf{C(2)} \\ \mathbf{GM(3,1)} & \mathbf{GM(3,2)} & \mathbf{GM(3,3)} & \mathbf{GM(3,4)} & \mathbf{C(3)} \\ \mathbf{GM(4,1)} & \mathbf{GM(4,2)} & \mathbf{GM(4,3)} & \mathbf{GM(4,4)} & \mathbf{C(4)} \end{array} = \begin{array}{c} \mathbf{BV(1)} \\ \mathbf{BV(2)} \\ \mathbf{RHS(3)} \\ \mathbf{RHS(4)} \end{array}$$

Coastal and island boundary vertices have a no net flux boundary constraint added to the assembled matrix.

3.23 Section XXI I

The system of equations is now solved by subroutine SOLN. This matrix solving routine programmed by Steve Smyth from **Knuth (1968, 1973)** takes advantage of the sparseness of the matrix by not storing zero values, and a second to tell us where in the matrix the nonzero values occur. The program is set to solve a 200 by 200 system with each row containing no more than 20 nonzero elements and another array, INTP (4900) keeps

track of where the nonzero elements belong in the matrix. If a larger matrix is to be solved, the two arrays can be increased in a manner described within the program itself. The routine begins by reducing the global matrix into the product of an upper triangular and lower triangular system. Partial pivoting on the columns is used and the triangular matrices are stored into the original **global** matrix. The lower triangular system is solved first, then the upper triangular system is solved for vector C.

$$\begin{bmatrix} \text{GM} \end{bmatrix} \text{ becomes } \begin{bmatrix} & \text{U} \\ \text{L} & \end{bmatrix}$$

The system now can be written as

$$\begin{bmatrix} & 0 \\ \text{L} & \end{bmatrix} \begin{bmatrix} & \text{U} \\ 0 & \end{bmatrix} \underline{C} = \text{RHS} .$$

Let

$$\begin{bmatrix} & \text{U} \\ 0 & \end{bmatrix} \underline{C} = \underline{y} .$$

now solve the following system:

$$\begin{bmatrix} \uparrow \\ \text{L} \end{bmatrix} \underline{y} = \text{RHS} .$$

Once y is obtained, the following system is solved for C:

$$\begin{bmatrix} & 0 \\ \text{U} & \end{bmatrix} \underline{C} = \underline{y} .$$

The decomposed global matrix and right-hand side are saved. **If** different sets of boundary conditions are to be tested, the same decomposed global matrix is used and the right-hand side **is** adjusted accordingly.

3.24 Section XXIII

Here surface velocities and bottom **geostrophic** velocities are calculated for the centroid of the triangles.

3.25 Section XXIV

This is an option to calculate the terms of the **vorticity** equation. The values are calculated at the triangle centroids and are as follows:

$$\text{Barotropic torque} = J(\xi, d),$$

$$\text{Baroclinic torque} = N_1 J(\alpha, d),$$

$$\text{Wind stress} = \nabla \times \vec{\tau}^w,$$

$$\text{Bottom friction} = -(\text{barotropic torque} + \text{baroclinic torque} + \text{wind stress}).$$

3.26 Section XXV

The plotting is executed in this section. The plotting is **basically** handled by several subroutines which draw and label the triangles, label the vertices, and contour any parameter defined at the vertices. A separate program is used to take the punched velocity data from the model and plot velocity arrows at the **centroids** of the triangle.

3.27 Section XXVI

This is the option to alter the right-hand side of the global system of equations to take into account new boundary conditions. The user determines the input for this subroutine for each set of boundary conditions. Basically, the routine changes the specific boundary values

in the right-hand side vector. Once this is done, the program returns to **SOLN** and resolves the system of equations using the decomposed global matrix, subject to the new boundary conditions. With this **system**, numerous sets of boundary conditions can be tested at minimal cost.

4. RESULTS

Once the theory and software for the model was developed, operational testing was carried out. The model was **run on simple** contrived test cases. These runs were made to develop a better understanding of the physics involved to test the finite element method which is regularly used in engineering studies but is relatively new to oceanography. A summary of the results along with a discussion of the problems encountered will be presented here.

4.1 Test Cases

The test cases were designed to give a clear idea of **how** the model reacts to different physical conditions. Four simple cases were analyzed. **In** the first two, the finite element technique yielded exact linear solutions. In the last two cases, the analytical solutions could not be exactly represented by the first-order bases set and the accuracy of the numerical solution depended upon the resolution yielded by the mesh system.

The first test case was run on a regular six by six grid with a mesh of 50 triangles. The boundary elevations increased uniformly to the north from zero to 5 cm and the **wind** stress was zero. The depth and density were constant, and the nondimensional parameters were: **CONST1** = 1.00, and **CONST2** = .025. The vorticity equation reduces to **Laplace's**

equation subject to the linear boundary conditions. Physically, the **geostrophic** flow is forced only by the surface slope and is unidirectional and nondivergent. The **geostrophically** driven bottom Ekman layer is also nondivergent and is transporting water from north to **south**. The analytical solution to the **vorticity** equation is $\xi = ky$ where k is a constant determined by the boundary elevation slope. The numerical solution for this case is exact since the finite element solution approximate the solution with piecewise linear functions and is accurate to the first order (fig. 8).

The second test case is nearly identical to the **first**. The boundary conditions were the same and once again, there was no stratification or wind forcing. For this case, however, the depth was decreased uniformly toward the north from **1200 m** to 200 m.

In this case the vorticity equation becomes

$$N^2 \nabla^2 \xi + \frac{\partial d}{\partial y} \frac{\partial \xi}{\partial x} = 0 ,$$

and the resulting **geostrophic** flow is unchanged from the previous case. The surface slope once again drives a unidirectional, nondivergent current which has no shear except in the bottom Ekman layer. Mass and **vorticity** are conserved within the region by having the **geostrophic** flow follow **isobaths**. The solution once again is $\xi = ky$, and the numerical solution is exact (fig. 9).

In the third case, **baroclinicity** was introduced into the model by taking the density as a linear function of y . The **bottom** depth, wind stress and boundary conditions were identical to those of case 2. Alpha, the integrated density, became a second-order function of y . The **vorticity**

equation for this case reduces to:

$$N_2 \nabla^2 \xi + \frac{\partial d}{\partial y} \frac{\partial \xi}{\partial x} = N_1 N_2 \nabla^2 \alpha = \text{const.}$$

Now, the linear basis set of functions used to approximate the solution cannot fit the exact solution and numerical errors are expected. Physically, the density field, depth, and boundary conditions are only functions of y and the resulting **barotropic** and **baroclinic** flows are in the x direction and nondivergent. The **baroclinic** mode increases with depth and flows counter to the **barotropic** mode. This results in a **level** of no motion at the mean depth of 700 m. Above the level of no motion, the boundary forced **barotropic** mode dominates, and the **geostrophic flow** is to the west. This in turn drives a bottom Ekman layer to the south. Below the level of no motion, the **baroclinic** mode dominates and the **geostrophic** flow is to the east. This forces a bottom Ekman layer to the north (Fig. 10). Therefore, the bottom Ekman layer forced by the boundary conditions and **baroclinic** field is convergent. However, the total flow must be nondivergent, and the interior **barotropic** mode (specified by the dependent variable, surface height) must adjust over the prescribed bathymetry to compensate for the bottom Ekman convergence. In seeking the analytic solution, we first note the similarity between the reduced **voriticity** equation for this case and Stommel's model equation (1965).

Stommel's Equation

$$\nabla^2 \psi + \frac{D}{R} B \frac{\partial \psi}{\partial x} = \sin \frac{\pi y}{b}$$

$$\psi = 0 \text{ on Boundary}$$

Diagnostic Model, Case 3 Equation

$$\nabla^2 \xi + \frac{\partial}{\partial y} \frac{\partial \xi}{\partial x} = N_1 \nabla^2 \alpha$$
$$\xi = K_y \text{ on Boundary}$$

This is a consequence of the integrated friction term being **set proportional** to the velocity in both models and the bathymetric stretching term for this case being of the same form as **Stommel's** beta term. If the boundary conditions for our vorticity equation were homogeneous, we would then expect the solution to be of the same form as **Stommel's** solution. The total solution in this case is just a linear combination of the solutions for the homogeneous equation solved for the nonhomogeneous boundary conditions (case 2; see equation A below) and the nonhomogeneous **equation** solved for the homogeneous boundary conditions (**Stommel**) type solution; (see equation B below).

Homogeneous Equation

$$N_2 \nabla^2 \xi + \frac{\partial}{\partial y} \frac{\partial \xi}{\partial x} = 0$$

$$\xi = k_y \text{ on Boundary}$$

Nonhomogeneous Equation

$$N_2 \nabla^2 \xi + \frac{\partial}{\partial y} \frac{\partial \xi}{\partial x} = N_1 N_2 \nabla^2 \alpha$$

B

$$\xi = 0 \text{ on Boundary}$$

Note the effect of the **baroclinicity** is to add a secondary **flow** onto the results obtained from the constant density case. Physically we

can expect the solution to show southward flow into deeper water to compensate for the converging bottom Ekman layer and then flow moving back to the north along the western boundary to satisfy the boundary conditions. **The results of the total solution show wave-like oscillations which are unrealistic and not what was expected from the analytical solution. Haney (1975) describes similar oscillatory solutions when** a numerical mesh cannot resolve a boundary layer. To see if this is the case, the secondary flow is examined by subtracting the results of the homogeneous equation subject to the nonhomogeneous boundary conditions, (i. e., case 2) from the total solution. Figure 11 indicates that the mesh system may have problems resolving the secondary flow. A western boundary current structure is evident but not clearly resolved. To show that this is the problem, the boundary layer size was increased by setting the nondimensional friction parameter, **CONST2**, equal to **1.25** from its original .025.

In case 3A the secondary flow in figures 12 and 13 is now well resolved. As expected, the secondary flow resembles **Stommel's** solution with a western boundary barotropic mode forcing water to the south to compensate for the convergent bottom Ekman layer and then moving back to the north **along** the Western boundary to satisfy the imposed boundary conditions. This confirms that the problem with the original solution for the third case was related to resolving the boundary layer.

The next step was to see if the triangles along the western boundary could be cut in half to increase the resolution of the secondary **flow**. The previous case (case 3) was run again on the same mesh with **CONST2** equal to .25. From the results in Figures 14 and 15, it can be seen

that the numerical grid does not clearly resolve the boundary layer.

For case 3B, the mesh system was then altered such that the triangles **along the western boundary were halved**. The results are shown in Figure 16.

The solution is improved for Case 3C. It is more symmetrical and the surface elevation gradients are not as large. In general, a decrease in mesh size leads to more resolution, but the improvement is difficult to quantify because the finite element solution depends upon the triangle shapes as was the mesh size. For example, as **the** triangles become less equilateral, the global matrix becomes less conditioned (**Strang and Fix, 1973**).

For the fourth case, the density is once again set to a constant. The wind stress is still zero and the boundary condition is once again **linear** in the y direction. These are the same conditions **as** in the first case, but now the depth is made to be a linear function of both x and y (depth = **Ax + By+ C**). See Figure 17.

The vorticity equation becomes:

$$N_2 \nabla^2 \xi + \frac{\partial d}{\partial y} \frac{\partial \xi}{\partial x} - \frac{\partial d}{\partial x} \frac{\partial \xi}{\partial y} = 0$$

The depth gradients are constants. Once again the linear basis set of functions used to approximate the solution cannot fit the exact solution and numerical errors are expected. In the interior, the flow attempts to follow **isobaths** but most deviate from the **isobaths** near the boundaries due to the boundary conditions. Along the north-south boundaries, the **barotropic** mode is not allowed to force water into or out of the region,

while the shallower water on the eastern **boundary** allows the **barotropic** mode to force less water into the region than is leaving on the western boundary. To compensate for this, a secondary flow with a boundary layer on the western side is set up. The secondary **flow** forces a convergent bottom Ekman layer to conserve water within the **region**.

In Figures 18 and 19 of the solution for case 4, clearly, the secondary flow and its boundary layer are not well-resolved. As in the previous case, the boundary layer thickness is increased by increasing the friction coefficient, **CONST2**, by an order of magnitude to .25.

In Figures 20 and 21, the solution for case 4A showing surface elevation and secondary flow, the **large** oscillations are gone and it is clear that the flow attempts to follow an isobath until it reaches the western boundary. The counterclockwise secondary flow and its western boundary layer is now well-defined. It forces a convergent bottom Ekman layer which compensates for the excess water the **barotropic** mode forces out of the region through the western boundary.

The next step is to increase the resolution along the western **boundary** by once again halving the triangle size along the western boundary.

In Figures 22 and 23 for case 4B, the difference in the solution yielded by the two different meshes is almost negligible. The current along the western boundary is better resolved, but **the** finer mesh results in only a slightly more symmetrical solution. The probable reason for this is that water is converging along the northern boundary and diverging along the southern boundary, and to improve the solution, more resolution along these boundaries is needed.

The results can be summarized by saying that the model physically compensates for continuity mismatches between the surface Ekman layer, boundary forced **barotropic** flow, and within the region which has either a convergent or divergent bottom Ekman layer. This secondary flow is similar to **Stommel**'s model (1965) with a western boundary current and is a consequence of setting the vertically integrated friction terms proportional to the velocity. **The** model's inability to resolve the secondary **flow** due to too coarse a mesh was a problem in the test cases. Halving the mesh size along the western boundary improved **the** solution, **but triangle shape as well as size affected the numerical solution.**

The last test case indicates that care should be taken in setting the boundary conditions. If unrealistic boundary conditions are imposed, the model will compensate by forming a boundary layer which may degrade the results. The boundary layer thickness depends on the potential **vorticity** gradient (i.e., bottom slope) so the problem will be different for different geophysical settings.

5. CONCLUSION

A diagnostic shelf circulation model developed by Galt (1975) is implemented using the finite element method. The model is **quasi-geostrophic** and incorporates variable depth, **baroclinicity**, a surface Ekman layer, and a bottom Ekman layer. Physically, the model assumes a steady state, a small Rossby number flow. The depth scale is taken to be much less than the horizontal length scale, and the bottom Ekman **layer** is assumed to be driven by a geostrophic flow. The **coriolis** parameter is set to a constant and vorticity balance is required between the **barotropic**

and **baroclinic stretching** terms and the bottom and surface Ekman **layers**.

The test cases indicate that the model accommodates the boundary **conditions** and forcing functions by creating a secondary **barotropic** flow within the region to conserve mass and **vorticity** through the bottom Ekman layer.

The model solves **an integrated vorticity** equation which is a **second-order**, nonhomogeneous, **elliptic** equation and is tested subject to **Dirichlet** boundary conditions. The dependent variable is the surface elevation solved for by the Finite Element Method. The program is written in Standard Fortran and is a collection of subroutines and overlays which can be easily altered, bypassed or used elsewhere. The input data requires standard STD station data, wind stress information, and the boundary surface elevations.

The major problems the model encounters are numerical. The spatial resolution of the model is limited and the exact position of current features cannot be predicted to any greater accuracy than the available input data. This means that although the model clearly recognizes the local dynamics, its resolution with respect to position, is no better than the station spacing, and this should be taken into consideration prior to taking stations. The stations must be **spaced to** create a mesh which can resolve both the secondary flow and forcing functions, particularly the density field, and depth.

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FIGURE CAPTIONS

Figure

#1 Five Station case where Roman numerals are global labels and triangles are labeled T1 to T4.

#2 Illustration of a **piecewise** continuous hat function associated with node V.

#3 Boundary triangle showing normal **and** alongshore directions.

#4 Sample triangle with labeling.

#5 Example of boundary triangles with labeling. Number of boundary points for each triangle:

$$IBTRI(1) = 2$$

$$IBTRI(2) = 1$$

$$IBTRI(3) = 2$$

Relabeled **local** vertices so that boundary points lead in a counter-clockwise order:

$$IP(1,1) = 40; \quad 1P(1,2) = 41; \quad IP(1,3) = 41$$

$$1P(2,1) = 41; \quad 1P(2,2) = 43; \quad IP(2,3) = 42$$

$$1P(3,1) = 44; \quad 1P(3,2) = 44; \quad IP(3,3) = 43$$

#6 Example of a triangle external **to** the region of interest. If the outward normal to the boundary is in the triangle, then the triangle is external to the region. In this example the outward normal **between vertices 1 and 2 fall** inside triangle 1 so triangle 1 is outside of the domain and" eliminated.

#7 Two triangle examples.

#8 Homogeneous water, flat bottom case, where **the geostrophic flow** is

- #8 nondivergent and **toward the** west and the bottom Ekman flow is (cent) nondivergent and toward the east.
- #9 Homogeneous water, sloping bottom case, where the **geostrophic flow** is nondivergent and toward the west and the bottom Ekman flow is **nondivergent and toward the south.**
- #10 **Baroclinic case with density and depth** uniformly increasing toward the south and a level of no motion at the mean depth above the level of no motion.
- #11 **Secondary** flow for case 3 where the density is a **linear function** of y . The boundary layer is not resolved, resulting in numerical oscillation. Elevations are in centimeters.
- #12 Surface elevation contours for case 3 with boundary layer thickness increased (**CONST2** = 1.25). Contours are **in** centimeters.
- #13 Secondary flow for case 3 with boundary **layer** thickness increased. Western boundary layer is now well resolved. Elevations are in centimeters. (**CONST2** = 1.25).
- #14 Surface elevations for case 3 with **CONST2** = .25. The boundary **layer** is not clearly resolved. Contours are .1 centimeter.
- #15 Secondary **flow** for case 3 where **CONST2** = .25. The boundary **layer** is not clearly resolved. Contours are .1 centimeter.
- #16 Secondary flow for case **3, where** the triangles **along** the western boundary are halved from previous case. The North-South symmetry of boundary layer is not yet fully resolved. Elevations are in centimeters. (**CONST2** = .25)

- #17 Non-dimensional **isobaths** for case 4 **where** each unit is equivalent to **200 m..** Depth = **Ax + By + C.**
- #18 Surface elevations for case 4 where contours are in centimeters. The oscillations indicate that the boundary **layer** is not resolved.
- #19 Secondary **flow** for case 4 where contours are in centimeters and the boundary layer is not **well** resolved.
- #20 Surface elevations for case 4 where contours are in centimeters.
CONST2 = .25,
- #21** Secondary flow for case 4 with **CONST2 = .25.** Elevations are in **centimeters.**
- #22 **Surface elevations for case 4** with **CONST2 = .25** and the **triangles** along the western boundary are halved.
- #23 Secondary flow for case 4 with **CONST2 = .25** and the **triangles** along the western boundary have been halved from the previous case **(figure 14).** Elevations are in centimeters.

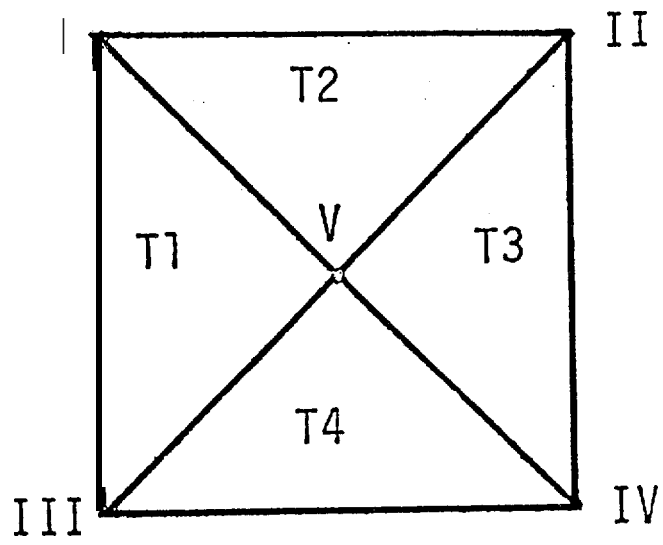


Figure 1.

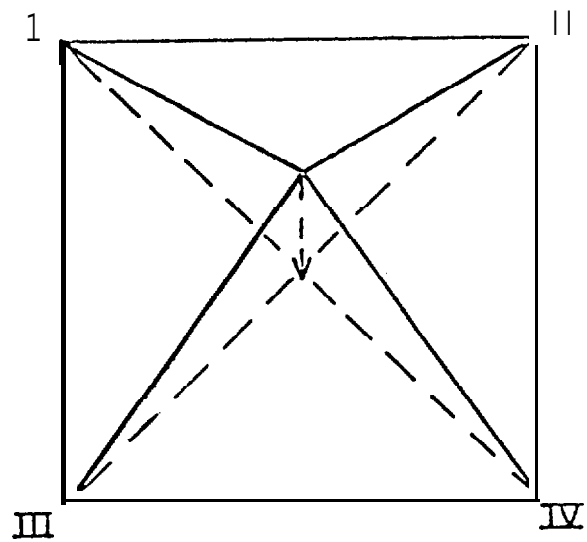


Figure 2.

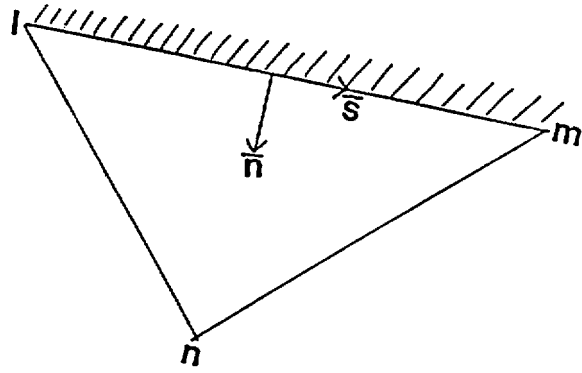


Figure 3.

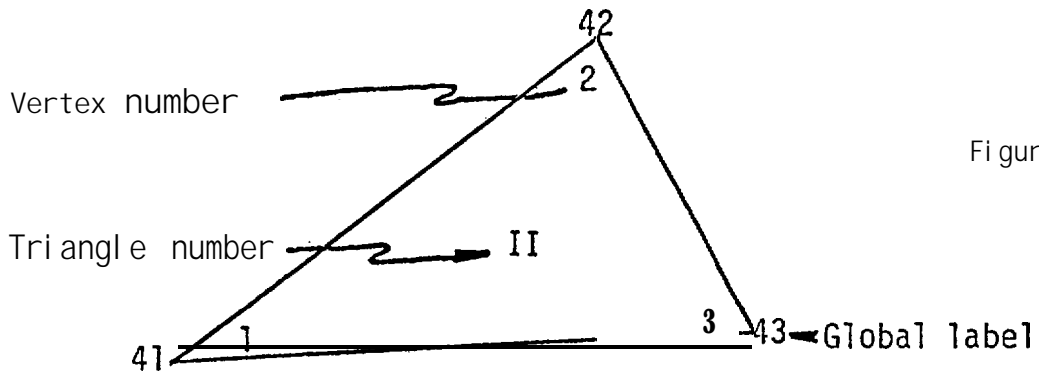


Figure 4.

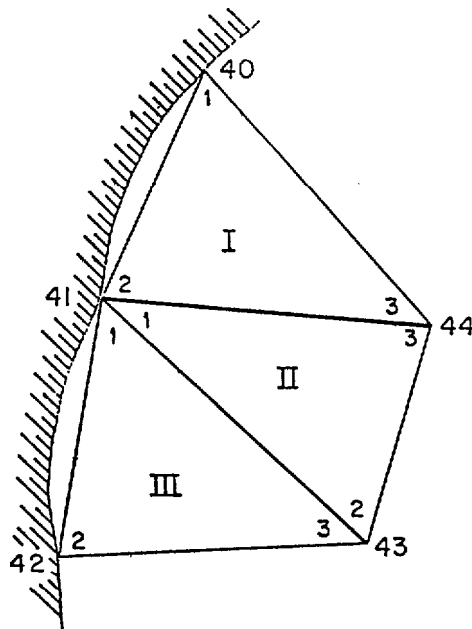


Figure 5.

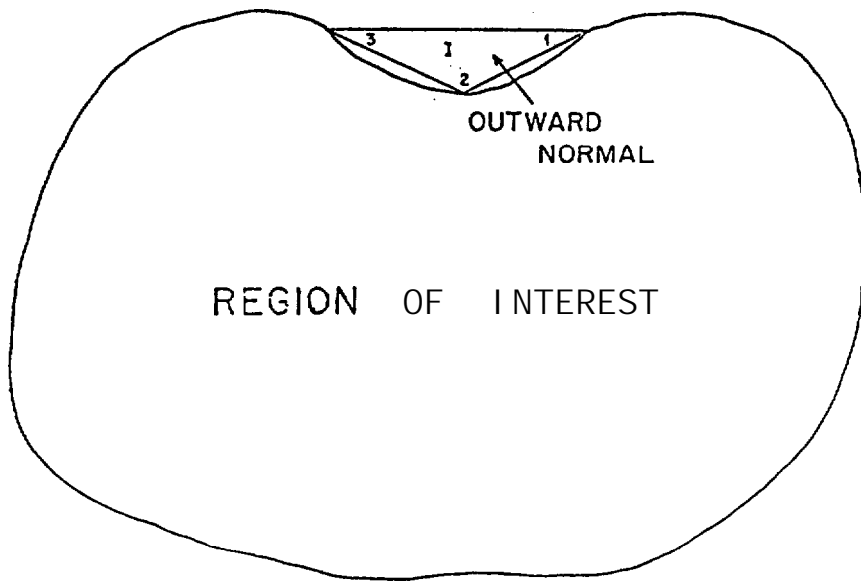


Figure 6.

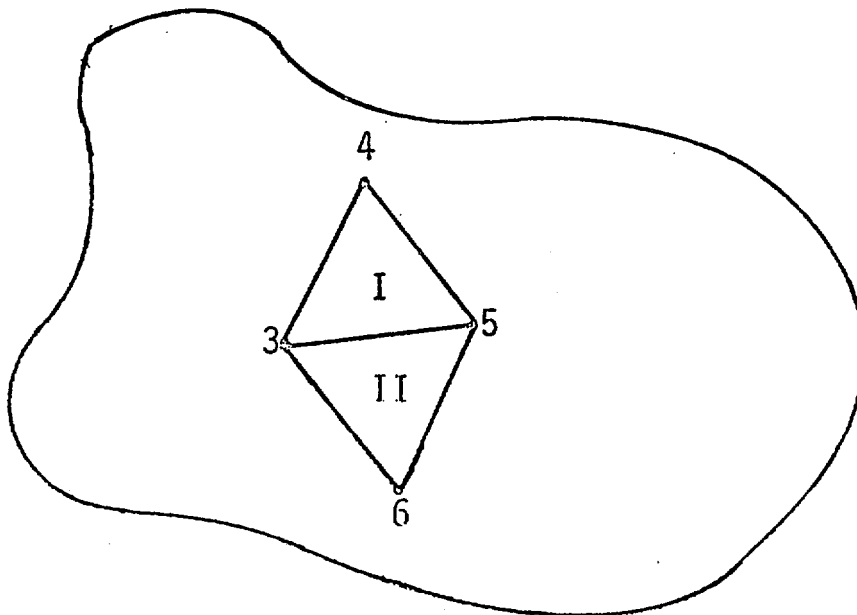


Figure 7.

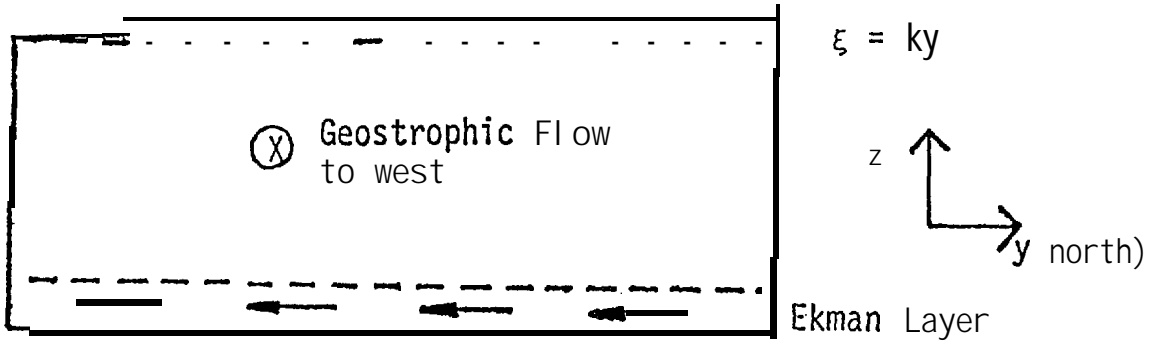


Figure 8.

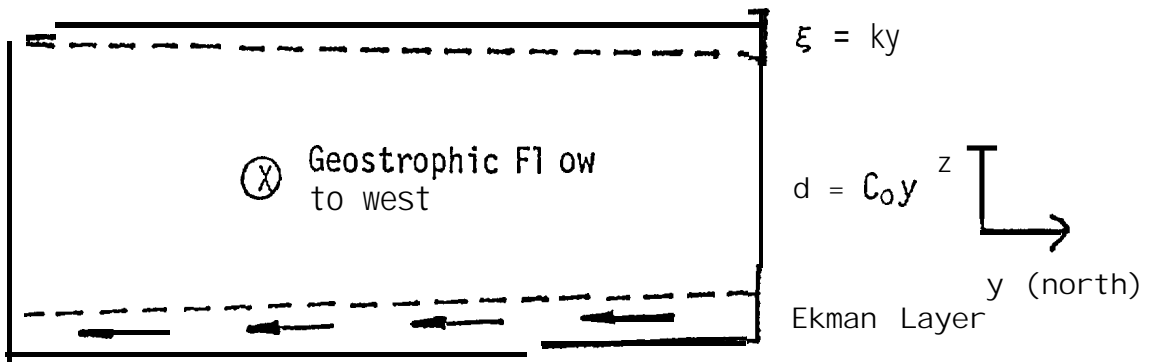


Figure 9.

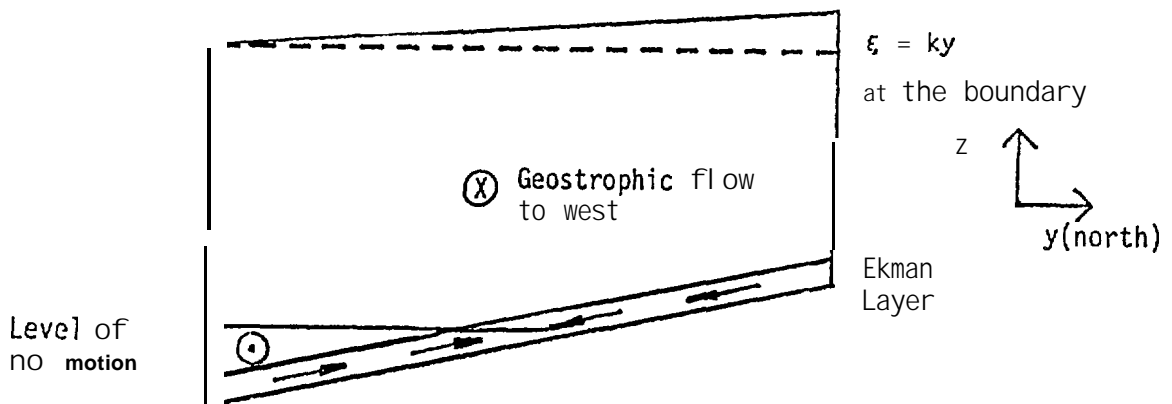


Figure 10.

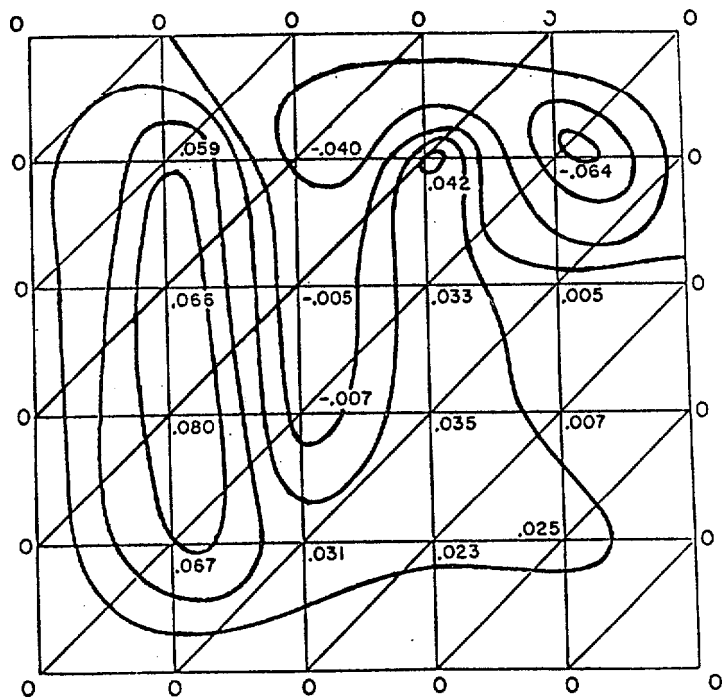


Figure 11.

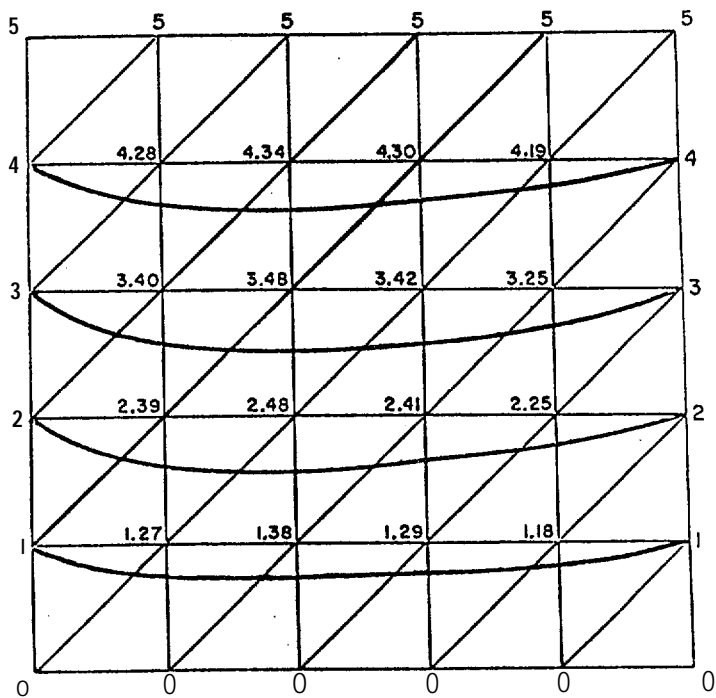


Figure 12.

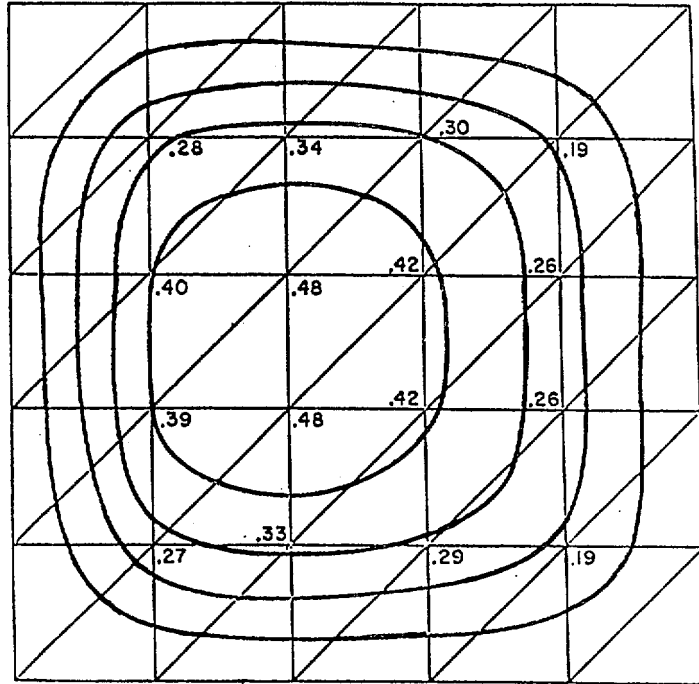


Figure 13.

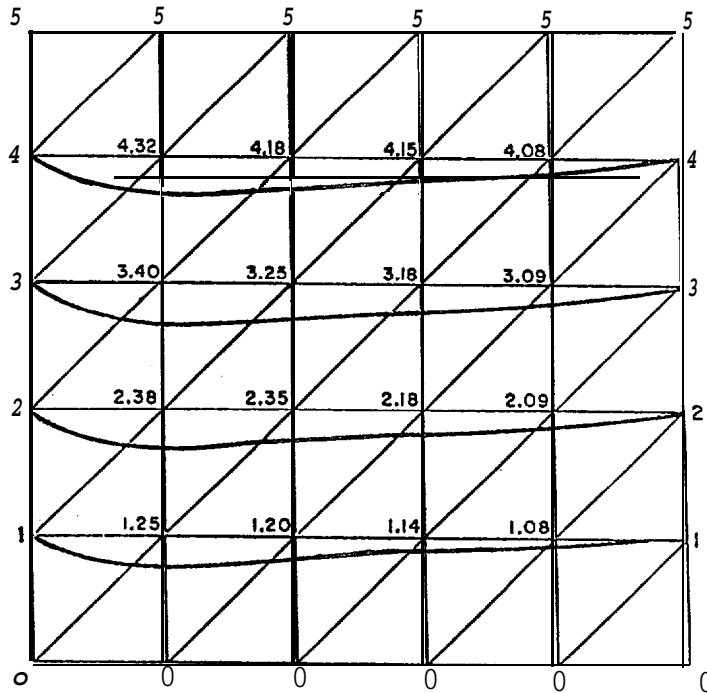


Figure 14.

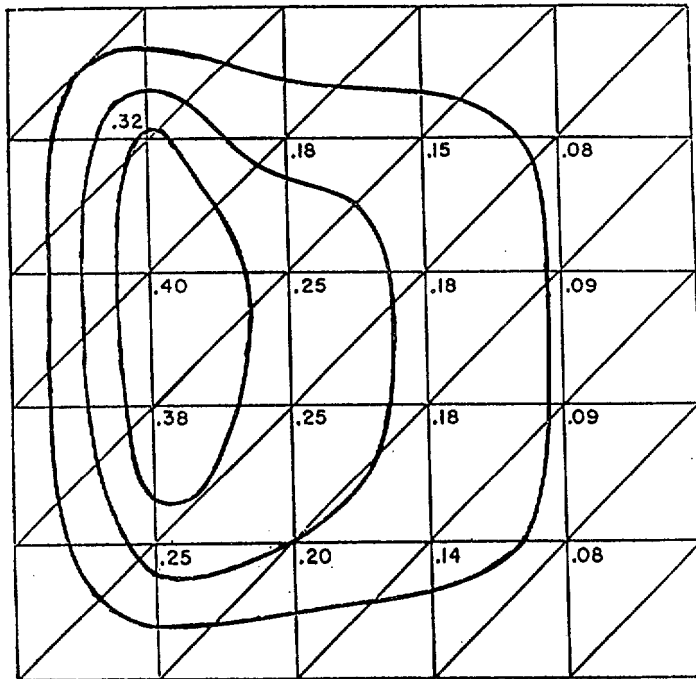


Figure 15.

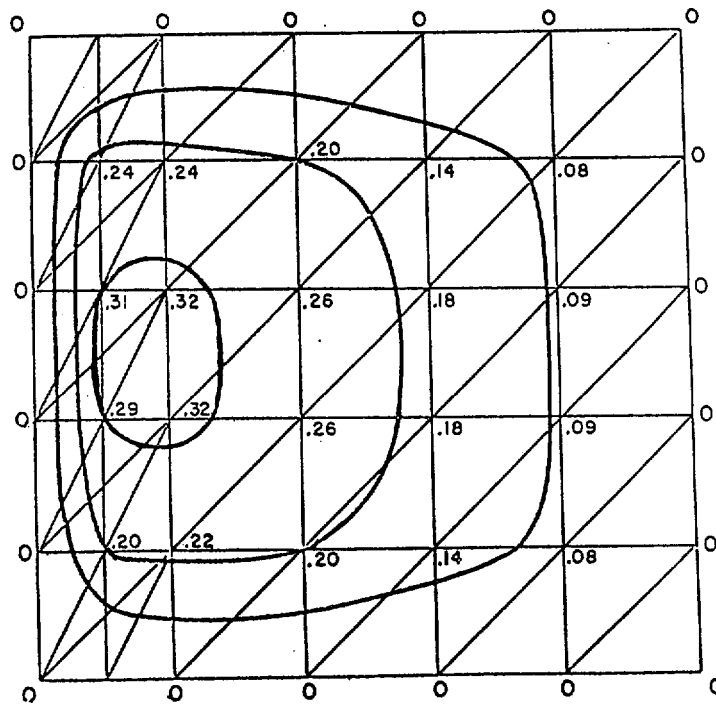


Figure 16.

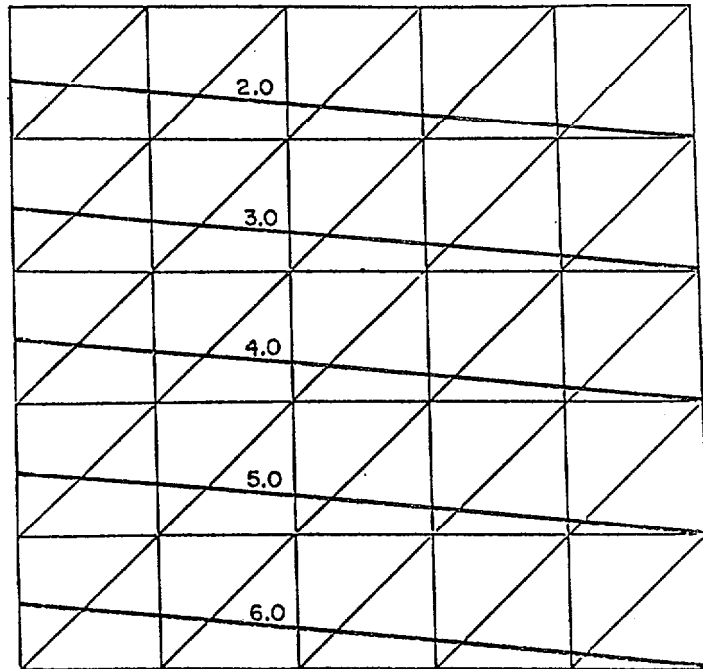


Figure 17.

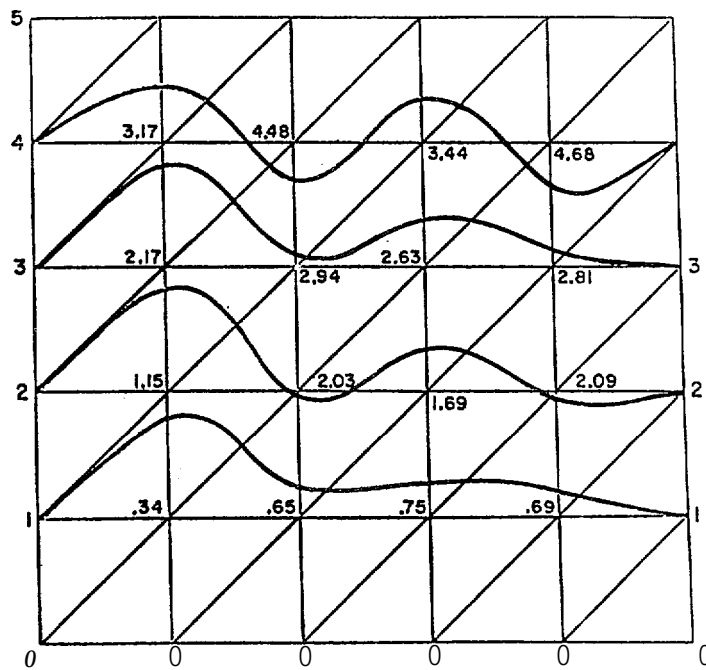


Figure 18.

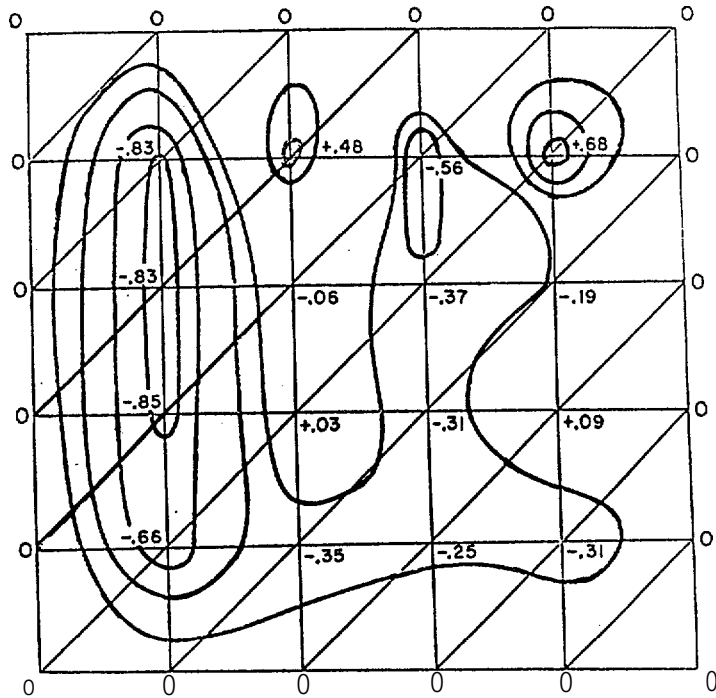


Figure 19.

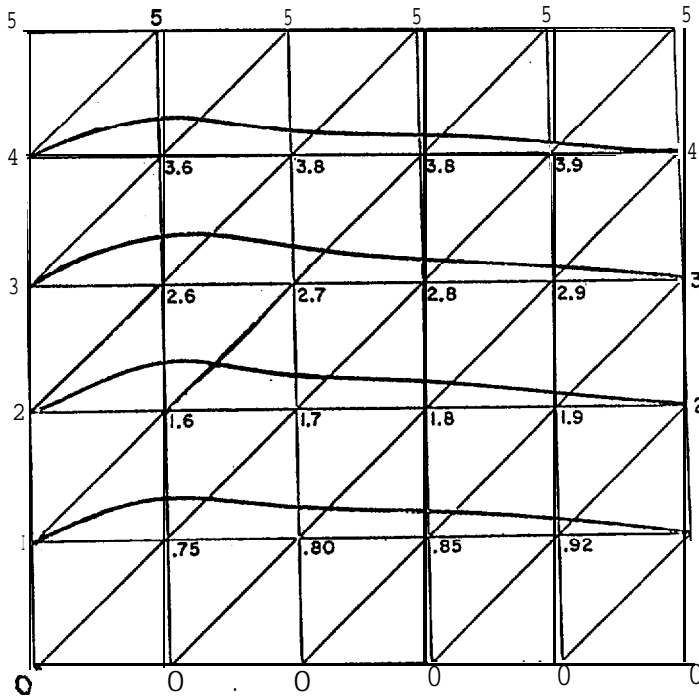


Figure 20.

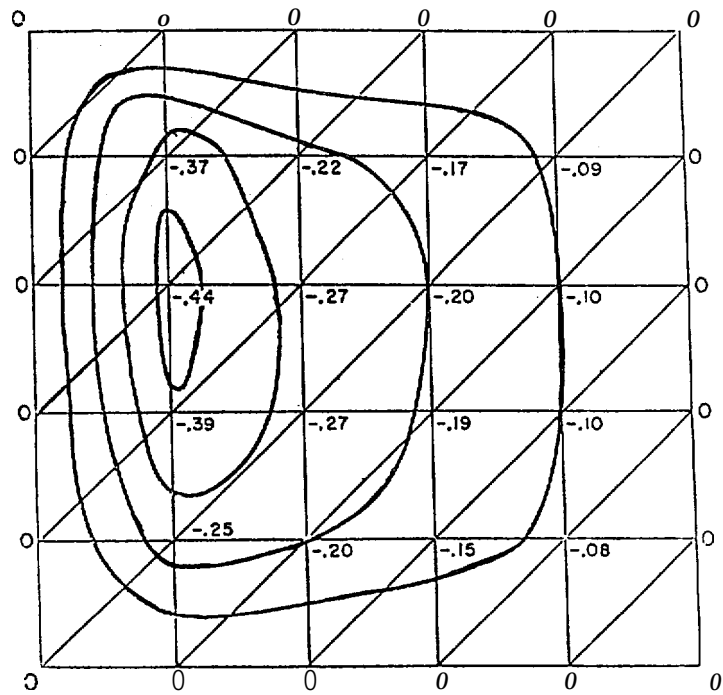


Figure 21.

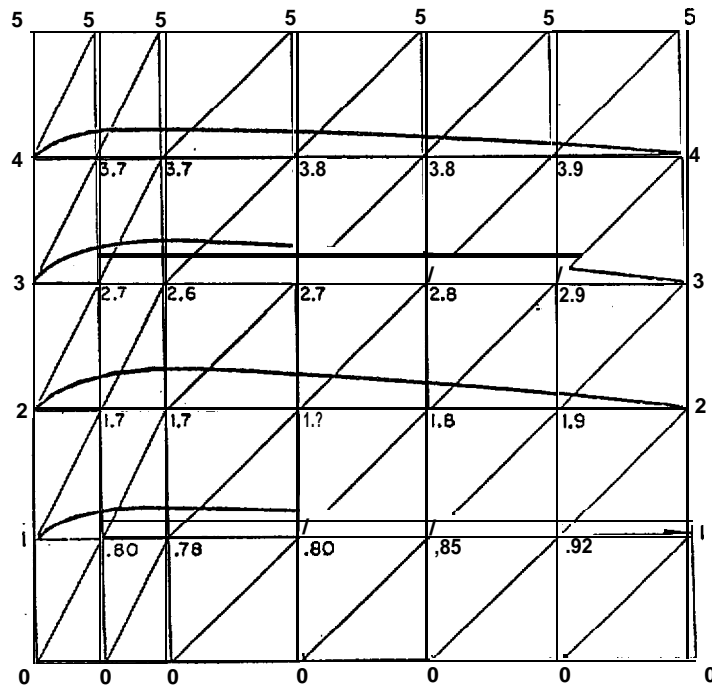


Figure 22.

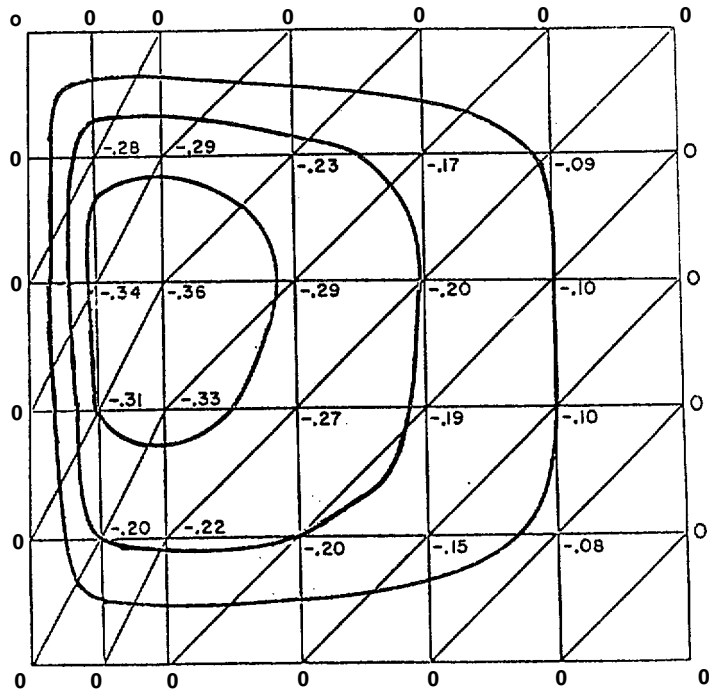
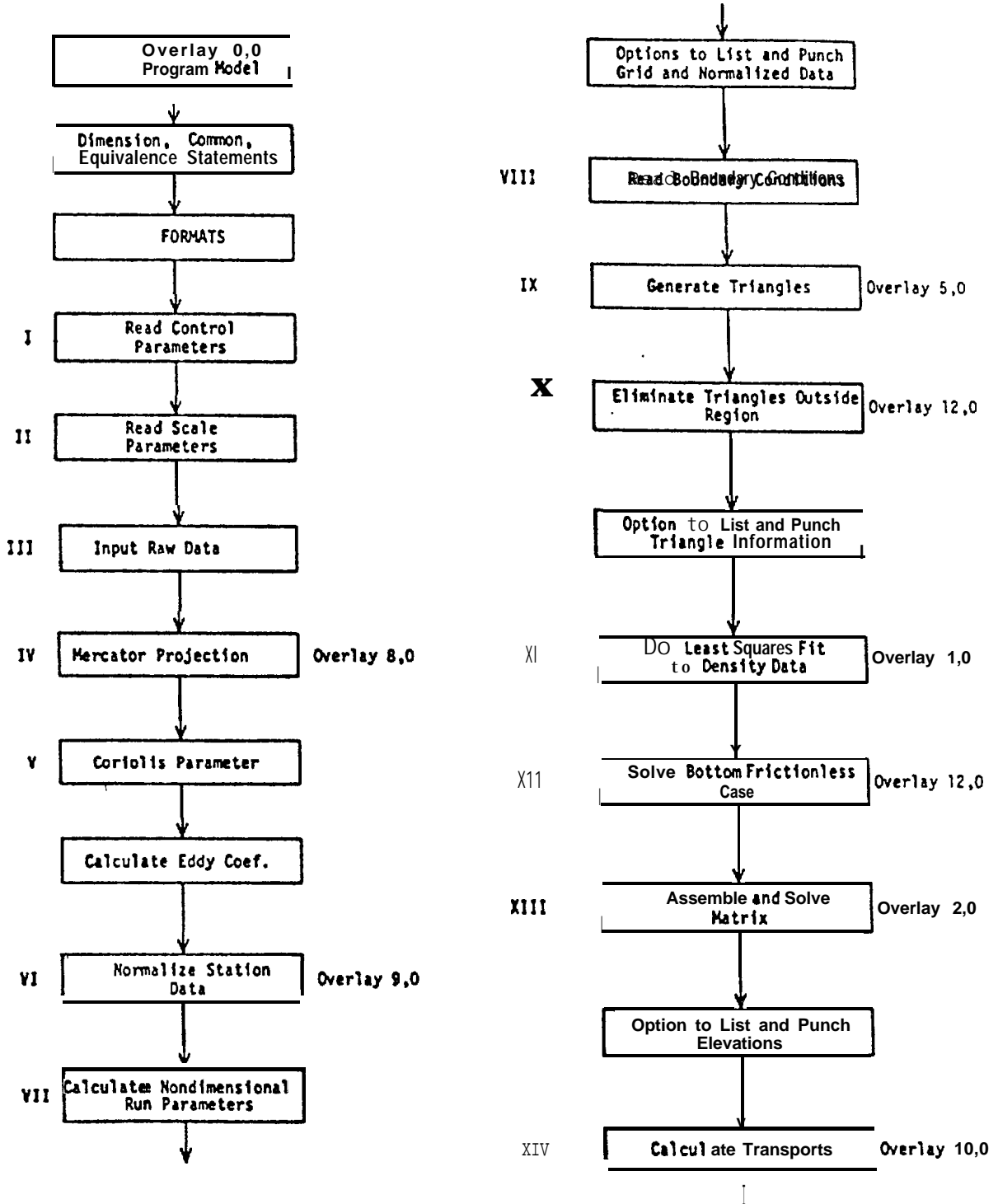
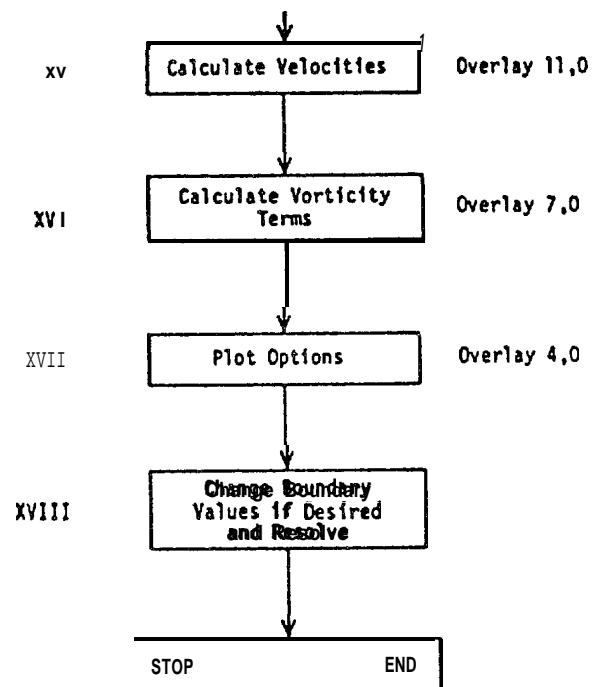


Figure 23.

Appendix 1
 REVISED FLOW CHART OF
 DIAGNOSTIC MODEL





APPENDIX II LISTING

KRONOS L419.39. 77/09/13.
 OPERATING SYSTEM
 JOB ORIGIN = BATCH.
 USER NUMBER/ID = GH
 JOBCARD NAME = GLEMS00

NN	hN	EEEEEEEEEEEE	111	YY	YY	KK	KK
NNN	NN	EEEEEEEEEEEE	1111	YY	YY	KK	KK
NNNN	NN	EE	1 11	YY	YY	KK	KK
NN NN	NN	EE	11	YY	YY	KK	KK
NN NN	NN	EE	11	YY	YY	KK	KK
NN NN	NN	EE	11	YY	YY	KK	KK
NN NN	NN	EE	11	YYY	YYY	KK	KK
NN NN	NN	EEEEEEEE	11	YYY	YYY	KK	KK
NN NN	NN	EEEEEEEE	11	YYY	YYY	KKKK	KK
NN NN	NN	EE	11	YYY	YYY	KKKKKK	KK
NN NN	NN	EE	11	YY	YY	KK	KK
NN NN	NN	EE	11	YY	YY	KK	KK
NN NN	NN	EE	11	YY	YY	KK	KK
NN NN	NN	EE	11	YY	YY	KU	KK
NN NN	NN	EEEEEEEEEEEE	111111111111	YY	YY	KK	KK
NN NN	NN	EEEEEEEEEEEE	111111111111	YY	YY	KK	KK

OUTPUT FOR: CLIFF FRIDLIND

PACIFIC MARINE ENVIRONMENTAL LABORATORY

3711 15TH AVE. N. E.

SEATTLE, WASHINGTON 98105

FTS PHONE: 399-4850

● W*W**4*****W4 ● *+m*4*4?44*+**

```

OVERLAY(MODEL,0,0)
PROGRAM MODEL(FILEI,OUTPUT,FILEO,FILE1,TAPE5=FILEI,TAPE6=OUTPUT,TA
CPE7=FILEO,TAPE1=FILE1,TAPE99)

```

C
C
C
C
C
C
C
C

```

    QUASIGEOSTROPHICMODEL WITH AN EXMAN BOTTOM FRICTION LAYER
    THE MAXIMUM NUMBER OF STATIONS THIS PROGRAM IS SETUP TO TAKE
    IS 200. IF MORE STATIONS ARE ANALYSED, THE DIMENSION STATEMENTS
    MUST BE INCREASED. THE PROGRAM AS IT STANDS TAKES ABOUT 750 COCH
    OCTAL IF THE U, W, GRAFIX LIBRARY IS ATTACHED.

```

C

```

DIMENSION XS(100),YS(100)
DIMENSION ALAT(200),ALONG(200)
DIMENSION LAT(200),LONG(200)
COMMON/LSCOEF/SA(4),SO(4),STNDVA,STNDVD

```

```

COMMON/IALPHA/ALPHA(200)
COMMON/IDELTA/DELTA(200)
COMMON/IN/N(300)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IA/A(3,3)
COMMON/EXTRA/EX(300)
COMMON/IB/B(3)
COMMON/CALC/CHP/XXMAX,YYMAX,ISTART,NBC
COMMON/IALP/ALPH(3)
COMMON/ICONST/CONST1,CONST2
COMMON/IDEPH/DEPTH(200)
COMMON/IGRAD/DALPHAX,DALPHAY,DDEPTHX,DDEPTHY,DEX,DEY,AREA
COMMON/IHEIGHT/HEIGHT(200)
COMMON/IIP/IP(3,350)
COMMON/INT/INTP(4500)
COMMON/IRHS/RHS(200)
COMMON/SCALES/USCALE,OSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
COMMON/HIND/TAUX,TAUY,CURL
COMMON/INCRK/VALP(4500)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
COMMON/CUTOFF/NIBP,NFLX,NOMAT,JJ2,DEEP

```

C

```

COMMON/XYPLOT/XPLOT,YPLOT
COMMON/GDIV/X1(102),Y1(102),X2(102),Y2(102),NX,NY,XDIV,YDIV
COMMON/DEG/NDEC
COMMON/DEG/DEGREE
COMMON/CHSIZE/SIZE
COMMON/BLCK/IBLOCK
COMMON/OBJ/XRANGE,YRANGE,XMIN,YMIN,YBT,SLFT,YTP,XRGHT
COMMON/SUB/XLEFT,YBOT,XSCALE,YSCALE
COMMON/STNCH/NCHR
COMMON/LTYPE/NLINE
COMMON/NPT/NPTS
EQUIVALENCE (HEIGHT(1),LONG(1))
EQUIVALENCE (ALAT(1),Y(1))

```

C
C
C
C
C
C
C

EQUIVALENCE(ALONG(1),X(1))
EQUIVALENCE(IP(1,1),LAT(1))

***** ***** ***** WARNING MIXED MODE OPERATIONS ABOUND*****

WE BEGIN WITH ALL THE FORHATS WENEED. NOTE THAT THE FORMAT
NUMBERS ARE ALL MULTIPLES OF 5.

5 FORMAT(15I5)
10 FORMAT(I3,I3,F6.2,I5,F6.2,F10.4,F14.4,F7.1,F6.3,F5.3,F6.3)
15 FORMAT(*1*)
20 FORMAT(*0*,*STAT*,5X,*LATITUDE*,5X,*LONGITUDE*,6X,*ALPHA*,11X,*DE
LTA,10X,*DEPTH*)
25 FORMAT(* ● t14t5XS13tIX,F4.1S5X ,I3,1X,F5.2,4X,F9.4,6X,F13.4,5X,F7.1
*,6X,F4.2,5X,F4.2,6X,F10.7)
30 FORMAT(*0*,*TRIANGLENO.*,10X,*VERTEX 1*,10X,*VERTEX 2*s10X,"VERTE
●X 3*)
35 FORMAT(**,4X,I3,19X,I3,14X,I3,15X,13)
40 FORMAT(*0*,*TRIANGLE NO.*,35X,*VERTICES*)
45 FORMAT(* ● g4Xs13S10XS*{*sF50 2,**,F5.2,*}* ,10X, ● [*tF502t*s*sF5,2, *
I 10X,*(**FS2***4*F5* 2,**)*)
50 FORMAT(I5,F20.3)
55 FORMAT(*0*,*BOUNDARY VAL. NO.*,10X,*GLOBAL LABEL*,10X,*BOUNDARY VA
LUE*,9X,*CENTIMETERS*)
60 FORMAT(* *,8X,I3,22X,I3,18X,F7.3,15X,F8.3)
65 FORMAT(*0*,*PROGRAM TERMINATED,TRIANGLE*,2X,I3,2X,*HAS BOUNDARY P
#OINTS*,2X,I3,**,2X,I3,**,2X,*AND*,2X,I3,2X,*FOR VERTICES*)
70 FORMAT(1H0,*PROGRAM STOPPED TO CHECK NEW BOUNDARY CONDITIONS*)
75 FORMAT(*0*,5X,I3,14X,I3,110*30X,I3)
80 FORMAT(*0*,*BOUNDARY VALUES*/,*0*,*B.P.*,6X,*LATITUDE*,10X,*LONGI
#TUDE*,10X,*VALUE*)
85 FORMAT(* *,I3,7X,I3,1X,F4.1,10X,I3,1X,F4.1,11X,F5.2)
90 FORMAT(*0*)
95 FORMAT(*0*,*STATNO.*,10X,*GLOBAL NO.**10X,"X COOR. ",10X,"Y-COOQ')
100 FORMAT(* *,2X,I3,15X,I3,13X,F6.2,10X,F6.2)
105 FORMAT(*1*,*RECHECK BOUNDARY TRIANGLE*,I3)
110 FORMAT(*1*,*STATION*,2X,I4,2X,*NOT ONE OF LISTED STATIONS")
115 FORMAT(*0*,*GLOBAL LABEL*,10X,*X-COOR*,10X,*Y-COOR*,17X,*ELEVATION
H NONDIH.*,5X,*ELEVATIONS IN CM.*,/)
120 FORMAT(* ● q4XS13S15XSf6.2s10X,F6.2t 20X,F9.5,12X,F10.5)
125 FORMAT(1H0,*RADIUS USED IN MERCATOR PROJECTION IS*,F10.5)
130 FORMAT(*1*,*BOUNDARYPOINTS*,1X,I3,1X,*AND ● t\$.Xt13t1XS*ARE IDENTICA
#L*)
135 FORMAT(**)
140 FORMAT(7F10.2)
145 FORMAT(**,*THIS LISTING IS BEFORE HE ELIMINATE TRIANGLES OUTSIDE
#OF CUR DOMAIN*)
150 FORMAT(7F10.3)
155 FORMAT(1H0,*X=0 LINE IS*,F7.4,1X,*RADIANS OF LONGITUDE WEST*)
160 FORMAT(1H,*Y=0 LINE IS*,F7.4,1X,*RADIANS OF LATITUDE NORTH*)
165 FORMAT(* ● j*STAT,*?9X,*GL. LAB.*,9X,*ALPHA*,11X,*DELTA*,11X,*DEPTH

```
*)
170 FORMAT(1X,I3,12X,I3,9X,F9.5,6X,F11.5,7X,F9.5,10X,F9.4)
175 FORMAT(* *,*NORMALIZED VALUES*,/)
190 FORMAT(* **Transport AND MEAN VELOCITIES NONDIMENSIONALIZED*,/)
1'35 FORMAT(1X,2F10.2,50X,*STA.*,2X,I3)
200 FORMAT(F10.4,F15.4,F10.2,F10.4,F10.4,15X,*STA.*,2X,I3)
205 FORMAT(3I5,55X,*TRIA.*, 1X,14)
210 FORMAT(F10.4,60X,*HEIGHT*,1X,I3)
215 FORMAT(* *,*SCALE PARAMETERS*)
220 FORMAT(*0*,*VELOCITY*,7X,F6.3,1X,*METERS/SEC*,//,* *,*DEPTH*,10X,F
*7.1,1X,*METERS*,//,**,*LENGTH*,9X,F8.1,1X,*METERS*,//,* *,$GRAJIT
*Y*,8X,F7.2,1X,*M/(SEC SQ)*,//,* *,*PERT. DENSITY*,2X,F6.4,1X,*GM/
*CM CU)*,//,* *,*CONST. DENSITY*,1X,F7.3,1X,*GM/(CM CU)*,//,* *,*GA
*MM*,10X,F7.1,1X,*GM/(CM SQ)*,//,* *,*CORIOLIS*,7X,F9.7, 1X,*1/SEC*
*)
225 FORMAT(*D*,*NONDIMENSIONAL RUNPARAMETERS*,//,* *,*CONST1=GEH/QFUL
* *,*F5.2,//,* *,*CONST2=GAMMA/QH=*,F7.5)
230 FORMAT(* *,*VELOCITY IS IN CENTIMETERS PER SECOND*,/)
235 FORMAT(* *,*ELEVATION SCALE FACTOR IS*,F8.3,1X,*CM. *)
245 FORMAT(3F15.8)
250 FORMAT(F10.4,F15.4,F10.4,36X,*STA.*,1X,I3)
255 FORMAT(*MEANCORICLIS IS*SF1008)
260 FORMAT(*WIND STRESS AND CURL VALUES*,3F10.4)
265 FORMAT(* *,*RAW STATION DATA*,/, * *,*TAUX=*,F10.4,5X,*TAUY=*,F10.
*4,5X,*CURL=*,F10.4)
270 FORMAT(*ALPHA COEF.*,5F10.5)
275 FORMAT(*DELTA COEF.*,5F10.5)
280 FORMAT(*D*,*EDDY COEFFICIENT=*,F10.3,1X,*GM/(CM SEC)* )
285 FORMAT(1H0.10H*****.2X,*GLOBAL MATRIX IS SINGULAR, PROBLEM
CTERMINATED*,10H*****)
```

C
C
C
C
C
C
C
C
C
C
C
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C
C
C
C
C
C
C
C
C
C

HERE WE READ IN CONTROL VALUES WHICH WILL TELL US WHAT WE WANT OUT AND WHAT WE WANT DONE

IF ANY OF THE THE PARAMETERS IS SET TO 1, THE PROGRAM WILL EXECUTE THAT OPTION. IF IT IS 09 THEN THE OPTION WILL BE BYPASSED ALL LIST OPTIONS BEGIN WITH L* AND ALL PUNCH OPTIONS BEGIN WITH IP.

LRXDATA=1 MEANS THAT THE RAW DATA WILL BE LISTED. DATA :

NOGRID=1 MEANS THAT THE CARTESIAN GRID WILL BE GENERATED, DATA :
NOTE THAT IF THIS IS 09 THEN THE GRID IS READ IN.

LGRID=1 MEANS THAT THE CARTESIAN GRID WILL BE LISTED.
IPGRID=1 MEANS THAT THE CARTESIAN GRID WILL BE PUNCHED.

NORMAL=1 MEANS THAT THE RAW DATA WILL BE NORMALIZED, DATA 3
ONCE AGAIN IF THIS IS SET TO 0, THEN THE DATA WILL HAVE TO BE READ IN.

LNORM=1 MEANS THAT THE NORMALIZED DATA WILL BE LISTED.
IPNORM=1 MEANS THAT THE NORMALIZED DATA WILL BE PUNCHED.

MAKETRI=1 MEANS THAT THE TRIANGLES WILL BE GENERATED. DATA 3

```

c      IF THIS IS SET TOO, THEN THE TRIANGLES WILL HAVE TO BE
C      READ IN
C      LTRI=1 MEANS THAT THE TRIANGLES WILL BE LISTED.
C      IPTRI=1 MEANS THAT THE TRIANGLE LABELS WILL BE PUNCHED.
C      ISTOP=1 WILL SEND THE PROGRAM TO THE GRAFIX ROUTINES AFTER
C      GENERATING THE TRIANGLES. THIS ALLOWS THE MESH TO BE CHECKED
C      BEFORE PROCEEDING ON.
C
C      NOCORY=1 MEANS THAT THE CORIOLIS PARAMETER WILL BE GENERATED. IF OATA
c      THIS IS 0, THEN THE OATA HAS TO BE READ IN. HENCE, NOCORY=1
c      WILL ALSO PUNCH THE MEAN CORIOLIS VALUE.
C
C      NOCONST=1 MEANS THAT THE NONDIMENSIONAL RUN PARAMETERS WILL BE DATA
c      GENERATED INSTEAD OF READ IN,
c      IPCCNST=1 MEANS THAT THE NONDIMENSIONAL RUN PARAMETERS WILL BE
c      PUNCHED,
c
c      LBV=1 WILL LIST THE BOUNDARY CONDITIONS THAT ARE READ IN. DATA
C
C      NOELEV=1 MEANS THAT THE PROGRAM WILL GENERATE THE SURFACE DATA
c      ELEVATIONS. THE ALTERNATIVE IS TO READ THEM IN
c      LELEV=1 MEANS THAT THE PROGRAM WILL LIST THE SURFACE ELEVATIONS.
c      IPELEV=1 MEANS THAT THE PROGRAM WILL PUNCH THE SURFACE ELEVATIONS.
C
C      NOTRANS=1 MEANS THAT THE PROGRAM WILL GENERATE THE TRANSPORTS OATA
c      IPTRANS=1 MEANS THAT THE PROGRAM WILL PUNCH THE TRANSPORT INFORMA.
c
c      NOVELC=1 MEANS THAT THE VELOCITIES WILL BE GENERATED. OATA 10
c      IPVELO=1 MEANS THAT THE VELOCITY INFORMATION WILL BE PUNCHED.
C
c      NOTERY=1 MEANS THAT THE VORTICITY TERMS WILL BE LISTED. DATA 11
C
C      NBC=NUMBER OF DIFFERENT BOUNDARY CONDITION SETS YOU HAVE. DATA 12
C
C      NOPLOT=1 MEANS THAT THE PROGRAM WILL DO CALCOMP PLOTTING. OATA 13
c      IWHAT=-1 MEANS THAT ONLY THE TRIANGLES WILL BE PLOTTED.
c      IWHAT=0 MEANS THAT BOTH THE TRIANGLES WILL BE PLOTTED AND THE
c      SURFACE ELEVATIONS WILL BE CONTOURED.
c      IWHAT=1 MEANS THAT ONLY THE SURFACE ELEVATIONS WILL BE CONTOURED.
C
C      LSF=1 MEANS THAT THE LEAST SQUARES FIT TO THE ALPHA AND DELTA DATA 14
c      FIELDS WILL BE DONE. IF THIS IS ZERO, THEN THE COEFFICIENTS
c      WILL HAVE TO BE READ IN. CONSEQUENTLY, IF LSF=1 THE
c      COEFFICIENTS WILL AUTOMATICALLY BE PUNCHED.
C      LCOEF=1 MEANS THAT THE LEAST SQUARES FIT INFORMATION WILL BE
C      LISTED.
C
C      SMTHA=THE NUMBER OF STANDARD OBLIVATIONS YOU WANT THE ALPHA FIELD OATA 15
c      SMOOTHED TO. IF SMTHA=0, THE WATER IS MADE HOMOGENEOUS. IF
c      SMTHA=-1., THEN NO SMOOTHING IS DONE.
C      SMTHD=DELTA SMOOTHING PARAMETER. THE OPTIONS ARE IDENTICAL TO
c      THE ALPHA SMOOTHING OPTIONS. SEE ABOVE FOR DETAILS.
C

```

```

c      IFILE=-1 MEANS THAT THE PROGRAM WILL PUT THE DECOMPOSED MATRIX      DATA 1
c      ONTO FILE1.
c      IFILE=0 MEANS THAT THE PROGRAM WILL DECOMPOSE THE MATRIX BUT NOT
c      PUT IT ONTO FILE.
c      IFILE=1 MEANS THAT THE PROGRAM WILL READ THE DECOMPOSED MATRIX
c      FROM FILE1.
c      *****REMEMBER TO REQUEST FILE1 AND CATALOG IT IF THE MATRIX IS
c      PLACED ONTO FILE1. ALSO REMEMBER TO ATTACH THE FILE IF THE
c      THE MATRIX IS TO BE READ FROM THE FILE.*****
c
c      NIBP=NUMBER OF INTERIOR (ISLAND) BOUNDARY POINTS YOU HAVE. ONE      DATA 1
c      ISLAND IS PERMITTED.
c      NFLX=NUMBER OF ONSHORE BOUNDARY POINTS YOU HAVE. THESE ARE THE
c      BOUNDARY POINTS WHICH DEFINE THE MAINLAND COASTLINE.
c
c      NOBCK=1 MEANS THAT THE PROGRAM WILL ALTER THE OPEN BOUNDARY      DATA 1
c      CONDITIONS BY SOLVING THE BOTTOM FRICTIONLESS CASE.
c      NOINTG=1 MEANS THAT THE INTEGRATION ALONG DEPTH CONTOURS WILL BE
c      DONE. THE ALTERNATIVE (NOINTG=0), IS TO READ IN THE
c      ELEVATION CHANGES ALONG THE DEPTH CONTOURS.
c      IPINTG=1 MEANS THAT THE ELEVATION CHANGES ALONG THE DEPTH CONTOURS
c      WILL BE PUNCHED OUT. NOTE THAT THE ELEVATION CHANGES ALONG
c      DEPTH CONTOURS ARE FUNCTIONS ONLY OF THE DEPTH, AND FORCING
c      FUNCTIONS, NOT OF THE BOUNDARY VALUES THEMSELVES.
c      IPBV=1 MEANS THAT THE NEWLY ADJUSTED BOUNDARY VALUES WILL BE
c      PUNCHED.
c      NOHOLT=1 MEANS THAT THE PROGRAM WILL BE TERMINATE AFTER THE
c      BOUNDARY VALUES HAVE BEEN ADJUSTED TO SEE IF THE BOUNDARY
c      CONDITIONS ARE REASONABLE.
c
c      DEEP=CUTOFF DEPTH AT WHICH THE BOUNDARY VALUES ARE OBTAINED FROM   DATA 1
c      DYNAMIC HEIGHT CALCULATIONS, THESE BOUNDARY VALUES WILL NOT
c      BE ALTERED.
c      THE QUANTITY DEEP IS READ IN NEGATIVE METERS.
c
c      READ(5,5)LRWDATA      DATA
c      READ(5,5)NOGRID,LGRID,IPGRID      DATA
c      READ(5,5)NORML,LNORM,IPNORM      DATA
c      READ(5,5)MAKETRI,LTRI,IPTRI,ISTO?  DATA
c      READ(5,5)NOCORY      DATA
c      READ(5,5)NOCONST,IPCONST      DATA
c      READ(5,5)LBV      DATA
c      READ(5,5)NOELEV,LELEV,IPELEV      DATA
c      READ(5,5)NOTRANS,IPTRANS      DATA
c      READ(5,5)NOVELO,IPVELO      DATA 1
c      READ(5,5)KOTERM      DATA 1
c      READ(5,5)NBC      DATA 1
c      READ(5,5)NOPLOT,INHAT      DATA 1
c      READ(5,5)LSF,LCCEF      DATA 1
c      READ(5,140)SMTHA,SMTHD      DATA 1
c      READ(5,5)IFILE      DATA 1
c      READ(5,5)NIBP,NFLX      DATA 1

```

```

READ(5,5)NOBCK,NOINTG,IPINTG,IPBV,NOHALT      DATA 1
READ(5,150)DEEP                                DATA 1
C
NEH8V=1
ISTART=0
C
C     WE NOW PROCEED TO READ IN THE SCALE PARAMETERS TO BE USED FOR OUR
C     NONDIMENSIONALIZED GRID AND OTHER SCALING.
C     THE VELOCITY SCALE, #USCALE#, IS IN METERS/SEC. THE DEPTH SCALE,
C     #DSCALE, IS IN METERS. THE HORIZONTAL LENGTH SCALE, #ALSCALE#,
C     ALSO IS IN METERS.
C     G, GRAVITY, IS IN METERS PER SECOND SQUARED
C     E, THE PERTURBATION DENSITY, IS IN GM. PER CM. CUBED
C     Q, THE CONSTANT DENSITY IS ALSO IN GM. PER CM. CUBED,
C     GAMMA, THE BOTTOM FRICTION COEFFICIENT, IS IN GM. PER CM. SQUARED
C     EDDY IS THE EDDY COEFFICIENT CALCULATED FROM GAMMA.
C
READ(5,150)USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA
DEEP=DEEP/OSCALE
C
C     NOW THE STATION DATA IS READ IN.
C     ALPHA IS ENTERED IN (GM/CM**3)*METERS AND DELTA IS ALPHA*METER
C     TAU, HIND STRESS, IS IN DYNES/(CM*CM)
C     CURL IS READ IN ASCYNES PER CM. CUBED.
C
C     AFTER THE LAST STATION DATA CARD IS READ, A CARD WITH STATION
C     NUMBER ZERO IS READ IN TO INDICATE THAT NO MORE STATION DATA
C     WILL BE INPUTED.
C
C     NOTE***THE DEPTH, ALPHA, AND DELTA VALUES ARE POSITIVE QUANTITIES
C
C     IF (NOGRID.EQ.0.AND.NORMAL.EQ.0) GO TO 111
C     I=1
C 2 READ(5,10)N(I) ,LAT(I) ,ALAT(I) ,LONG(I) ,ALONG(I) ,ALPHA(I) ,DELTA(I) ,D
C     PTH(I)
C     DEPTH(I)=-DEPTH(I)
C     IF(N(I).EQ.0) GO TO 4
C     I=I+1
C     GO TO 2
C
C 4  NVRTX=I-1
C     READ(5,245)TAUX,TAUY,CURL
C
C     WE EXIT FROM HERE WITH THE VALUE OF NVRTX, THE NUMBER OF VERTICES
C
C     HERE THE STATION DATA IS ECHO CHECKED IF REQUESTED
C
C     IF(LRWDATA.EQ.0) GO TO 8
C     WRITE(6,15)
C     WRITE(6,265)TAUX,TAUY,CURL
C     WRITE(6,20)
C     WRITE(6,90)

```

```

      DO 6 J=1,NVRTX
6 WRITE(6,25)N(J),LAT(J),ALAT(J),LONG(J),ALONG(J),ALPHA(J),DELTA(J),
      #DEPTH(J)
8 CONTINUE
C
C
111 CONTINUE
C
      IF(NOGRID.EQ.0) GO TO 12
      IPUNCH=IPGRID
      CALL CVERLAY(5HMODEL,8,0,0)
      XMAX=DALPHAX
      YMAX=DALPHAY
      YMIN=DDEPTHX
      RADIUS=CDEPTHY
      XMIN=DEX
      GO TO 13
12 CONTINUE
C
      *****NOTE THAT IF THE GRIO Subroutine ISBYPASSED, ONE NEEDS TO
      READ IN YMIN,YMAX,YYMAX, AND XXMAX
C
      READ(5,5)NVRTX
      DO 3001 I=1,NVRTX
      READ(5,195)X(I),Y(I),N(I)
3001 CONTINUE
      READ(5,140)YMIN,YMAX,YYMAX,XXMAX
13 CONTINUE
C
C
      NOW WE GO ON TO CALCULATE F KNOT, THE HEAN CORIOLISVALUE.
C
      IF(NOCORY.EQ.0) GO TO 22
      CALL BETA1(YMIN,YMAX,F0)
      WRITE(7,255)F0
      GO TO 23
22 READ(5,255)F0
23 CONTINUE
C
      EDDY=GAMMA*GAMMA*2.*FC/Q
C
      HERE THE STATION DATA IS NORMALIZED IF REQUESTED.
C
      IF(NORMAL.EQ.0) GO TO 24
      IPUNCH=IPNORM
      CALL CVERLAY(5HMODEL,9,0,0)
      GO TO 6026
C
24 CONTINUE
      DO 1012 I=1,NVRTX
      READ(5,250)ALPHA(I),DELTA(I),DEPTH(I),N(I)
1012 CONTINUE

```



```

      READ(5,260)TAUX,TAUY,CURL
C
C
C
6026 CONTINUE
C   HERE WE LIST THE DIMENSIONAL COEFFICIENTS
C
      WRITE(6,15)
      WRITE(6,215)
      WRITE(6,220)USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO
      WRITE(6,280)EDDY
C
C   HERE WE HAVE THE OPTION TO GENERATE THE NON DIMENSIONAL RUN
C   PARAMETERS OR READ THEM IN
C   WE ALSO HAVE THE OPTION TO PUNCH THEM UP FOR FUTURE USE
C
      IF(NOCNST.EQ.1) GO TO 89
C
C   HERE NONDIMENSIONAL RUN PARAMETERS ARE READ IN
C   THESE ARE THE CONST COEFFICIENTS IN THE EQUATION
      READ(5,245)CONST1,CONST2
C
      GO TO 91
89 CONTINUE
      CONST1=(G*E*DSCALE)/(Q*FO*USCALE*ALSCALE)
      CONST2=GAMMA/(Q*DSCALE*100.)
91 CONTINUE
      WRITE(6,225)CONST1,CONST2
C
C   THIS IS AN OPTION TO OUTPUT GRID DATA
C
      IF(LGRID.EQ.0) GO TO 16
      WRITE(6,15)
      WRITE(6,95)
      WRITE(6,90)
      DO 14 I=1,NVRTX
      HRXTE(6,1001N[I],SI,X(I),Y(I)
14 CONTINUE
      WRITE(6,125)RADIUS
      WRITE(6,155)XMIN
      WRITE(6,160)YMIN
16 CONTINUE
C
C
C   THIS IS AN OPTION TO LIST THE NORMALIZED DATA
C
      IF(LNORM.EQ.0) GO TO 29
      WRITE(6,15)
      WRITE(6,175)
      WRITE(6,165)
      DO 27 I=1,NVRTX
      WRITE(6,170)N(I),I,ALPHA(I),DELTA(I),DEPTH(I)
27 CONTINUE

```

```

29 CONTINUE
C
C
C THIS IS AN OPTION TO PUNCH NORMALIZED DATA
C
C IF(IPCONST.EQ.0) GO TO 31
C WRITE(7,245)CCNST1,CONST2
31 CONTINUE
C
C *****
C
C WENOWPROCEED TO READ IN THE TRIANGLES IF NECESSARY.
C IFMAKETRI=0, THEN THE TRIANGLE VERTEX NUMBERS WILLBE READ IN
C ANO NO TRIANGLES WILL BE GENERATED.
C
C IF(MAKETRI.EQ.1) GO TO 902
C HERE NTRI, THE NUMBER OF TRIANGLES ARE READ IN
901 READ(5,5)NTRI
C NOW TO READIN THE GLOBAL LABELS OF EACH TRIANGLE VERTEX
C DO 903 I=1,NTRI
C READ(5,5)(IP(J,I),J=1,3)
903 CONTINUE
902 CONTINUE
C
C
C WENOW READ INTHEBOUNDARY VALUES AND THEIR STATION NUMBERS
C SURFACE ELEVATIONS ALONG THE BOUNDARYSHOULD BE IN CM.
C
C *****
C REMEMBER, IF AN ISLAND IS PRESENT, ITS BOUNDARY CONDITIONS SHOULD
C BE READIN FIRST IN CLOCKWISE ORDER. THEN THE INSHORE BOUNDARY
C CONDITIONS SHCULDBEREAD IN COUNTERCLOCKWISE ORDER. THESE
C ARE THEN FOLLOVEDBY THE REST OF THE BOUNDARY CONDITIONS READ
C IN COUNTERCLOCKWISE ORDER.
C THE BOUNDARY Elevations FOR THE NO FLUX BOUNDARIES WILL BE
C CALCULATE RELATIVE TO THE FIRST NO FLUX STATION. THEREFORE,
C IF AN ISLAND IS PRESENT, THE ELEVATION OF THE FIRST ISLAND
C BOUNDARY POINT NEEDS TO BE DEFINED. THEN THE ELEVATION OF
C THE FIRST ONSHORE, COASTLINE BOUNDARY STATION MUST ALSO BE
C SPECIFIED. ALLCTHER NO FLUX BOUNDARY ELEVAY1ONS OONT NEED
C TO BESPECIFIED.
C A BLANK CARD SHCULD BE READ IN AFTER ALL THEBOUNDARYCONDIDITIONS
C HAVE BEEN READ.
C ● **+***4*+?***?****
C
C DIM=G/(FO*USCALE*ALSCALE*Q*100.)
C I=1
58 READ(5,50) ISTAT,BVAL
C IF(ISTAT.EQ.0) GO TO 402
C 00 54 J=1,NVRTX
C IF(ISTAT.NE.N(J)) GO TO 54
C IB(I)=J

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```

      BV(I)=BVAL*DIM
      I=I+1
      GO TO 58
54  CONTINUE
      WRITE(6,110)ISTAT
      GO TO 2001
402 CONTINUE
      62 NBV=I-1
C
C      HERE, WE EXIT WITH, NBV, THE NUMBER OF BOUNDARY POINTS
C
C      HERE HE HAVE AN OPTION TO ECHO CHECK THEBOUNDARYCONDITIONS
C
      IF(LBV.EQ.0) GO TO 746
      WRITE(6,15)
      WRITE(6,55)
      WRITE(6,90)
      DO 64 I=1,NBV
      BVV=BV(I)/DIM
      WRITE(6,60)I,IB(I),BV(I),BVV
      64 CONTINUE
746 CONTINUE
C
C      NOW GENERATE THE TRIANGLES IF REQUESTED.
C
      IF(MAKETRI.EQ.0) GO TO 904
      IPUNCH=NI8P
      CALL OVERLAY(5HMODEL,5,0,0)
C
904 CONTINUE
C
401 CONTINUE
      IF(MAKETRI.EQ.0) GO TO 754
C
C      IF TRIANGLES WERE INTERNALLY GENERATED, WE WILL PROCEED TO
C      ELIMINATE THE TRIANGLES EXTERIOR TO THE REGION OF INTEREST.
C
      LIST=LTRI
      CALL OVERLAY(5HMODEL,6,0,0)
754 CONTINUE
C
      IF(LTRI.EQ.0) GO TO 57
C      TRIANGLE NUMBERS ALONG WITH THE GLOBAL LABELS OF EACH VERTEX IS
C      LISTED AND ON THE NEXT PAGE, THE VERTEX COORDINATES ARE LISTED
C
      WRITE(6,15)
      WRITE(6,30)
      WRITE(6,90)
      DO 26 I=1,NTRI
26  WRITE(6,35)I,(IP(J,I),J=1,3)
      WRITE(6,15)
      WRITE(6,40)

```

```

WRITE(6,90)
DO 28 I=1,NTRI
  II=IP(1,I)
  IL=IP(2,I)
  IM=IP(3,I)
28 WRITE(6,45) I,X(II),Y(II), X(IL),Y(IL),X(IM),Y(IM)
57 CONTINUE
C
C THIS IS THE OPTION TO PUNCH THE TRIANGLE OATA
C
IF(IPTRI.EQ.0) GO TO 157
WRITE(7,5)NTRI
DO 156 I=1,NTRI
  WRITE(7,205)IP(1,I),IP(2,I),IP(3,I),I
156 CONTINUE
157 CONTINUE
C
C
C WE NOW FIT THE ALPHA AND DELTA TO A THIRD ORDER POLYNOMIAL BY
C DOING A LEAST SQUARES FIT TO THE ALPHA AND DELTA FIELDS.
C
IPUNCH=LSF
LIST=LCOEFF
SA(1)=SMTHA
SD(1)=SMTHD
CALL CVERLAY(5HMODEL,1,0,0)
C
C
C 132 CONTINUE
C *****
C
C NOW PROCEED TO ALTER THE BOUNDARY CONDITIONS BY SOLVING THE
C INVISCID CASE ALONG BOUNDARY DEPTH CONTOURS.
C
C
IF(NOBACK.EQ.0) GO TO 68
LIST=NOINTG
IPUNCH=IPINTG
CALL CVERLAY(5HMODEL,12,0,0)
IF(IPBV.EQ.0) GO TO 67
DO 66 I=1,NBV
  BVV=BV(I)/DIM
  J=IB(I)
66 WRITE(7,50)N(J),BVV
67 CONTINUE
IF(NOHALT.EQ.0) GO TO 68
WRITE(6,70)
GO TO 2001
68 CONTINUE
C
C IF THE LEAST SQUARES COEF. TO THE BAROCL. FIELD WAS GENERATED
C THEN WE WILL SAVE THE VALUES

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```

        IF(ISOV.EQ.0) GO TO 69
C      NOW PROCEED TO PUNCH THE VALUES UP SO WE DO NOT HAVE TO
C      REGENERATE THEM AGAIN.
        WRITE(7,270)SA(1),SA(2),SA(3),SA(4),STNOVA
        WRITE(7,275)SD(1),SD(2),SD(3),SD(4),STNOVD
169 CONTINUE

C      IF(ISTOP.EQ.1) GO TO 2999
C      ● *****

C      133 CONTINUE
C      WENOW ASSEMBLE THE MATRIX

C      NOMAT=0
C      IF(NEWBV.GT.1) NOMAT=-1
C      IF(NOELEV.EQ.1) GO TO 164
C      DO 162 I=1,NVRTX
C      READ(5,210)HEIGHT(I)
162 CONTINUE
C      GO TO 134
164 CONTINUE
C      LIST=IFILE
C      CALL OVERLAY(5HMODEL,2,0,0)
C      IF(NVRTX.LT.0) 60 TO 4001

C      134 CONTINUE
C      U
C      THIS IS AN OPTION TO LIST THE ELEVATION OF THE VERTICES.
C      C
C      IF(LELEV.EQ.0) GO TO 178
C      WRITE(6,15)
C      ELEV=(F0*USCALE*ALSCALE/G)*100.
C      WRITE(6,235)ELEV
C      WRITE(6,115)
C      DO 176 I=1,NVRTX
C      DIM=HEIGHT(I)*ELEV
C      WRITE(6,120)I,X(I),Y(I) ● HEIGHT(I),DIM
176 CONTINUE
178 CONTINUE

C      THIS IS THE OPTION TO PUNCH THE ELEVATION DATA
C      C
C      IF(IPELEV.EQ.0) GO TO 159
C      DO 158 I=1,NVRTX
C      WRITE(7,210) HEIGHT(I)SI
158 CONTINUE
159 CONTINUE

C      HERE HE HAVE THE OPTION TO CALCULATE THE TRANSPORT AT THE CENTROID
C      OF EACH TRIANGLE
C      C
C      IF(NCTRANS.EQ.0) GO TO 184

```

```

IPUNCH=IPTRANS
CALL OVERLAY(5HMODEL,10,0,0)
C
184 CONTINUE
C
C OPTION TO CALCULATE AND LIST EKMAN VELOCITY, BAROTROPIC VELOCITY
C THEIRSUM, AND BOTTOM VELOCITY
C
IF(NOVELO.EQ.0) GO TO 186
IPUNCH=IPVELO
CALL OVERLAY(5HMODEL,11,0,0)
185 CONTINUE
C
C OPTION TO CALCULATE AND LIST THE DYNAMIC BALANCE TERMS.
C
IF(NOTERM.EQ.0) GO TO 188
CALL OVERLAY(5HMODEL,7,0,0)
188 CONTINUE
C WE NOW HAVE THE OPTION OF PLOTTING THE TRIANGLES AND LABELING
C THE VERTICIES WITH THEIR ELEVATIONS.
C ONCE AGAIN THE UNIV.CF HASH.*S N.P.S. SYSTEM IS UTILIZED.
C
2999 CONTINUE
IF(NOPLOT.EQ.0.AND.NBC.EQ.1) GO TO 2001
IF(NOPLOT.EQ.0) GO TO 1999
C
C WE NOW PROCEED TO PLOT THE SURFACE ELEVATIONS.
C LIST=IKHAT
CALL OVERLAY(5HMODEL,4,0,0)
C
C
1999 CONTINUE
IF(NEHBV.GE.NBC) GO TO 2001
CALL NEHBVAL
NEHBV=NEHBV+1
IF(JJ2.EQ.0) GO TO 133
GO TO 132
C
C
C IF THE FORCING FUNCTIONS ARE ALTERED, THEN THE NEW VALUES ARE
C READ IN SUBROUTINE NEHBVAL ALONG WITH ANY NEW BOUNDARY VALUES
C THEN ONE REASSEMBLES THE RIGHT HAND SIDE AND READJUSTS THE NEW
C BOUNDARY VALUES BY SETTING JJ2 IN COMMON BLOCK CUTOFF TO 1 IN
C SUBROUTINE NEHBVAL. THIS WILL SEND THE PROGRAM INTO BCHK. IF
C ONLY THE BOUNDARY VALUES ARE CHANGED IN SUBROUTINE NEHBVAL, THEN
C JJ2=0 AND ONLY THE NEW BOUNDARY VALUES ARE ALTERED AND NOT THE
C ENTIRE RIGHT HAND SIDE.
C
C
4001 WRITE(6,285)
2001 STOP
ENO

```

```

OVERLAY(MODEL,1,0)
PROGRAM LEAST
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH
COMMON/IALPHA/ALPHA(200)
COMMON/IDELTA/DELTA(200)
COMMON/LSCOEFS/SA(4),SD(4),STNDVA,STNDVD
COMMON/IHEIGHT/HEIGHT(200)
COMMON/IDEPHT/DEPTH(200)
270 FORMAT(*ALPHA CCEF**,5F10.5)
275 FORMAT(*ALPHA CCEF.*,5F10.5)
SMTHA=SA(1)
SMTHD=SD(1)
LSF=IPUNCH
IF(LSF.EQ.0) GO TO 166
LCOEFS=LIST
CALL LQFIT(ALPHA,SA,STNDVA,LCOEFS,NVRTX)
LCOEFS=-LCOEFS
CALL LQFIT(DELTA,SD,STNDVD,LCOEFS,NVRTX)
C *****NOTE, THE COEFFICIENTS ARE STORED INTO SA, AND SD* SA HOLDS
c THE COEFFICIENTS FOR ALPHA AND SO FOR DELTA.
GO TO 167
166 CONTINUE
c HERE WE READ IN THE ALPHA AND DELTA COEFFICIENTS IF THEY WERE
c NOT GENERATED,
READ(5,270) SA(1),SA(2),SA(3),SA(4),STNDVA
READ(5,275) SD(1),SD(2),SD(3),SD(4),STNDVD
167 CONTINUE
c
C WE NOW HAVE THE OPTION OF SMOOTHING THE ALPHA AND DELTA FIELDS.
IF(SMTHA.EQ.-1.) GO TO 168
CALL SMOOTH(ALPHA,SA,SMTHA,STNDVA,NVRTX)
168 CONTINUE
IF(SMTHD.EQ.-10) GO TO 169
CALL SMOOTH(DELTA,SD,SMTHD,STNDVD,NVRTX)
169 CONTINUE
END

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```

OVERLAY(MODEL,2,C)
PROGRAM MATASS
COMMON/IN/N(300)
COMMON/IRHS/RHS(200)
COMMON/IWCRK/VALP(4500)
COMMON/INT/INTP(4500)
COMMON/LSCOEFS/SA(4),SO(4)
COMMON/IALPHA/ALPHA(200)
COMMON/IDEPTH/DEPTH(200)
COMMON/IIP/IP(3,350)
COMMON/IA/A(3,3)
COMMON/IB/B(3)
COMMON/IY/Y(200)
COMMON/IX/X(200)
COMMON/NUMB/NVRTX,NTRI,IFILE,MASL,NEWBV
COMMON/HIND/TAUX,TAUY,CURL
COMMON/IALP/ALPH(3)
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IHEIGHT/HEIGHT(200)
COMMON/ICNST/CONST1,CONST2
COMMON/IGRAD/DALPHAX,DALPHAY,DDEPTHX,DDEPTHY,DEX,DEY,AREA
COMMON/CUTOFF/NIBP,NFLX,JJ1,JJ2
C WENCH PREPARE TO ASSEMBLE THE MATRIX BY SETTING IT TO ZERO
C ANDBY SETTING THE INTEGER BOOK KEEPING ARRAY TO ZERO.
C
IF(JJ1.EQ.-1) GO TO 199
IF(NEWBV.GT.1) GO TO 201
CALL SETMAT(NVRTX,IFILE,MASL)
C
C
C WENOW PROCEED TO CALCULATE GRADIENTS AND ASSEMBLE THE MATRIX
C
199 CONTINUE
CALL OVERLAY(5HMODEL,2,1,0)
C
201 CONTINUE
C
CALL OVERLAY(5HMODEL,2,2,0)
END

```



```

A(3,1)=X(M)
A(3,2)=Y(M)
A(1,3)=1.0
A(2,3)=1.0
A(3,3)=1.0
C
CALL TRIAREA(A, AREA)
AREA=ABS(AREA)
C
CALL GRAD(DEPTH(J),DEPTH(L),DEPTH(M),DDEPTHX,DDEPTHY,CDEPTH)
C
CALL ALPHX(K,CALPHAX,DALPHAY,ALPHA,SA,ALPH)
C
C
C
100 104 I=1,3
DO 102 II=1,3
102 B(II)=0.
B(I)=1.
C
CALL GRAD(B(1),B(2),B(3),DSHAPEX(I),DSHAPEY(I),CSHAPE(I))
C
C
104 CONTINUE
C
CALL MATRIX(DSHAPEX,DSHAPEY,K,NVRTX,NTRI,IFILE,MASL)
C
C
C
128 K=K+1
IF(K.GT.NTRI) GO TO 132
GO TO 72
C
132 CONTINUE
C
C
NONPROCEED TO AOO ON THE CONTRIBUTIONS FROM THE NO FLUX BOUNDARY
CONOITIONS*
C
C
CALL BASS(VALP,RHS)
C
C
HERE WE ADD THE PRESCRIBED BOUNDARY CONDITONS TO THE RIGHT HANO
SIDE.
C
CALL BC(NVRTX,NBV,IB,BV,MASL)
C
END

```

```

OVERLAY (MODEL,2,2)
PROGRAM SCLN
COMMON/NUMB/NVRTX,NTRI,IFILE,MASL,NEWBV
COMMON/INT/INTP(4500)
COMMON/IHEIGHT/HEIGHT(200)
COMMON/IHCRK/VALP(4500)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IRHS/RHS(200)
100 FORMAT(E12.5,020)
NR0W=NVRTX
NCOL=NVRTX
SMALL=.0000001
IF(NEWBV.GT.1) GO TO i
IF(IFILE)2,2,4
2 CONTINUE
C
c
c
HERE THE MATRIX IS DECOMPOSED.
CALL DCPK(NR0W,NCOL,IS,IR,IF,SMALL,INTP,VALP,MASL)
IF(IS.EQ.1) GO TO 10
IF(IFILE.EQ.0) GO TO i
c
c
c
OPTION TO CREATE FILE
11 "00 6 I=1,4500
WRITE(1,100)VALP(I),INTP(I)
6 CONTINUE
GO TO 1
C
C
C
OPTION TO REAC FROM FILE
4 00 a I=1,4500
JK=I-1
READ(1,100)VALP(I),INTP(I)
GO TO 1
8 CONTINUE
c
1 CONTINUE
c
C
c
WENOWADD THE BOUNDARY CONDITIONS IN. NOTE THEY MUST BEADDED
INTO VALP AFTER THE MATRIX HAS BEEN DECOMPOSED.
00 112 K=1,NRCW
VALP(K)=RHS(K)
112 CONTINUE
c
CALL SLVK(NR0W,NCOL,IE,INTP,VALP)
IF(IE.EQ.1) GO TO 12
GO TO 21
10 WRITE(6,15)
15 FORNAT(*0*,*SING IS 1, MATRIX IS SINGULAR*)
NVRTX=-NVRTX
GO TO 301
12 WRITE(6,20)

20 FORMAT(*0*,*ERROR IS 1, DIVISION BY ZERO IN SLVK*)
NVRTX=-NVRTX
GO TO 301
21 CONTINUE
00 22 I=1,NR0W
J=I+NR0W
22 HEIGHT(I)=VALP(J)
301 CONTINUE
ENO

```

```

OVERLAY (MODEL,4,0)
PROGRAM DRAW
COMMON/IRHS/RHS(200)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
COMMON/IX/XA(200)
COMMON/IY/YA(200)
COMMON/IIP/IP(3,350)
COMMON/NUMB/NVRTX,NTRI,IWHAT,IPUNCH,NEWBV
COMMON/IN/N(300)
COMMON/IHEIGHT/HEIGHT(200)
COMMON/CALCOMP/XXMAX,YYMAX,ISTART,NBC
DIMENSION CON(20)
DIMENSION TLABEL(3),X(200),Y(200)
c THIS SECTION IS FORCALCOMPLOTTIN
c THE UNIVERSITY OF WASHINGTON'S NUMERICAL PLOTTIN SYSTEM IS USED
c WE HAVE THE OPTION TO ORAH LABEL ANO CONTOUR EACH POINT AND TRIANGLE
XXMAX=XXMAXA
YYMAX=YYMAXA
DIM=(FO*USCALE*ALSCALE)*100./G

c
0 0 302 I=1,NVRTX
X(I)=XA(I)
Y(I)=YA(I)
302 CONTINUE
RATIO=XXMAX/YYMAX
YSIZE=6.
XSIZE=RATIO*YSIZE
XINC=XSIZE+.5
XSTART=.5
YSTART=2.
IF(IWHAT.EQ.1) GO TO 501
ENCODE(30,34,TLABEL)
34 FORMAT(27HTRIANGLES ANO GLOBAL LABELS)
CALL SETUP(ISTART,1,XSIZE,YSIZE,TLABEL,1,0.,XXMAX,0.,YYMAX,05,05,X
#START,YSTART)
CALL DRTRI(X,Y,IP,NTRI,2,N)
0 0 41 I=1,NVRTX
41 RHS(I)=FLCAT(I)
CALL ADVANC(0.,0.)
CALL TRILABL(X,Y,IP,NTRI,.112,1)
CALL ADVANC(0.,0.)
CALL VRTXLB(X,Y,RHS,0,NVRTX,.098,1)
IF(IWHAT)2,3,2
3 CALL ADVANC(XINC,0.)
2 CONTINUE
ISTART=1
IF(IWHAT.EQ.-1) GO TO 502
501 CONTINUE
ENCODE(30,33,TLABEL)
3 3 FORMAT(26HSURFACE ELEVATION CONTOURS)
CALL SETUP(ISTART,1,XSIZE,YSIZE,TLABEL,1,0.,XXMAX,0.,YYMAX,05,05,X
#START,YSTART)
00 9 I=1,NVRTX
HEIGHT(I)=HEIGHT(I)*DIM
9 CONTINUE
CALL KONTRI(X,Y,IP,CON,NTRI,NVRTX,8,HEIGHT,1)
CALL FLTBND(X,Y,IB,NBV,1)
CALL VRTXLB(X,Y,HEIGHT,1,NVRTX,.091,3)
404 CONTINUE
ISTART=1
502 IF(NEWBV.LT.NBC) GO TO 1990
CALL EXITPL
GO TO 1
1998 CALL ADVANC(XINC,0.)
1 CCNTINUE
END

```

```

OVERLAY (MODEL,5,0)
PROGRAM MESH

C
C
C   HERE WE GENERATE THE MESH.
C
COMMON/INCRK/P(204,2),VERT(402,6)
COMMON/INT/ISIDE(607,2),ITRI(403,3)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IIP/IP(3,350)
COMMON/NUMB/NVRTX,NTRI,LIST,NISP,NEHBV
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/CALCOMP/XXMAX,YYMAX,ISTART,NBC

C
DO 101 I=1,NVRTX
P(I,1)=X(I)
P(I,2)=Y(I)
101 CONTINUE
CALL TRIAN(ISIDE,ITRI)
DO 2 I=1,NTRI
IS1=ITRI(I,1)
IS2=ITRI(I,2)
JP1=ISIDE(IS1,1)
JP2=ISIDE(IS1,2)
JP3=ISIDE(IS2,1)
IF (.JP1.EQ.JP3.OR.JP2.EQ.JP3) JP3=ISIDE(IS2,2)
IP(1,I)=JP1
IP(2,I)=JP2
IP(3,I)=JP3
2 CONTINUE

C
END

```

```

OVERLAY (MCDEL,6,0)
PROGRAM OUTSIDE
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IIP/IP(3,350)
COMMON/NUMH/NVRTX,NTRI,LTRI,IPUNCH,NEWBV
COMMON/IHCRK/IBTRI(350)
COMMON/IX/X(200)
COMMON/IY/Y(200)

C
C
C
C
C
CALCULATE THE NUMBER OF POINTS IN EACH TRIANGLE AND ORDER THE
BOUNDARY POINTS. THE CODE IS AS FOLLOWS, THE VALUE OF IBTRI(K)
WILL TELL US HOW MANY BOUNDARY POINTS TRIANGLE #K# HAS.

5 FORMAT(*1*,*WE HAVE FOUND A BAD TRIANGLE WITH IBTRI GT 3 IN
HPROGRAM OUTSIDE, TRI=#,I4)
10 FORMAT(**,*THE GLOBAL LABELS ARE*,3I4)
15 FORMAT(*1*)
150 FORMAT(**,*THIS LISTING IS DONE AFTER WE HAVE ELIMINATED TRIANGLE
#S OUTSIDE OF OUR DOMAIN*)
30 FORMAT(*0*,*TRIANGLE NO. #,10X,*VERTEX 1*,10X,*VERTEX 2*,10X,*VERTE
*x 3*)
90 FORMAT(*0*)
35 FORMAT(* ● ,GX,I?,3X,13,14X913,15X, I3)
155 FORMAT(*1*,*PROGRAM IS TERMINATED BECAUSE OF FAULTY BOUNDARY TRIAN
GLE #,/, * ● 9*!;TR: WAS GREATER THAN 3*)
CALL FINDBP(IB,IIP,IBTRI,NTRI,NBV)

C
C
C
HERE WE HAVE THE OPTION TO ECHO CHECK THE BOUNDARY POINT SEQUENCES

DO 1 I=1,NTRI
IF (IBTRI(I).LT.4) GO TO 1
WRITE(6,5) I
WRITE(6,10) IP(1,I),IP(2,I),IP(3,I)
1 CONTINUE

C
C
C
HERE WE MAKE ONE FINAL CHECK OF OUR BOUNDARY TRIANGLES.
IF IBTRI IS GREATER THAN 3, THE PROGRAM IS KILLED.
● *W@*IT IS SUGGESTED THAT IBVCHK=1 UNTIL ONE GETS PAST THIS POINT.
THIS WILL ALLOW ONE TO FIND THE BAD TRIANGLES.

C
C
C
DO 68 I=1,NTRI
IF (IBTRI(I).GT.3) GO TO 911
68 CONTINUE
GO TO 281
911 WRITE(6,155)
GO TO 754
281 CONTINUE

C
C
C
THIS SECTION CHECKS TO SEE THAT ALL THE BOUNDARY TRIANGLES ARE
INSIDE THE DOMAIN

C
C
C
IF THERE ARE EXTRANEIOUS TRIANGLES OUTSIDE OF THE DOMAIN, THEY
WILL BE ELIMINATED AND NTRI WILL BE ADJUSTED ACCORDINGLY

CALL ELIM(IBTRI,IP,X,Y,NTRI)

C
C
754 CONTINUE
END

```

```

OVERLAY(MODEL,7,0)
PROGRAM TERM
COMMON/NUMB/NVRTX,NTRI,LIST, IPUNCH,NEWSV
COMMON/IHEIGHT/HEIGHT(200)
COMMON/ICNST/CONST1,CONST2
COMMON/LSCOEFS/SA(4),SD(4)
COMMON/IALPHA/ALPHA(200)
COMMON/IIP/IP(3,350)
COMMON/IA/A(3,3)
COMMON/IB/B(3)
COMMON/IDEPH/DEPTH(200)
COMMON/WIND/TAUX,TAUY,CURL
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IALP/ALP(3)
COMMON/IGRAD/DALPHAX,DALPHAY,DDEPTHX,DDEPTHY,DEX,DEY,AREA
WRITE(6,1)
1 FORMAT(*1*.*DYNAMIC BALANCE TERMS*)
WRITE(6,2)
2 FORMAT(*0*.*TRI*,8X,*BAROTROPIC TORQUE*,8X,*BAROCLINIC TORQUE*,7X,
/*CURL OF WIND*,5X,*BOTTOM FRICTION*)
DO 999 I=1,NTRI
J=IP(1,I)
K=IP(2,I)
L=IP(3,I)
A(1,1)=X(J)
A(1,2)=Y(J)
A(1,3)=1.0
A(2,1)=X(K)
A(2,2)=Y(K)
A(2,3)=1.0
A(3,1)=X(L)
A(3,2)=Y(L)
A(3,3)=1.0
CALL GRAD(DEPTH(J),DEPTH(K),DEPTH(L),DDEPTHX,DDEPTHY,CDEPTH)
CALL ALPHX(I,DALPHAX,DALPHAY,ALPHA,SA,ALP)
CALL GRAD(HEIGHT(J),HEIGHT(K),HEIGHT(L),DEX,DEY,CE)
CALL DYBALAN(BRT,BRC,CURL,BFRIC,CONST1)
WRITE(6,3)I,BRT,BRC,CURL,BFRIC
3 FORMAT(* *,I3,11X,F10.4,14X,F10.4,12X,F10.4,9X,F10.4)
999 CONTINUE
END

```

```

OVERLAY(MODEL,10,0)
PROGRAM GRID
COMMON/IN/N(300)
COMMON/IGRAD/XXMAX,YMAX,YMIN,RADIUS,XMIN,EXTRA(2)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/HEIGHT/HEIGHT(z00)
COMMON/IIP/IP(3,350)
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
COMMON/CALCCMP/XXMAX,YMAX,ISTART,NBC
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
DIMENSION ALAT(200),ALONG(200),LAT(200),LONG(200)
EQUIVALENCE(HEIGHT(1),LONG(1))
EQUIVALENCE(ALAT(1),Y(1))
EQUIVALENCE(ALONG(1),X(1))
EQUIVALENCE(IP(1,1),LAT(1))
CALL CARTSN(LAT,ALAT,LONG,ALONG,NVRTX,ALSCALE,XXMAX,YMAX,XMAX,YMA
AX,YMIN,X,Y,RADIUS,XMIN)
IPGRID=IPUNCH
THIS IS THE OPTION TO PUNCH THE COORDINATE OATA UP
c
c
IF(IPGRID.EQ.0) GO TO 152
WRITE(7,5)NVRTX
5 FORMAT(15I5)
DO 151 I=1,NVRTX
WRITE(7,195)X(I),Y(I),N(I)
195 FORMAT(F10.3,F10.3,5DX,*STA.*,2X,I3)
151 CONTINUE
WRITE(7,140)YMIN,YMAX,YMAX,XXMAX,RADIUS
140 FORMAT(7F10.2)
152 CONTINUE
END

```

```

OVERLAY(MODEL,11,0)
PROGRAM NRML
COMMON/IN/N(300)
COMMON/IALPHA/ALPHA(200)
COMMON/IDELTA/DELTA(200)
COMMON/IDEPH/DEPTH(200)
COMMON/WIND/TAUX,TAUY,CURL
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
CALL NORM(ALPHA,DELTA,DEPTH,TAUX,TAUY,CURL,NVRTX)
IPNORM=IPUNCH
250 FORMAT(F10.4,F15.4,F10.4,36X,*STA.*,1X,I3)
260 FORMAT(*WIND STRESS AND CURL VALUES*,3F10.4)
IF(IPNORM.EQ.0) GO TO 154
DO 153 I=1,NVRTX
WRITE(7,250)ALPHA(I),DELTA(I),DEPTH(I),N(I)
153 CONTINUE
WRITE(7,260)TAUX,TAUY,CURL
154 CONTINUE
END

```

```

OVERLAY(MODEL,12,0)
PROGRAM TRNS
COMMON/ICCNST/C1,C2
COMMON/IHEIGHT/HEIGHT(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPTRANS,NEHBV
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
COMMON/IIP/IP(3,350)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IALPHA/ALPHA(200)
COMMON/IDELTA/DELTA(200)
COMMON/IDEPH/DEPTH(200)
COMMON/IGRAD/DALPHAX,DALPHAY,DDEPTHX,DDEPTHY,DELEVX,DELEVY,AREA
COMMON/WIND/TX,TY,CURL
COMMON/LSCOEF/SA(4),SD(4)
COMMON/IA/A(3,3)
COMMON/IB/B(3)
COMMON/IALP/ALP(3)

```

```

C
C   SUBROUTINE TO CALCULATE TRANSPORTS AT CENTROID OF EACH TRIANGLE
C   CX AND CY ARE THE LOCATIONS OF TRIANGLE CENTERS
C   XTRANS AND YTRANS ARE THE TRANSPORTS IN THE X AND Y DIRECTIONS
C   TTRANS IS THE TOTAL TRANSPORT

```

```

C
C   WRITE(6,15)
15  FORMAT(*1*)
C   DIM=USCALE*DSCALE*0
C   WRITE(6,240)DIM
240  FORMAT(* *,*TRANSPORT SCALE FACTOR IS*,F8.3,1X,*CUBIC METERS PER S
      #SECOND PER SQUARE METER ASSUMING DENSITY IS ONE.*)
C   WRITE(6,230)
230  FORMAT(* *,*VELOCITY IS IN CENTIMETERS PER SECOND*,/)
C   WRITE(6,180)
180  FORMAT(* *,*TRIANGLE*,3X,*X-COOR*,4X,*Y-COOR*,7X,*X-TRANSP*,7X,*Y-
      #TRANS*,5X,*TOT. TRANSP*,5X,*DEPTH*,6X,*U-MEAN*,4X,*V-MEAN*,5X,*V T
      #OT*,/)

```

```

C
C   DO 100 I=1,NTRI
C   J=IP(1,I)
C   K=IP(2,I)
C   L=IP(3,I)

```

```

C
C   A(1,1)=X(J)
C   A(1,2)=Y(J)
C   A(1,3)=1.
C   A(2,1)=X(K)
C   A(2,2)=Y(K)
C   A(2,3)=1.0
C   A(3,1)=X(L)
C   A(3,2)=Y(L)
C   A(3,3)=1.
C   CALL GRAD(HEIGHT(J),HEIGHT(K),HEIGHT(L),DELEVX,DELEVY,CELEV)
C   CALL GRAD(DEPTH(J),DEPTH(K),DEPTH(L),DDEPTHX,DDEPTHY,CODEPTH)

```



```

      CALL ALPHX(I,DALPHAX,DALPHAY,ALPHA,SA,ALP)
C     DELTAGRADIENTSAREHANDLED LIKE THE ALPHA GRADIENTS
      CALL ALPHX(I,DDELTA,ODELTAY,DELTA,SO,ALP)
C
      CX=(X(J)+X(K)+X(L))/3.
      CY=(Y(J)+Y(K)+Y(L))/3.
C
      DEP=(DEPTH(J)+DEPTH(K)+DEPTH(L))/3.
C
      XTRANS=DELEVY*DEP-C1*ODELTAY+C2*(DELEVY-DELEVX)-C1*C2*(DALPHAX-DAL
      PHAY)+TY
C
      YTRANS=-(DELEVX*DEP)+C1*ODELTAX-C2*(DELEVY+DELEVX)-C1*C2*(DALPHAY+
      DALPHAX)-TX
C
      TRANS=(XTRANS*XTRANS+YTRANS*YTRANS)**.5
C
      DEP=-DEP*200.
      XTRANS=XTRANS*DIM
      YTRANS=YTRANS*DIM
      TRANS=TRANS*DIM
      U=XTRANS/DEP*100.
      V=YTRANS/DEP*100.
      VT=TRANS/DEP*100.
      WRITE(6,185)I,CX,CY,XTRANS,YTRANS,TRANS,DEP,U,V,VT
185 FORMAT(3X,I3,5X,F5.2,4X,F6.2,4X,F11.4,4X,F11.4,4X,F11.4,3X,F7.1,3X
      ,F3.4,2X,F9.4,2X,F9.4)
      IF(IPTTRANS.EQ.0)GO TO 100
      WRITE(7,260)XTRANS,YTRANS,TRANS,U,V,VT,I
260 FORMAT(6F10.3,10X,*TRANS*,2X,I3)
100 CONTINUE
101 CCNTINUE
      END

```

```

OVERLAY(MODEL,13,0)
PROGRAM VELO
COMMON/IHEIGHT/HEIGHT(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPVELO,NEWB
DIMENSION ALPH(3)
COMMON/IGRAD/DALPHAX,DALPHAY,DDEPTHX,DDEPTHY,DEX,DEY,AREA
COMMON/LSCOEF/SA(4),SD(4)
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO,EOOY
COMMON/IIP/IP(3,350)
COMMON/IA/A(3,3)
COMMON/IB/B(3)
COMMON/IALPHA/ALPHA(200)
COMMON/IDEPH/DEPTH(200)
COMMON/HIND/TAUX,TAUY,CURL
COMMON/IX/X(200)
COMMON/IY/Y(200)
WRITE(6,1)
1 FORMAT(*1*,*COMPARATIVE VELOCITIES INCH/SEC*)
WRITE(6,2)
2 FORMAT(*0*,16X,*EKMAN*,26X,*BAROTROPIC*,25X,*SURFACE*,26X,*BOTTOM*
*,/)
WRITE(6,4)
4 FORMAT(* *,*TRI*,5X,*U*,9X,*V*,7X,*TOTAL*,10X,*U*,9X,*V*,7X,*TOTAL
*,8X,* u *,5X,* v *,5X,*TOTAL*,10X,*U*,9X,*V*,7X,*TOTAL*,/)
C
00 999 K=1,NTRI
I=IP(1,K)
J=IP(2,K)
L=IP(3,K)
A(1,1)=X(I)
A(1,2)=Y(I)
A(1,3)=1.
A(2,1)=X(J)
A(2,2)=Y(J)
A(2,3)=1.
A(3,1)=X(L)
A(3,2)=Y(L)
A(3,3)=1.
C
CALL GRAD(DEPTH(I),DEPTH(J),DEPTH(L),DDEPTHX,CDEPTHY,CDEPTH)
CALL ALPHX(K,DALPHAX,CALPHAY,ALPHA,SA,ALPH)
CALL GRAD(HEIGHT(I),HEIGHT(J),HEIGHT(L),DEX,DEY,CE)
CALL EKMAN(UF,VE,TOTE)
CALL BAROT(UB,VB,TOTB)
CALL SURF(UF,VE,U2,VB,US,VS,TOTS)
CALL BOTT(UBOT,VBOT,TOTBOT)
WRITE(6,5)K,UF,VE,TOTE,UB,VB,TOTB,US,VS,TOTS,UBOT,VBOT,TOTBOT
5 FORMAT(* ● ,13,F8.3,2X,F8.3,2X,F8.3,5X,F8.3,2X,F8.3,2X,F8.3,5X,F8.3
*,2X,F8.3,2X,F8.3,5X,F8.3,2X,F8.3,2X,F8.3)
IF(IPVELO.EQ.0) GO TO 952
WRITE(7,105)K,US,VS,TOTS,UBOT,VBOT,TOTBOT
105 FORMAT(I5,6F10.3,2X,*VELOCITY*)
952 CONTINUE
999 CONTINUE
END

```

```

OVERLAY(MODEL,14,0)
PROGRAM BCHK

C
C
C
C
C
PROGRAM TO APPROXIMATE BOUNDARY CONDITIONS BY SOLVING
BOTTOM FRICTIONLESS CASE.

COMMON/EXTRA/XX(100),YY(100),OO(100)
COMMON/IGRAD/IFLG,IBEGIN,IEND,NIBP,NM
COMMON/IF/IF(3,350)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/ICNST/CONST1,CONST2
COMMON/IDPTH/DEPTH(200)
COMMON/IALPHA/ALPHA(200)
COMMON/BOUND/IB(75)●BV(75)NBV
COMMON/WIND/TAUX,TAUY,CURL
COMMON/NUMB/NVRTX,NTRI,NOINTG,IPINTG,NEWBV
COMMON/IA/A(3,3)
COMMON/IB/B(3)
COMMON/IN/N(300)
COMMON/CUTOFF/IBP,NFLX,J1,J2,DEEP
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
COMMON/LSCOEFS/SA(4),SD(4)
COMMON/IHEIGHT/XI(100),YI(100)
COMMON/IRHS/DST(100),EI(100)

C
ISLAND=IBP
NIBP=IBP
LANO=NFLX
ESCALE=FO*USCALE*ALSCALE*Q*100./G
IF(NEWBV.GT.1) GO TO 198
IF(NOINTG.EQ.0) GO TO 201

C
C
C
ENTER OVERLAY TO OBTAIN ELEVATION CHANGES ALONG OEPH CONTOURS*

CALL OVERLAY(5HMODEL,12,1)
GO TO 207
198 DO 199 I=1,NBV
    XI(I)=XX(I)
    YI(I)=YY(I)
199 EI(I)=BV(I)+OO(I)
    GO TO 207
201 DO 206 I=1,NBV
    J=IB(I)
    READ(5,200)X,N(J),XI(I),YI(I),DH
    XX(I)=XI(I)
    YY(I)=YI(I)
    DH=DH/ESCALE
    DO(I)=DH
206 EI(I)=BV(I)+DH
207 CONTINUE
    IBP=ISLAND
    NFLX=LANO

```

```

NIB?=ISLAND
C
C      RESULTS FROMSCLVER ARE LISTED HERE.
IF(NEWBV.GT.1) GO TO 203
CALL WHIN(DST)
C
WRITE(6,25)
DO 21 I=1,NBV
BVV=BV(I)*ESCALE
J=I2(I)
DH=0.
DP=DEPTH(J)*DSCALE
CALL BYPASS(I,IYES)
IF(IYES.EQ.1) GO TO 19
CALL WHCUT(DST, XI(I),YI(I),EDST)
EEI=EI(I)*ESCALE
DH=EEI-BVV
GO TO 121
19 EDST=0.0
EEI=BVV
121 IF(IPINTG,EQ.0) GO TO 202
WRITE(7,200) I,N(J),XI(I),YI(I),DH
202 CONTINUE
21 WRITE(5,30) I,J,N(J),BVV,DP,X(J),Y(J),DST(I),XI(I),YI(I),EDST,EEI,D
#H
203 CONTINUE
C
C      THIS IS WHERE THE BOUNDARY ELEVATIONS ARE ALTERED ACCORDING
C      TO THE RESULTS FROMSCLVER.
CALL ALTER(XI,YI)
C
C      THE NEW BOUNDARY ARE LISTED HERE.
WRITE(6,35)
DO 41 I=1,NBV
J=I2(I)
BVV=BV(I)*ESCALE
41 WRITE(6,40) I,J,N(J),BVV
C
C      HERE THE NEW BOUNDARY VALUES ARE PLOTTED UP AS A FUNCTION OF
C      DISTANCE ALONG THE BOUNDARY.
C
C      CALL OVERLAY(5HMODEL,12,2)
C
5 FCRMA?I3F10,2I
10 FORMAT(3I5,55X,*TRIA.*, 15)
15 FORMAT(I5,F10.2)
25 FORMAT(1H1,*BND.*,3X,*GLB.*,3X,*STA.*,4X,*ELEV.*,6X,*DEPTH*,5X,*EN
#TR. COOR. (DIST.)*,5X,*EXIT COOR. (DIST.)*,5X,*EXIT ELEV.*,5X,*ELEV.
#CHNG.*,/)
30 FORMAT(1H ,I3,3X,I4,3X, I3,5X,F6.2 ,4X,F6.0,5X,F5.2,* ,*,F5.2,*(*,F5.
#2,*),*,5X,F5.2,* ,*,F5.2,*(*,F5.2,*),*,5X,F8.4,7X,F8.4)
35 FORMAT(*1*,*BND. NO.*,5X,*GLB. NO.*,5X,*STA. NO.*,5X,*NEW ELEV.*,/
#)
40 FORMAT(* ,I5,8X,I5,8X,I5,8X,F9.4)
200 FORMAT(2I5, 2F10.3,2F10.4)
205 FORMAT(F10.4,15X,F10.4)
210 FORMAT(47X,F10.4)
215 FORMAT(F15.7)
220 FORMAT(11X,4F10.4)
305 FORMAT( 1X,F10.2SF1002,54X,I5 )
310 FORMAT(2F10.2)
END

```



```

SUBROUTINE NEWBVAL
C
C SUBROUTINE TO READ IN NEW BOUNDARY VALUES.
C
COMMON/IRHS/RHS(200)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
COMMON/HIND/TAUX,TAUY,CURL
COMMON/CUTOFF/NIBP,NFLX,NOMAT,JJ
ESCALE=G/(FO*USCALE*ALSCALE*Q*100.)
C
5 FORRAT(15,F10*4)
10 FORMAT(3F10.4)
C
READ (5,10)TAUX,TAUY,CURL
WSCL=FO*USCALE*DSCALE*Q*10000.
TAUX=TAUX/WSCL
TAUY=TAUY/WSCL
CURL=CURL/(WSCL*ALSCALE*100.)
C
C WE HAVE JUST READ IN NEW HIND STRESS VALUES
C
DO 1 I=1,NBV
READ(5,5)IBN,BV(I)
BV(I)=BV(I)*ESCALE
1 CONTINUE
C
C WE HAVE READ IN THE NEW BOUNDARY VALUES ALONG WITH THEIR BOUNDARY
C NUMBERS, THEN PROCEEDED TO NONDIMENSIONALIZED THEM.
C
C NOW RETURN TO REASSEMBLE THE RIGHT HANDED SIDE AND USE THE NEW
C BOUNDARY VALUES. THIS IS DONE BY SETTING NOMAT=-1.
C
JJ=1
C
RETURN
END

```

```

SUBROUTINE TRIAREA(A, AREA)
DIMENSION A(3,3)
AA=A(1,1)*A(2,2)*A(3,3)-A(2,3)*A(3,2)
BB=-A(1,2)*A(2,1)*A(3,3)-A(2,3)*A(3,1)
CC=A(1,3)*A(2,1)*A(3,2)-A(2,2)*A(3,1)
AREA=.5*(AA+BB+CC)
RETURN
END
132
134
136
138
140
142
144
145

```

SUBROUTINE SOLVE(A,B)	148
DIMENSION A(3,3),B(3),C(3),X(3)	150
CALL TRIAREA(A,AREA)	152
DO 2 J=1,3	154
DO 1 I=1,3	156
K=J-1	158
IF(J.NE.1) A(I,K)=C(I)	160
C(I)=A(I,J)	162
A(I,J)=B(I)	164
1 CONTINUE	166
CALL TRIAREA(A,X(J))	168
2 CONTINUE	172
A(1,3)=C(1)	174
A(2,3)=C(2)	175
A(3,3)=C(3)	178
B(1)=X(1)/AREA	180
B(2)=X(2)/AREA	182
B(3)=X(3)/AREA	184
8 RETURN	186
END	188

SUBROUTINE GRAD (E,F,G,DX,DY,C)	190
	192
SUBROUTINE TO CALCULATE GRADIENTS	194
E,F, AND G ARE THE VALUES TO BE FILLED INTO THE B VECTOR	196
DX,DY AND C ARE THE SOLUTIONS TO BE RETURNED	198
	200
COMMON/IA/A(3,3)	202
COMMON/IB/B(3)	204
B(1)=E	206
B(2)=F	208
B(3)=G	210
CALL SOLVE(A,B)	212
DX=B(1)	214
DY=B(2)	216
C=B(3)	218
RETURN	220
END	222

	SUBROUTINE BETA1(YMIN,YMAX,FO)
C	
C	
C	THIS SUBROUTINE CALCULATES THE MEAN CORICLIS VALUE FOR THE REGION
C	FO IS THE HEAN CORICLIS VALUE
C	
	OMEGA=.000072722052
C	
	DEG=YMIN
	FO=2.*(OMEGA)*SIN(DEG)
	DEG=YMAX
	FM=2.*(OMEGA)*SIN(DEG)
	FC=(FO+FM)/2.
	RETURN
	END

```

SUBROUTINE ALPHX(I,DALPHAX,DALPHAY,ALPHA,S,ALPH)
DIMENSION ALPH(3),ALPHA(1),S(1)
COMMON/IIP/IP(3,350)
COMMON/IDEPTH/DEPTH(200)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IA/A(3,3)
COMMON/IB/B(3)
C
C
C "SUBROUTINE TO GET ALPHA AND DELTA GRADIENTS BY USING A THIRD ORDER
C   LEAST SQUARES FIT TO THE ALPHA AND DELTA FIELDS.
C
C   J=IP(1,I)
C   K=IP(2,I)
C   L=IP(3,I)
C
C   RDEP=(DEPTH(J)+DEPTH(K)+DEPTH(L))/3.
C
C   CHECK TO SEE IF ALL THE DEPTHS ARE EQUAL
C
C   IF(DEPTH(J).EQ.DEPTH(K).AND.DEPTH(J).EQ.DEPTH(L)) GO TO 3
C   GO TO 4
3  RDEP=DEPTH(J)
C   ALPH(1)=ALPHA(J)
C   ALPH(2)=ALPHA(K)
C   ALPH(3)=ALPHA(L)
C   GO TO 5
4  CONTINUE
C
C   IF DEPTHS ARE NOT EQUAL, USE LSF FUNCTION TO GET ALPHA OR DELTA
C   AT REFERENCE DEPTH.
C
C   DO 1 M=1,3
C   N=IP(M,I)
C   D0=DEPTH(N)
C   DZ=RDEP-D0
C   D1=3.*S(1)*D0*D0+2.*S(2)*D0+S(3)
C   D2=6.*S(1)*D0+2.*S(2)
C   D3=6.*S(1)
C   ALPH(M)=ALPHA(N)+D1*DZ+D2*(DZ*DZ/2.)+D3*(DZ*DZ*DZ/6.)
1  CONTINUE
C
C   RESET A, THE POSITION MATRIX AND GET HORIZONTAL GRADIENTS
C
5  CONTINUE
C   A(1,1)=X(J)
C   A(1,2)=Y(J)
C   A(1,3)=1.
C   A(2,1)=X(K)
C   A(2,2)=Y(K)
C   A(2,3)=1.
C   A(3,1)=X(L)
C   A(3,2)=Y(L)
C   A(3,3)=1.
C
C   CALL GRAD(ALPH(1),ALPH(2),ALPH(3),DALPHAX,DALPHAY,CALPHA)
C   RETURN
C   END

```



```

SUBROUTINE INVR ( A, N, B, M, DETERM, ISIZE, JSIZE )
C
C NAME: INVR
C PURPOSE: LINEAR EQUATION SOLUTION (MATRIX INVERSION)
C ALGORITHM: GAUSS-JORDAN ELIMINATION, FULL PIVOT SEARCH.
C SEE ANY NUMERICAL ANALYSIS TEXT FOR REFERENCE.
C AUTHOR: ORIGINAL VERSION, CIRCA 1966, AUTHOR UNKNOWN.
C RECOPIED, 1976, RIK LITTLEFIELD (U.W.), WITH
C STYLISTIC CHANGES AND MINOR BUG CORRECTIONS (NO
C ALGORITHM OR CALLING SEQUENCE CHANGES)
C USAGE: SEE U, WASH. COMPUTING INFORMATION CENTER DOCUMENT
C NUMBER W00042 FOR FULL DESCRIPTION, BASICALLY,
C A = INPUT: COEFFICIENT MATRIX, LOGICALLY (N,N),
C PHYSICALLY (ISIZE,*). OUTPUT: A-INVERSE.
C e = INPUT: RIGHT-HAND SIDE, LOGICALLY (N,M),
C PHYSICALLY (ISIZE,*). OUTPUT: SOLUTION MATRIX.
C DETERM = DETERMINANT OF A, 0, IF A APPEARS SINGULAR.
C JSIZE = CURRENTLY UNUSED, ORIGINALLY 2ND DIM. OF A.
C LIMITS: (100,100) SYSTEM. CHANGE DIMENSION STATEMENTS FOR
C LARGER SYSTEMS.
C TIMING: ORDER (N**3). TYPICAL .4 TO .5 SECONDS FOR (20,20),
C M=0, USING *RUN* FORTRAN COMPILERS COC 6400.
C COMMENTS: THIS PARTICULAR IMPLEMENTATION OF THE ALGORITHM IS NOT
C THE BEST POSSIBLE - SEE ANY MATH SUBROUTINE LIBRARY
C (E.G., IMSL) FOR IMPROVED ROUTINES
C
REAL A(ISIZE,1), B(ISIZE,1)
INTEGER PIVOT(100), INOEX(100,2), J
INTEGER COLUMN, RCN
DO 10 J = 1,N
DETERM = 1.
10 PIVOT(J) = 0
DO 130 I = 1,N
C
C • +4 FULL SEARCH FOR PIVOT ELEMENT (BRANCH OUT IF NO NON-ZERO
C • +* PIVOT IS FOUND)
C
AHAX = 0.0
00 30 I1 = 1,N
IF ( PIVOT(I1).NE.0 ) GO TO 30
DO 20 J = 1,N
IF ( PIVOT(J).NE.0 ) GO TO 20
IF ( ABS(A(I1,J)) • LEQ AMAX ) GO TO 20
ROW = I1
COLUMN = J
AMAX = ABS(A(I1,J))
20 CONTINUE
30 CONTINUE
IF ( AHAX .EQ. 0.0 ) GO TO 200
PIVOT(COLUMN) = 1
C
C • VV INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL
C

```

	IF (ROH .EQ. COLUMN) GO TO GO	00630
	DETERM = -DETERM	00640
	DO 40 J = 1,N	00650
	SWAP = A(RCH,J)	00650
	A(ROH,J) = A(COLUMN,J)	00670
40	A(COLUMN,J) = SWAP	00630
	IF (M.LE.0) GO TO 60	00690
	DO 50 J = 1,M	00700
	SWAP = B(ROH,J)	013710
	B(ROH,J) = B(COLUMN,J)	00720
50	B(COLUMN,J) = SWAP	00730
60	INDEX(I,1) = RCH	00740
	INDEX(I,2) = COLUMN	00750
	PVTELM = A(COLUMN,COLUMN)	00760
	DETERM = DETERM*PVTELM	00770
C		00780
C	*** NORMALIZE PIVCT ROW (DIVIDE BY PIVOT ELEMENT)	00790
C		00800
	A(COLUMN,COLUMN) = 1.0	00810
	DO 70 J = 1,N	00820
70	A(COLUMN,J) = A(COLUMN,J)/PVTELM	00830
	IF (M.LE.0) GO TO 90	00840
	DO 80 J = 1,M	00850
80	B(COLUMN,J) = B(COLUMN,J)/PVTELM	00860
C		00870
C	*** REDUCE NON-PIVOT ROWS	00880
C		00890
90	DO 120 I1 = 1,N	00900
	IF (I1.EQ.COLUMN) GO TO 120	00910
	T = A(I1,COLUMN)	00920
	A(I1,COLUMN) = 0.0	00930
	DO 100 J = 1,N	00940
100	A(I1,J) = A(I1,J) - A(COLUMN,J)*T	00950
	IF (M.LE.0) GO TO 120	00960
	DO 110 J = 1,M	00970
110	B(I1,J) = B(I1,J) - B(COLUMN,J)*T	00980
120	CONTINUE	00990
130	CONTINUE	01000
C		01010
C	*** Elimination DONE, INTERCHANGE COLUMNS TO COMPLETE INVERSE	01020
C		01030
	DO 150 J = 1,N	01040
	L = N+1-J	01050
	IF (INDEX(L,1).EQ.INDEX(L,2)) GO TO 150	01060
	ROW = INDEX(L,1)	01070
	COLUMN = INDEX(L,2)	01080
	DO 140 I = 1,N	01090
	SWAP = A(I,ROW)	01100
140	A(I,ROW) = A(I,COLUMN)	01110
	A(I,COLUMN) = SWAP	01120
150	CONTINUE	01130
C	RETURN	01140
C		01150
C	*** SINGULAR MATRIX - ERROR EXIT	01160
C		01170
	200 DETERM = 000	01180
	RETURN	
	ENO	01200

```

SUBROUTINE SMOOTH(VAL,S,D,SD,NPTS)
COMMON/IOPTH/DEP(200)
DIMENSION VAL(1),S(1)

C
C
C
SUBROUTINE TO SMOOTH THE DATA ACCORDING TO LEAST SQUARES FIT,
DO 1 I=1,NPTS
V=S(1)*DEP(I)+DEP(I)*DEP(I)+S(2)*DEP(I)+DEP(I)+S(3)*DEP(I)+S(4)
DD=VAL(I)-V
IF(DD.LT.-D) DD=-D*SD
IF(DD.GT.D) DD=D*SD
VAL(I)=DD+V
1 CONTINUE
RETURN
END

SUBROUTINE SETMAT(NVRTX,IFILE,MASL)
COMMON/IWCRK/VALP(4500)
COMMON/INT/INTP(4500)
COMMON/IRHS/RHS(200)

C
C
C
THIS SUBROUTINE SETS THE MATRIX AND RIGHT HAND SIDE TO O OPERATE

IF(IFILE.EQ.1) GO TO 15
00 99 I=1,4500
VALP(I)=0.
99 INTP(I)=0
15 00 16 I=1,200
16 RHS(I)=0.
17 CONTINUE
NROW=NVRTX
NCOL=NVRTX
MSZ=4500

C
C
C
HERE HE TELL THE SOLVING ROUTINE THAT WE ARE READY

CALL MINIT(INTP,NROW,NCOL,MSZ,MASL)
RETURN
ENO

SUBROUTINE NORM(ALPHA,DELTA,DEPTH,TAUX,TAUY,CURL,NVRTX)
COMMON/SCALES/USCALE,DSCALE,ALSCALE,G,E,D,SAMHA,FO,EDDY
DIMENSION ALPHA(1),DELTA(1),DEPTH(1)
●**V*
C
C
C
SUBROUTINE USED FOR NORMALIZATION OF STATION DATA
C
C
C
ALPHA IS DENSITY INTEGRATE VERTICALLY (GM/CM**3)*M
C
C
C
DELTA IS ALPHA INTEGRATED VERTICALLY (GM/CM**3)*M**2
C
C
C
DEPTH IS CEPTH(M)
C
C
C
TAUX AND TAUY ARE HIND STRESS VALUES IN THE X AND Y DIRECTION
C
C
C
WIND STRESS UNITS ARE DYNES/CM*CM
C
C
C
DSCALE IS THE DEPTH SCALE (M)
C
C
C
USCALE IS THE HORIZONTAL VELOCITY SCALE (M/SEC)
C
C
C
FO IS THE AVERAGE CORIOLIS PARAMETER
C
C
C
Q AND E ARE THE MEAN AND PERTURBATION DENSITY RESPECTIVELY
C
C
C
NVRTX IS THE NUMBER OF STATIONS
C
C
C
●**+***
C
C
C
TO CALCULATE SCALE FACTORS
C
C
C
ALPH=E*DSCALE
C
C
C
DELT=ALPH*DSCALE
C
C
C
0 0 12 I=1,NVRTX
C
C
C
ALPHA(I)=(ALPHA(I)+DEPTH(I)*Q)/ALPH
C
C
C
DELTA(I)=(DELTA(I)-(DEPTH(I)*DEPTH(I)*Q)/2.)/DELT
C
C
C
DEPTH(I)=DEPTH(I)/DSCALE
C
C
C
12 CONTINUE
C
C
C
STRESS=FO*USCALE*DSCALE*10000.*Q
C
C
C
TAUX=TAUX/STRESS
C
C
C
TAUY=TAUY/STRESS
C
C
C
STRESS=STRESS/(100.*ALSCALE)
C
C
C
CURL=CURL/STRESS
C
C
C
RETURN
C
C
C
ENO

```

```

SUBROUTINE CARTSN(LAT,ALAT,LONG,ALONG,NVRTX,ALSCALE,XXMAX,YYMAX,XH
v AX, YMAX, YMIN, X, Y, RADIUS, XMIN)
DIMENSION LAT(1),ALAT(1),LONG(1),ALONG(1),X(1),Y(1)
CALL RADIANS(NVRTX,LAT,ALAT,LONG,ALONG,YMIN,XMIN,YMAX,AVEL,X,Y)
CALL MERCTR(X,Y,ALSCALE,NVRTX,XMIN,YMIN,AVEL,RADIUS)
YYMAX=0.
XXMAX=0.
DO 18 I=1,NVRTX
YYMAX=AMAX1(YYMAX,Y(I))
XXMAX=AMAX1(XXMAX,X(I))
1.8 CONTINUE
RETURN
END

```

```

SUBROUTINE RADIANS(NVRTX,LAT,ALAT,LONG,ALONG,YMIN,XMIN,YMAX,AVEL,X
v ,Y)
THIS SUBRCUTINE CONVERTS OEGREES LATITUDE ANDLONGTUDE INTO
RADIANS. IT ALSO RETURNS THEMIMUMLATIDUDE TO BE USED AS THE
Y=0 REFERENCE AND THE MAXIMUM LONGITUDE(H) TO BE USEO AS THE X=0
REFERENCE. THE AVERAGE LATITUDE IS ALSO RETURNED.

```

```

DIMENSION LAT(1),LONG(1),ALAT(1),ALONG(1),X(1),Y(1)
RADIAN=3.141492654/180.
AVEL=0.
DO 1 I=1,NVRTX
DEG=ALAT(I)/60.
ALAT(I)=FLOAT(LAT(I))+DEG
ALAT(I)=ALAT(I)*RADIAN
AVEL=AVEL+ALAT(I)
DEG=ALONG(I)/60.
ALONG(I)=FLOAT(LONG(I))+DEG
1 ALONG(I)=ALONG(I)*RADIAN
AVEL=AVEL/FLOAT(NVRTX)
YMIN=ALAT(1)
XMIN=ALONG(1)
YMAX=ALAT(1)
DO 2 I=2,NVRTX
YMIN=AMIN1(YMIN,ALAT(I))
XMIN=AMAX1(XMIN,ALONG(I))
2 YMAX=AMAX1(YMAX,ALAT(I))
RETURN
END

```

```

SUBROUTINE MERCTR(X,Y,ALSCALE,NVRTX,XMIN,YMIN,AVEL,RADIUS)
THIS Subroutine DOES THE MERCATOR TRANSFORMATION. THE DISTANCES
ARE SCALED BY THE LENGTH SCALE(ALSCALE) AND THE AVERAGE DISTORTION
FACTOR SUCH THAT THE UNIT LENGTH IN X AND Y IS APPROXIMATELY ONE
HORIZONTAL LENGTH SCALE.

```

```

DIMENSION X(1),Y(1)
RADIUS=6378000./ALSCALE*COS(AVEL)
XSHIFT=XMIN*RADIUS
ARG=YMIN/2.+0.7853982
ARG=TAN(ARG)
YSHIFT=RADIUS*ALOG(ARG)
DO 1 I=1,NVRTX
X(I)=-{RADIUS*X(I)-XSHIFT}
Y(I)=RADIUS*ALOG(TAN(Y(I)/2.+0.7853982))-YSHIFT
1 CONTINUE
RETURN
END

```

```

SUBROUTINE HESH
C
C
C   HERE WE GENERATE THE MESH.
COMMON/IWCRK/P(204,2),VERT(402,6)
COMMON/INT/ISIDE(607,2),ITRI(403,3)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IIP/IP(3,350)
COMMON/NUMB/NVRTX,NTRI,LIST,NIBP,NEWBV
COMMON/BOUND/IS(75),BV(75),NBV
COMMON/CALCOMP/XXMAX,YYMAX,ISTART,NBC
C
  0  0  101 I=1,NVRTX
  P(I,1)=X(I)
  P(I,2)=Y(I)
101 CONTINUE
  CALL TRIAN
  DO 2 I=1,NTRI
  IS1=ITRI(I,1)
  IS2=ITRI(I,2)
  IS3=ITRI(I,3)
  JP1=ISIDE(IS1,1)
  JP2=ISIDE(IS1,2)
  JP3=ISIDE(IS2,1)
  IF(JP1.EQ.JP3.OR.JP2.EQ.JP3) JP3=ISIDE(IS2,2)
  IP(1,I)=JP1
  IP(2,I)=JP2
  IP(3,I)=JP3
  2 CONTINUE
C
  RETURN
  END

SUBROUTINE TRIAN
C
C   THE INFORMATION NEED TO RUN THE PROGRAM IS AS FOLLOWS,
C   AN INTEGER ARRAY T WHICH KEEPS TRACK OF WHAT THREE SIDES EACH
C   TRIANGLE HAS. THIS MUST BE A NTRI BY 3 ARRAY WHERE NTRI IS
C   THE MAXIMUM NUMBER OF TRIANGLES EXPECTED.
C   AN INTEGER ARRAY, S, WHICH RECORDS THE ENDPOINTS OF EACH LINE.
C   THIS MUST BE AN NSIDE BY 2 ARRAY WHERE NSIDE IS THE MAXIMUM
C   NUMBER OF SIDES ONE EXPECTS.
C   NP, THE NUMBER OF POINTS ONE HAS,
C   NIBP, THE NUMBER OF INTERIOR BOUNDARY POINTS,
C   A REAL ARRAY, P, WHICH CONTAINS THE X AND Y COORDINATES OF EACH
C   POINT. THE X COORDINATE GOES INTO THE P(NP,1) POSITION
C   AND THE Y COORDINATE GOES INTO THE P(NP,2) POSITION.
C   THEREFORE P IS AN NP BY 2 ARRAY WHERE NP IS THE NUMBER OF
C   POINTS.
C   ALSO NEED ARE TWO WORKING ARRAYS, VERT(NT,3) AND IS(3)
C   VERT WILL STORE THE COORDINATES OF EACH VERTEX OF EACH
C   TRIANGLES AS THEY ARE GENERATED. IS WILL CONTAIN THE SIDES.
C   *****NOTE*****
C   IF INTERIOR BOUNDARY POINTS ARE ENTERED (ISLAND), THEN THEY MUST
C   BE THE FIRST DATA CARDS READ IN AND THEY MUST BE READ IN
C   CLOCK WISE ORDER.
C   THE EXTERIOR BOUNDARY STATION NUMBERS ARE READ IN AFTER THE
C   X AND Y COORDINATES OF EACH STATION HAS BEEN ENTERED, AND
C   THE EXTERIOR BOUNDARY STATION S ARE READ IN COUNTERCLOCK
C   WISE ORDER.
C
  INTEGER S,T
  DIMENSION IS(3)
  COMMON/IWCRK/P(204,2),VERT(402,6)
  COMMON/INT/S(607,2),T(403,3)
  COMMON/NUMB/NP,NT,LIST,NIBP,NEWBV
  COMMON/CALCOMP/XMAX,YMAX,ISTART,NBC
  COMMON/BOUND/IB(75),BV(75),NBV
C

```

```

C THE FIRST STEP IS TO FIND THE MAXIMUM DOMAIN COVERED BY THE POINTS
XMIN=0.
YMIN=0.
C
IF(XMIN.NE.XMAX) GO TO 101
XMAX=P(1,1)
XMIN=XMAX
YMAX=P(1,2)
YMIN=YMAX
DO 1 I=2,NP
IF(P(I,1).GT.XMAX)XMAX=P(I,1)
IF(P(I,1).LT.XMIN)XMIN=P(I,1)
IF(P(I,2).GT.YMAX)YMAX=P(I,2)
IF(P(I,2).LT.YMIN)YMIN=P(I,2)
1 CONTINUE
101 CONTINUE
C
NOW THE OUTER LIMITS ARE SET,
C
DX=(XMAX-XMIN)*.1
DY=(YMAX-YMIN)*.1
P(201,1)=XMIN-DX
P(201,2)=YMIN-DY
P(202,1)=XMAX+DX
P(202,2)=P(201,1)
P(203,1)=P(202,1)
P(203,2)=YMAX+DY
P(204,1)=P(201,1)
P(204,2)=P(203,2)
C
C NOW THE INITIAL POINT OF REAL DATA IS USED TO FORM THE FIRST
C EIGHT SIDES AND FOUR TRIANGLES,
C
S(1,1)=201
S(1,2)=202
S(2,1)=202
S(2,2)=203
S(3,1)=203
S(3,2)=204
S(4,1)=204
S(4,2)=201
S(5,1)=201
S(5,2)=1
S(6,1)=202
S(6,2)=1
S(7,1)=203
S(7,2)=1
S(8,1)=204
S(8,2)=1
T(1,1)=1
T(1,2)=5
T(1,3)=6
T(2,1)=6
T(2,2)=7
T(2,3)=2
T(3,1)=3
T(3,2)=7
T(3,3)=8
T(4,1)=4
T(4,2)=5
T(4,3)=8
NS=8
NT=4
C
C THIS FILLS IN THE INITIAL VERTICES OF THE TRIANGLES
C
C NOW PROCEED TO LABEL THE X AND Y COORDINATES OF THE TRIANGLES
C
00 Z I=1,4
2 CALL LOADVER(VERT,P,S,T,I)

```

```

C
C THE Retaining POINTS ARE NOW ADDED ONE BY ONE
C
DO 6 I=2,NP
X=P(I,1)
Y=P(I,2)
C X AND Y BECOME THE NEXT POINT TO BE ADDED TO THE MESH
C NOW PROCEED TO FIND OUT WHAT TRIANGLE X AND Y ARE IN
C
IFLAG=0
CALL INSIDE(VERT,X,Y,NT,ITRI)
C ITRI IS NOW THE TRIANGLE THAT CONTAINS THE POINT I.
C
IF(ITRI.EQ.-2) GO TO 6
IF(ITRI.NE.0) GO TO 102
WRITE(6,200)I
200 FORMAT(*0*,*POINT*,I5,* IS NOT IN DOMAIN*)
GO TO 6
102 CONTINUE
C
C HERE, THE NEW TRIANGLES AND SEGMENTS ARE ADDED.
C WE BEGIN BY LABELING THE SIDES AND VERTICES OF THE FIRST TRIANGLE,
C
IS1=T(ITRI,1)
IS2=T(ITRI,2)
IS3=T(ITRI,3)
IP1=S(IS2,2)
IF(S(IS2,1).NE.S(IS1,1).AND.S(IS2,1).NE.S(IS1,2)) IP1=S(IS2,1)
IP2=S(IS1,2)
IF(S(IS1,1).NE.S(IS2,1).AND.S(IS1,1).NE.S(IS2,2)) IP2=S(IS1,1)
IP3=S(IS1,2)
IF(IP3.EQ.IP2) IP3=S(IS1,1)
C
C NOW THE NEW LINE SEGMENTS ARE GENERATED.
C
S(NS+1,1)=IP1
S(NS+1,2)=I
S(NS+2,1)=IP2
S(NS+2,2)=I
S(NS+3,1)=IP3
S(NS+3,2)=I
C
C NOW THE NEW TRIANGLES ARE CREATED
C
T(ITRI,1)=IS1
T(ITRI,2)=NS+2
T(ITRI,3)=NS+3
T(NT+1,1)=IS2
T(NT+1,2)=NS+1
T(NT+1,3)=NS+3
T(NT+2,1)=IS3
T(NT+2,2)=NS+1
T(NT+2,3)=NS+2
C
C NOW THE VERTICES OF THE NEW TRIANGLES ARE LOCATED.
C
CALL LOADVER(VERT,P,S,T,ITRI)
II=NT+1
CALL LOADVER(VERT,P,S,T,II)
II=NT+2
CALL LOADVER(VERT,P,S,T,II)
C
C NOW THE NUMBER OF TRIANGLES AND THE NUMBER OF LINES ARE UPDATED.
C
NT=NT+2
NS=NS+3
C

```

```

C     NOW THE TRIANGLES THAT SHARE SIDES,IS1,IS2, AND IS3 ARE EACH
C     CHECKED FOR POTENTIAL REORIENTATION,
C
      IS(1)=IS1
      IS(2)=IS2
      IS(3)=IS3
      DO 5 J=1,3
C     HERE TO FIND TWO NEIGHBORING TRIANGLES.
C
      CALL NEIG(IS(J),T,JT1,JT2,NT)
C
C     NOW TO ORDER THE PAIR OF TRIANGLES.
C
      IF(JT2.EQ.0) GO TO 5
      JS1=IS(J)
      JP1=S(JS1,1)
      JP2=S(JS1,2)
C
      DO 3 K=1,3
      JST1=T(JT1,K)
      JST2=T(JT2,K)
      IF(S(JST1,1).EQ.JP1.AND.S(JST1,2).NE.JP2) JS2=JST1
      IF(S(JST1,2).EQ.JP1.AND.S(JST1,1).NE.JP2) JS2=JST1
      IF(S(JST1,1).EQ.JP2.AND.S(JST1,2).NE.JP1) JS3=JST1
      IF(S(JST1,2).EQ.JP2.AND.S(JST1,1).NE.JP1) JS3=JST1
      IF(S(JST2,1).EQ.JP1.AND.S(JST2,2).NE.JP2) JS4=JST2
      IF(S(JST2,2).EQ.JP1.AND.S(JST2,1).NE.JP2) JS4=JST2
      IF(S(JST2,1).EQ.JP2.AND.S(JST2,2).NE.JP1) JS5=JST2
      IF(S(JST2,2).EQ.JP2.AND.S(JST2,1).NE.JP1) JS5=JST2
3     CONTINUE
C
      JP3=S(JS3,1)
      IF(JP3.EQ.JP2) JP3=S(JS3,2)
      JP4=S(JS5,1)
      IF(JP4.EQ.JP2) JP4=S(JS5,2)
C
C
C
C     THE TRIANGLES ARE NOW CHECKED TO SEE IF THEY FORM
C     A CONVEX REGION.
C
      X1=P(JP4,1)
      Y1=P(JP4,2)
      X2=P(JP3,1)
      Y2=P(JP3,2)
      X3=P(JP1,1)
      Y3=P(JP1,2)
      X=P(JP2,1)
      Y=P(JP2,2)
      CALL INNER(X1,Y1,X2,Y2,X3,Y3,X,Y,IC)
      IF(IC.EQ.1) GO TO 5
      X3=X
      Y3=Y
      X=P(JP1,1)
      Y=P(JP1,2)
      CALL INNER(X1,Y1,X2,Y2,X3,Y3,X,Y,IC)
      IF(IC.EQ.1) GO TO 5
C

```



```

%      NOW CHECK FOR BOUNDARY SEGMENTS
c
IF(JP3.GT.200.OR.JP4.GT.200) GO TO 5
IF(JP1.GT.200.OR.JP2.GT.200) GO TO 4
00 307 KJ=1,NBV
K1=IB(KJ)
IF(JP1.NE.K1.AND.JP2.NE.K1) GO TO 307
IMORE=KJ+1
ILESS=KJ-1
IF(ILESS.EQ.0) GO TO 331
ILESS=IB(ILESS)
IF(JP1.EQ.ILESS.OR.JP2.EQ.ILESS) GO TO 5
331 CONTINUE
IF(IMORE.GT.NBV) GO TO 332
IMORE=IB(IMORE)
IF(JP1.EQ.IMORE.OR.JP2.EQ.IMORE) GO TO 5
GO TO 308
332 CONTINUE
307 CONTINUE
308 DO 309 KJ=1,NBV
K1=IB(KJ)
IF(JP3.NE.K1.AND.JP4.NE.K1) GO TO 309
IMORE=KJ+1
ILESS=KJ-1
IF(ILESS.EQ.0) GO TO 431
ILESS=IB(ILESS)
IF(JP3.EQ.ILESS.OR.JP4.EQ. ILESS) GO TO 4
431 CONTINUE
IF(IMORE.GT.NBV) GO TO 432
IMORE=IB(IMORE)
IF(JP3.EQ.IMORE.OR.JP4.EQ. IMORE) GO TO 4
GO TO 311
432 CONTINUE

```

```

c      IN THIS SECTION, THE FLAGGED TRIANGLES ARE ELIMINATED AND THE
c      LIST COMPACTED. THE ACTUAL NUMBER OF TRIANGLES REMAINING IS
c      RETURNED AS NT.

```

```

T(NT+1,1)=0
ITOP=NT+1
IBEGIN=1
17 DO 10 I=IBEGIN,ITOP
IF(T(I,1).NE.0) GO TO 10
GO TO 16
10 CONTINUE
16 NEXT=I+1
DO 9 J=NEXT,ITOP
9 IF(T(J,1).NE.0) GO TO 13
GO TO 18
13 INTV=J-I
ITOP=ITOP-INTV
DO 14 K=I,ITOP
L=K+INTV
DO 15 M=1,3
15 T(K,M)=T(L,M)
14 CONTINUE
IBEGIN=I+1
GO TO 17
18 CONTINUE
DO 11 I=1,NT
IF(T(I,1).EQ.0) GO TO 12
11 CONTINUE
12 NT=I-1
RETURN
END

```

```

SUBROUTINE LOADVER(VERT,P,S,T,I)
INTEGER S(607,2),T(403,3)
INTEGER P1,P2,P3,S1,S2
DIMENSION VERT(402,6),P(204,2)
S1=T(I,1)
S2=T(I,2)
P1=S(S1,1)
P2=S(S1,2)
P3=S(S2,1)
IF(P3.EQ.P1.OR.P3.EQ.P2) P3=S(S2,2)
VERT(I,1)=P(P1,1)
VERT(I,2)=P(P2,1)
VERT(I,3)=P(P3,1)
VERT(I,4)=P(P1,2)
VERT(I,5)=P(P2,2)
VERT(I,6)=P(P3,2)
RETURN
END

```

```

SUBROUTINE INNER(X1,Y1,X2,Y2,X3,Y3, X,Y,IC)
DIMENSION A(3,3)
CALL LOAD(A,X1,Y1,X2,Y2,X3,Y3)
CALL TRIAREA(A,AREA)
IF(AREA.EQ.0.) GO TO 8
CALL LOAD(A,X,Y,X2,Y2,X3,Y3)
CALL TRIAREA(A,AREA1)
CALL LOAD(A,X1,Y1,X,Y,X3,Y3)
CALL TRIAREA(A,AREA2)
AREA1=AREA1/AREA
IF(AREA1.LT.0.) GO TO 10
IF(AREA1.EQ.1) GO TO 9
AREA2=AREA2/AREA
IF(AREA2.LT.0.) GO TO 10
IF(AREA2.EQ.1) GO TO 9
AREA3=1.-AREA1-AEA2
IF(AREA3.LT.0.) GO TO 10
IF(AREA3.EQ.1) GO TO 9
IC=1
RETURN
10 IC=0
RETURN
9 CONTINUE
IF(X1.EQ.X) GO TO 11
IF(X2.EQ.X) GO TO 12
IF(X3.EQ.X) GO TO 13
GO TO 10
11 IF(Y1.EQ.Y) GO TO 14
GO TO 10
12 IF(Y2.EQ.Y) GO TO 14
GO TO 10
13 IF(Y3.EQ.Y) GO TO 14
GO TO 10
14 IC=-1
RETURN
8 CONTINUE
IC=2
RETURN
END

```

```

SUBROUTINE INSIDE (VERT,X,Y,NT,IPTRI)
DIMENSION VERT(402,6)
DO 1 I=1,NT
IF (AMIN1 (VERT (I,1),VERT (I,2),VERT (I,3)).GT.X) GO TO 1
IF (AMAX1 (VERT (I,1),VERT (I,2),VERT (I,3)).LT.X) GO TO 1
IF (AMIN1 (VERT (I,4),VERT (I,5),VERT (I,6)).GT.Y) GO TO 1
IF (AMAX1 (VERT (I,4),VERT (I,5),VERT (I,6)).LT.Y) GO TO 1
CALL INNER (VERT (I,1),VERT (I,4),VERT (I,2),VERT (I,5),VERT (I,3),VERT (
vI,6),X,Y,IC)
IF (IC.EQ.1) GO TO 2
IF (IC.EQ.-1) GO TO 3
IF (IC.EQ.2) GO TO 4
1 CONTINUE
WRITE (6,5) X,Y
5 FORMAT (*0*,*POINT*,2F8.2,2X,*NOT IN ANY TRIANGLE*)
IPTRI=0
RETURN
2 IPTRI=I
RETURN
3 IPTRI=-2
WRITE (6,10) X,Y,I
10 FORMAT (*0*,*WE HAVE A DUPLICATE POINT*,2F8.2,15)
RETURN
4 IPTRI=I
RETURN
END

```

```

SUBROUTINE LOAD (A,X1,Y1,X2,Y2,X3,Y3)
DIMENSION A (3,3)
A (1,1)=X1
A (1,2)=Y1
A (1,3)=1.
A (2,1)=X2
A (2,2)=Y2
A (2,3)=1.
A (3,1)=X3
A (3,2)=Y3
A (3,3)=1.
RETURN
ENO
SUBROUTINE CHKA (ITRI,VERT,IFLAG)
DIMENSION VERT (402,6),A (3,3)
X1=VERT (ITRI,1)
X2=VERT (ITRI,2)
X3=VERT (ITRI,3)
Y1=VERT (ITRI,4)
Y2=VERT (ITRI,5)
Y3=VERT (ITRI,6)
CALL LOAD (A,X1,Y1,X2,Y2,X3,Y3)
CALL TRIAREA (A,AREA)
IF (AREA.EQ.0.) GO TO 1
IFLAG=0
RETURN
1 IFLAG=1
RETURN
END

```

```

SUBROUTINE SWEEP(P,S,T,NT,ITIME,NIBP)
C
C THIS SUBROUTINE SWEEPS THROUGH THE TRIANGLES AND COMPARES
C NEIGHBCRS FOR GOODNESS.
C
C P IS THE POINT ARRAY AS DESCRIBED IN TRIAN.
C S IS THE SIDE ARRAY AS DESCRIBED IN TRIAN.
C T IS THE TRIANGLE ARRAY AS DESCRIBED IN TRIAN.
C ITIME IS A COUNTER TELLING US HOW MANY TRIANGLES HAVE BEEN CHANGED
C NIBP IS THE NUMBER OF INTERIOR BOUNDARY POINTS*
C
C INTEGER S(607,2),T(403,3)
C COMMON/BOUND/IB(75),BV(75),NBV
C DIMENSION P(204,2)
C ITIME=0
C
C HERE THE SWEEP BEGINS,
C
C DO 100 I=1,NT
C   DO 2 J=1,3
C
C BEGIN BY EXAMINING THE J SIDE OF TRIANGLE I
C   IS=T(I,J)
C
C HERE WE LOCATE THE TWO NEIGHBORING TRIANGLES THAT HAVE SIDE ISO
C
C CALL NEIG(IS,T,JT1,JT2,NT)
C IF(JT2.EQ.0) GO TO 2
C
C PROCEED TO CODE THE POINTS OF THE NEIGHBORING TRIANGLES.
C
C   JP1=S(IS,1)
C   JP2=S(IS,2)
C   IS1=T(JT1,1)
C   IF(IS.EQ.IS1) IS1=T(JT1,2)
C   JP3=S(IS1,1)
C   IF(JP3.EQ.JP2.OR.JP3.EQ.JP1) JP3=S(IS1,2)
C   IS1=T(JT2,1)
C   IF(IS.EQ.IS1) IS1=T(JT2,2)
C   JP4=S(IS1,1)
C   IF(JP4.EQ.JP2.OR.JP4.EQ.JP1) JP4=S(IS1,2)
C
C NOW CHECK FOR CONVEX TRIANGLES*
C
C   X1=P(JP4,1)
C   Y1=P(JP4,2)
C   X2=P(JP3,1)
C   Y2=P(JP3,2)
C   X3=P(JP1,1)
C   Y3=P(JP1,2)
C   X=P(JP2,1)
C   Y=P(JP2,2)

```

```

C      CALL INNER(X1,Y1,X2,Y2,X3,Y3,X,Y,IC)
      IF(IC.EQ.1) GO TO 2
      X3=X
      Y3=Y
      X=P(JP1,1)
      Y=P(JP1,2)

C      CALL INNER(X1,Y1,X2,Y2,X3,Y3,X,Y,IC)
      IF(IC.EQ.1) GO TO 2

C      C
      C      NOW CHECK FOR BOUNDPRY SEGMENTS
      C
      IF(JP3.GT.200.OR.JP4.GT.200) GO TO 2
      IF(JP1.GT.200.OR.JP2.GT.200) GO TO 4

C      DO 307 KJ=1,NBV
      K1=IB(KJ)
      IF(JP1.NE.K1.AND.JP2.NE.K1) GO TO 307
      ILESS=KJ-1
      IMORE=KJ+1
      IF(ILESS.EQ.0) GO TO 331
      ILESS=IB(ILESS)
      IF(JP1.EQ.ILESS.C?.JP2.EQ.ILESS) GO TO 2
331 CONTINUE
      IF(IMORE.GT.NBV) GO TO 332
      IMORE=IB(IMORE)
      IF(JP1.EQ.IMORE.C?.JP2.EQ.IMORE) GO TO 2
      GO TO 308.
332 CONTINUE
307 CONTINUE
308 DO 309 KJ=1,NBV
      K1=IB(KJ)
      IF(JP3.NE.K1.AND.JP4.NE.K1) GO TO 309
      ILESS=KJ-1
      IMORE=KJ+1
      IF(ILESS.EQ.0) GO TO 431
      ILESS=IB(ILESS)
      IF(JP3.EQ.ILESS.OR.JP4.EQ.ILESS) GO TO 4
431 CONTINUE
      IF(IMORE.GT.NBV) GO TO 432
      IMORE=IB(IMORE)
      IF(JP3.EQ.IMORE.OR.JP4.EQ.IMORE) GO TO 4
      GO TO 311
432 CONTINUE
309 CONTINUE
311 CONTINUE

C      C
      C      NOW PROCEED TO CALCULATE AND COMPARE THE GOODNESS OF THE
      C      NEIGHBORING TRIANGLES.
      C
      G1=GOOD(JP1,JP2,JP3,P)

```

```

G2=GOOD(JP1,JP2,JP4,P)
G3=GOOD(JP1,JP3,JP4,P)
G4=GOOD(JP2,JP3,JP4,P)
GH=AMIN1(G3,G4)
IF(G1.LT.GH) GO TO 4
IF(G2.LT.GH) GO TO 4
GO TO 2
4 CONTINUE

C
C THIS IS WHERE THE SWITCHING OF THE TRIANGLES ARE DONE.
C WE BEGIN BY LABELING THE SIDES FOR IDENTIFICATION.
C
JS1=IS
S(JS1,1)=JP4
S(JS1,2)=JP3
DO 200 K=1,3
JST1=T(JT1,K)
JST2=T(JT2,K)
IF(S(JST1,1).EQ.JP1.AND.S(JST1,2).NE.JP2) JS2=JST1
IF(S(JST1,2).EQ.JP1.AND.S(JST1,1).NE.JP2) JS2=JST1
IF(S(JST1,1).EQ.JP2.AND.S(JST1,2).NE.JP1) JS3=JST1
IF(S(JST1,2).EQ.JP2.AND.S(JST1,1).NE.JP1) JS3=JST1
IF(S(JST2,1).EQ.JP1.AND.S(JST2,2).NE.JP2) JS4=JST2
IF(S(JST2,2).EQ.JP1.AND.S(JST2,1).NE.JP2) JS4=JST2
IF(S(JST2,1).EQ.JP2.AND.S(JST2,2).NE.JP1) JS5=JST2
IF(S(JST2,2).EQ.JP2.AND.S(JST2,1).NE.JP1) JS5=JST2
200 CONTINUE

C
C NOW THE TRIANGLES ARE ALTERED.
C AND THE CHANGES RECORDED.
C
T(JT1,1)=JS1
T(JT1,2)=JS2
T(JT1,3)=JS4
T(JT2,1)=JS1
T(JT2,2)=JS3
T(JT2,3)=JS5
ITIME=ITIME+1
GO TO 100
2 CONTINUE
100 CONTINUE
RETURN
ENO

SUBROUTINE FINDBP(IB,IP,IBTRI,NTRI,NBV)
DIMENSION IB(1),IP(3,1),IBTRI(1)
C THIS SUBROUTINE CALCULATES THE NUMBER OF POINTS IN EACH TRIANGLE
C AND ORDERS THE BOUNDARY POINTS.
DO 1601 MN=1,NTRI
1601 IBTRI(MN)=0
1)0 622 K=1,NBV
00 622 J=1,NTRI

DO 621 I=1,3
IF(IB(K).NE.IP(I,J)) GO TO 621
IBTRI(J)=IBTRI(J)+1
I2=IBTRI(J)
NUM=IP(I2,J)
IP(I2,J)=IP(I,J)
IP(I,J)=NUM
GO TO 622
621 CONTINUE
622 CONTINUE

```

C THIS SECTION CHECKS TO SEE IF THE BOUNDARY TRIANGLES AND NUMBERING
 C SYSTEM ARE CONSISTENT
 C

```

DO 633 J=1,NTRI
NUM=IBTRI(J)-2
IF(NUM)633,634,643
634 DO 637 K=1,NBV
IF(IB(K).NE.IP(1,J)) GO TO b37
IJ=K+1
IF(IB(IJ).EQ.IP(2,J)) GO TO 633
IF(IP(1,J).EQ.IB(1).AND.IP(2,J).EQ.IB(NBV)) GO TO 641
DO 734 M=IJ,NBV
IF(IB(M).EQ.IP(2,J)) GO TO 758
GO TO 734
758 IBTRI(J)=0
GO TO b33
734 CONTINUE
DO 736 M=1,NBV
IF(IB(M).EQ.IP(3,J)) GO TO b40
736 CONTINUE
GO TO 635
641 CONTINUE
NUM=IP(1,J)
IP(1,J)=IP(2,J)
IP(2,J)=NUM
GO TO 633
637 CONTINUE
635 IBTRI(J)=5

```

C
 C IBTRI(J)=5 INDICATES THAT NO BOUNDARY POINTS WERE FOUND IN THE
 C TRIANGLE EVEN THOUGH IBTRI HAS OVER 2 ORIGINALLY
 C

```

FUNCTION GOOD(JP1,JP2,JP3,P)
DIMENSION AL(3),P(204,2)
DIMENSION X(2),Y(2)
X(1)=P(JP1,1)
X(2)=P(JP2,1)
Y(1)=P(JP1,2)
Y(2)=P(JP2,2)
AL(1)=ALENGTH(X,Y)
X(2)=P(JP3,1)
Y(2)=P(JP3,2)
AL(2)=ALENGTH(X,Y)
X(1)=P(JP2,1)
Y(1)=P(JP2,2)
AL(3)=ALENGTH(X,Y)
ALM=AL(1)
I=1
DO 2 J=2,3
IF(AL(J).GT.ALM) GO TO 1
GO TO 2
1 I=J
ALM=AL(J)
2 CONTINUE
RLL=0.
DO 3 J=1,3
IF(J.NE.I) RLL=RLL+AL(J)
3 CONTINUE
GOCC=RLL/ALM
RETL=ALM
END

```

```

SUBROUTINE ELIM(IBTRI,IP,X,Y,NTRI)
DIMENSION IBTRI(1),IP(3,1),X(1),Y(1)
COMMON/IA/A(3,3)
COMMON/IB/B(3)
COMMON/INT/ISUM(300),IPROD(300)
C
C THIS SUBROUTINE ELIMINATES TRIANGLES OUTSIDE OF THE DOMAIN
C
DO 662 J=1,NTRI
IF(IBTRI(J).LT.2) GO TO 662
663 NN=IP(1,J)
M=IP(2,J)
L=IP(3,J)
664 DX=X(M)-X(NN)
DY=Y(M)-Y(NN)
DS=((DX**2.)+(DY**2.))**.5
DCOSX=DY/DS
DCOSY=-DX/DS
666 A(1,1)=X(L)
A(1,2)=Y(L)
A(1,3)=1.
A(2,1)=X(NN)
A(2,2)=Y(NN)
A(2,3)=1.
A(3,1)=X(M)
A(3,2)=Y(M)
A(3,3)=1.
B(1)=1.
B(2)=J.
B(3)=J.
CALL SOLVE(A,B)
667 DX=X(NN)+0.5*DX+0.01*DS*DCOSX
DY=Y(NN)+0.5*DY+0.1*DS*DCOSY
DS=B(1)*DX+B(2)*DY+B(3)
IF(DS.LT.0) GO TO 662
IBTRI(J)=6
662 CONTINUE
I=NTRI
262 DO 674 J=1,NTRI
IF(IBTRI(J).NE.6) GO TO 674
272 IF(J.EQ.I) GO TO 677
I=I-1
DO 676 K=J,I
L=K+1
IBTRI(K)=IBTRI(L)
IP(1,K)=IP(1,L)
IP(2,K)=IP(2,L)
676 IP(3,K)=IP(3,L)
IBTRI(NTRI)=0
IF(IBTRI(J).EQ.6) GO TO 272
674 CONTINUE
677 NTRI=I+1
DO 802 I=1,NTRI

GO TO 633
643 00 649 K=1,NBV
IF(IB(K).NE.IP(1,J)) GO TO 649
IJ=K+1
IF(IB(IJ).EQ.IP(2,J)) GO TO 651
KK=NBV-1
IF(IP(1,J).EQ.IB(KK).AND.IP(2,J).EQ.IB(KK)) GO TO 735
00 737 M=IJ,NBV
737 IF(IB(M).EQ.IP(2,J)) GO TO 651
GO TO 635

```



```

735 CONTINUE
    IJ=NBV-1
    IF (IB(IJ).NE.IP(2,J)) GO TO 640
    IF (IB(NBV).NE.IP(3,J)) GO TO 640
    NUM=IP(1,J)
    IP(1,J)=IP(2,J)
    IP(2,J)=IP(3,J)
    IP(3,J)=NUM
649 CONTINUE
    GO TO 633
651 IJ=K+2
    IF (IB(1).EQ.IP(3,J)) GO TO 633
    IF (IB(IJ).EQ.IP(3,J)) GO TO 633
    IF (IP(1,J).EQ.IB(1).AND.IP(3,J).EQ.IB(NBV)) GO TO 739
    DO 852 M=IJ,NBV
852 IF (IS(M).EQ.IP(3,J)) GO TO 743
    GO TO 635
743 IBTRI(J)=3
    GO TO 633
739 IF (IB(NBV).NE.IP(3,J)) GO TO 640
    NUM=IP(1,J)
    IP(1,J)=IP(3,J)
    IP(3,J)=IP(2,J)
    IP(2,J)=NUM
    GO TO 633
640 IBTRI(J)=4
c
633 CONTINUE
c
r   IBTRI(J)=4 INDICATES THAT THE BOUNDARY POINTS WERE NOT IN SEQUENCE
    RETURN
    END

```

```

SUBROUTINE BYPASS(I,IYES)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/CUTOFF/NIBP,NFLX,JJ1,JJ2,DEEP
COMMON/DEPTH/DEPTH(200)
IYES=0
J=IB(I)
IF (DEPTH(J).LE.DEEP) IYES=1
NF=NF+FLX+NIBP
IF (I.LE.NF) IYES=1
RETURN
END

```

```

    ISUM(I)=IP(1,J)+IP(2,J)+IP(3,J)
802 IPROD(I)=IP(1,J)*IP(2,J) ● IP(3,J)
    ICOUNT=0
807 IEND=NTRI-ICOUNT
    DO 804 I=1,IEND
    IF (ISUM(I).NE.ISUM(IEND)) GO TO 804
    IF (IPROD(I).NE.IPROD(IEND)) GO TO 804
    IF (I.EQ.IEND) GO TO 804
    ICOUNT=ICOUNT+1
    GO TO 807
804 CONTINUE
    NTRI=NTRI-ICOUNT
    RETURN
    END

```

```

SUBROUTINE WHOUT(DST,X1,Y1,EDST)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IX/X(200)
COMMON/IY/Y(200)
DIMENSION DST(1)
CALL WHERE(X1,Y1,J1,J2)
I2=IB(J1)
ADD=((X(I2)-X1)**2.+(Y(I2)-Y1)**2.)**.5
EDST=DST(J1)+ADD
RETURN
END

```

```

SUBROUTINE WHIN(DST)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IX/X(200)
COMMON/IY/Y(200)
DIMENSION DST(1)
DST(1)=0.
DO 9 I=2,NBV
J=IB(I)
L=I-1
K=IB(L)
DT=((X(K)-X(J))**2.+(Y(K)-Y(J))**2.)**.5
9 DST(I)=DST(L)+DT
RETURN
END

```

```

SUBROUTINE GUESS(X1SY1OJ1,JZ,ELEV)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
I1=IB(J1)
I2=IB(J2)
DS1=((X(I1)-X1)**2.+(Y(I1)-Y1)**2.)**.5
DS2=((X(I2)-X1)**2.+(Y(I2)-Y1)**2.)**.5
DS=DS1+DS2
ELEV=(DS2/DS)*BV(J1)+(DS1/DS)*BV(J2)
RETURN
END

```

```

SUBROUTINE ALTER(XI,YI)

```

C
C
C

THIS ROUTINE ALTERS THE OLD BOUNDARY CONDITIONS.

```

COMMON/IRHS/DST(100),EI(100)
COMMON/IDEPTH/DEPTH(200)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
COMMON/CUTCOFF/NIBP,NFLX,J1,J2
DIMENSION XI(1),YI(1)
DO 10 I=1,NBV
CALL BYPASS(I,IYES)
IF(IYES.EQ.1) GO TO 10
9 DH=EI(I)-BV(I)
CALL WHOUT(DST,XI(I),YI(I),EDST)
IF(EDST.LT.DST(I)) GO TO 10
8 CALL WHERE(XI(I),YI(I),J1,J2)
CALL GUESS(XI(I),YI(I),J1,J2,ELEV)
BV(I)=ELEV-DH
10 CONTINUE
RETURN
END

```

```

Subroutine BTH(X1,X2,Y1,Y2,X,Y,IYES)
IF(AMAX1(X1,X2).LT.X) GO TO 1
IF(AMIN1(X1,X2).GT.X) GO TO 1
IF(AMAX1(Y1,Y2).LT.Y) GO TO 1
IF(AMIN1(Y1,Y2).GT.Y) GO TO 1
IYES=1
RETURN
1 IYES=0
RETURN
ENO

```

```

SUBROUTINE WHERE(X1,Y1,J1,J2)
COMMON/IGRAD/IFLG,IBEGIN,IEND,NIBP,HH
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
I=NIBP+1
I1=IB(I)
I=IB(NBV)
CALL BTH(X(I),X(I1),Y(I),Y(I1),X1,Y1,IYES)
IF(IYES.NE.1) GO TO 1
J1=NBV
J2=NIBP+1
RETURN
1 ISTCP=NBV-1
00 2 I=1,ISTOP
J=I+1
K1=IB(I)
K2=IB(J)
CALL BTH(X(K1),X(K2),Y(K1),Y(K2),X1,Y1,IYES)
IF(IYES.EQ.0.) GO TO 2
J1=I
J2=J
RETURN
2 CONTINUE
WRITE(6,10)X1,Y1
10 FORMAT(*0*,2F10.2,3X,*NOT ON BOUNDARY*)
RETURN
END

```

```

SUBROUTINE INTG(X1,Y1,X2,Y2,ELEV1,ELEV2,I TRI,SA,OP)
DIMENSION SA(1)
COMMON/IALPHA/ALPHA(200)
COMMON/HIND/TAUX,TAUY,CURL
COMMON/ICNST/CONST1,CONST2
COMMON/IIP/IP(3,350)
IF(X1.EQ.X2.AND.Y1.EQ.Y2) GO TO 1
DS=((X1-X2)**2+(Y1-Y2)**2)**.5
C A L L JACOB(I TRI,DDX,DDY,AJ,SA)
CALL DDON(X1,Y1,X2,Y2,DDX,DDY,DN)
IF(ABS(DN).LT..000001) GO TO 2
ELEV2=(CONST1*AJ+CURL)*DS/DN+ELEV1
RETURN
1 ELEV2=0.
RETURN
2 ELEV2=ELEV1
WRITE(6,10) I TRI
10 FORMAT(1H0,*WE HAVE RUN INTO A TRIANGLE WITH NO DEPTHGRADIENTS*,2
CX,I3)
RETURN
END

```

```

SUBROUTINE SOLVER(ELEV1,X1,Y1,ELEV2,X2,Y2,IGLB,SA)
C
C   THIS IS THE ROUTINE THAT SOLVES THE FIRST ORDER EQUATION.
C
COMMON/CUTOFF/IFINIS,NFLX,J1,J2
COMMON/IGRAD/IFLG,IBEGIN,IEND,NIBP,IDONE
COMMON/IDPTH/DEPTH(200)
COMMON/NUMB/NVRTX,NTRI,NOINTG,IPINTG,NEWBV
DIMENSION SA(1)
DP=DEPTH(IGLB)
IFINIS=0
IEND=0
IBEGIN=0
IFLG=0
IDONE=0
C
C   BEGIN BY LOCATING THE FIRST TRIANGLE WE WILL WORK WITH.
C
CALL FIRST(IGLB,ITRI,0)
IF(ITRI.NE.0) GO TO 1
X2=X1
Y2=Y1
ELEV2=ELEV1
RETURN
C
C   NOW FIND THE POINT ALONG THE TRIANGLE BOUNDARY WHICH HAS THE
C   SAME DEPTH AS THE POINT WE CAME FROM.
C
1 CALL FNDPT(X1,Y1,ITRI,X2,Y2,DP)
C
C   NOW INTEGRATE FROM THE ORIGINAL POINT TO THE SECOND POINT
C   WITHIN THE TRIANGLE.
C
CALL INTG(X1,Y1,X2,Y2,ELEV1,ELEV2,ITRI,SA,DP)
ELEV1=ELEV2
IENC=IEND+1
IF(IEND.EQ.NTRI) GO TO 7
C
C   NOW LOCATE THE NEXT TRIANGLE THE DEPTH CONTOUR ENTERS,
C   THEN GO BACK TO ONE AND FIND THE SECOND POINT AGAIN.
C
CALL EXTEND(X2,Y2,ITRI,NEWTRI)
IF(NEWTRI.EQ.0) RETURN
5 X1=X2
Y1=Y2
ITRI=NEWTRI
GO TO 1
:
7,WRITE(6,100)OP
100FORMAT(1H0,*WE ARE LOST FOLLOWING*,1X,F6.2,1X,*DEPTH CONTOUR-)
RETURN
END

```

```

SUBROUTINE BETW(VAL,VAL1,VAL2,IYES)
COMMON/IGRAD/IFLG,IBEGIN,IEND,NN,NM
IFLG=0
IYES=0
IF(VAL.LE.VAL1.AND.VAL.GE.VAL2) GO TO 1
IF(VAL.GE.VAL1.AND.VAL.LE.VAL2) GO TO 1
RETURN
1 IYES=1
IF(VAL.EQ.VAL1) IFLG=1
IF(VAL.EQ.VAL2) IFLG=1
RETURN
ENO

```

```

SUBROUTINE FIRST(IGLB,ITRI,IOLD)
COMMON/CUTOFF/IFINIS,NFLX,IP1,IP2
COMMON/IGRAD/IFLG,IBEGIN,IEND,NIBP,IDONE
COMMON/IIP/IP(3,350)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IDPTH/DEPTH(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
DO 2 I=1,NTRI
IF(I,EQ,IOLD) GO TO 2
IF(I,EQ,IFINIS) GO TO 2
IF(I,EQ,IDONE) GO TO 2
DO 1 J=1,3
K=IP(J,I)
IF(IGLB,EQ,K) GO TO 3
1 CONTINUE
GO TO 2
3 CONTINUE
I1=IP(1,I)
I2=IP(2,I)
I3=IP(3,I)
IF(IGLB,EQ,I1) GO TO 4
IF(IGLB,EQ,I2) GO TO 5
IF(IGLB,EQ,I3) GO TO 6
IF(IGLB,EQ,I1) GO TO 4
IF(IGLB,EQ,I2) GO TO 5
IF(IGLB,EQ,I3) GO TO 6
CALL BETH(DEPTH(IGLB),DEPTH(I1),DEPTH(I2),IYES)
IF(IYES,EQ,1) GO TO 6
GO TO 2
5 CONTINUE
IF(IGLB,EQ,I1) GO TO 4
IF(IGLB,EQ,I3) GO TO 6
CALL BETH(DEPTH(IGLB),DEPTH(I1),DEPTH(I3),IYES)
IF(IYES,EQ,1) GO TO 6
GO TO 2
4 CONTINUE
IF(IGLB,EQ,I2) GO TO 5
IF(IGLB,EQ,I3) GO TO 6
CALL BETH(DEPTH(IGLB),DEPTH(I2),DEPTH(I3),IYES)
IF(IYES,EQ,1) GO TO 6
GO TO 2
8 IBEGIN=0
2 CONTINUE
ITRI=0
RETURN
6 ITRI=1
IF(IFLG,EQ,0) GO TO 7
IBEGIN=IGLB
RETURN
7 IBEGIN=0
RETURN
ENO

```

```

SUBROUTINE VERTCH(X1,Y1,IOLD,IYES,IGLB)
COMMON/BOUND/IB(75),BV(75),NBV
COMMON/IIF/IP(3,350)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
IF(IOLD.LT.0) IOLD=-IOLD
00 1 I=1,3
K=IP(I,IOLD)
DX=X1-X(K)
DY=Y1-Y(K)
DS=(DX*DX+DY*DY)●-.5
IF(DS.LT..00000001) GO TO 2
1 CONTINUE
IYES=0
RETURN
2 IYES=1
DO 3 I=1,NBV
J=IB(I)
IF(J.EQ.K) GO TO 4
3 CONTINUE
IGLB=K
RETURN
4 IGLB=0
RETURN
END

```

```

SUBROUTINE EXTEND(X1,Y1,IOLD,NEWTRI)
COMMON/IIF/IP(3,350)
COMMON/IGRAD/IFLG,IBEGIN,IEND,NIBP,IDCNE
COMMON/CUTOFF/IFINIS,NFLX,J1,J2
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEWBV
CALL VERTCH(X1,Y1,IOLD,IYES,IGLB)
IF(IYES.EQ.1) GO TO 7
DO 5 I=1,NTRI
IF(I.EQ.IOLD) GO TO 5
DO 4 J=1,2
K=IP(J,I)
IF(K.NE.J1.AND.K.NE.J2) GO TO 4
JJ=J+1
DO 3 L=JJ,3
K=IP(L,I)
IF(K.NE.J1.AND.K.NE.J2) GO TO 3
NEWTRI=I
RETURN
3 CONTINUE
4 CONTINUE
5 CONTINUE
6 NEWTRI=0
RETURN
7 IF(IGLB.EQ.0) GO TO 6
RECCRD WHENCE WE CAME.
IFINIS=IOLD
CALL FIRST(IGLB,NEWTRI,IOLD)
RECCRD TO WHERE WE TREK.
IDONE=NEWTRI
RETURN
END

```

```

SUBROUTINE DDCN(X1,Y1,X2,Y2,DDX,DDY ● ON)
DX=X2-X1
DY=Y2-Y1
DS=(DX*DX+DY*DY)**.5
DN=CX/DS*CDY-GY/DS*CDX
RETURN
END

```

```

SUBROUTINE JACOB(ITRI,DOX,DDY,AJ,SA)
COMMON/IALPHA/ALPHA(200)
COMMON/IDEPTH/DEPTH(200)
COMMON/IIP/IP(3,350)
DIMENSION SA(1)
DIMENSION ALPH(3)
COMMON/IA/A(3,3)
I1=IP(1,ITRI)
I2=IP(2,ITRI)
I3=IP(3,ITRI)
CALL FILL(ITRI,A)
CALL ALPHX(ITRI,DAX,DAY,ALPHA,SA,ALPH)
CALL GRAD(DEPTH(I1),DEPTH(I2),DEPTH(I3),DOX,DDY,CC)
AJ=DAY*DDX-DAX*DDY
RETURN
END

```

```

SUBROUTINE INTERS(OP,X2,Y2,X1,Y1)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IIP/IP(3,350)
COMMON/IDEPTH/DEPTH(200)
COMMON/CUTOFF/NIBP,NFLX,IP1,IP2
D1=DEPTH(IP1)
D2=DEPTH(IP2)
DS1=D1-OP
DS2=D2-OP
DS=D2-D1
W1=DS2/DS
W2=DS1/DS
IF(D1.NE.D2) GO TO 15
X2=X(IP2)
Y2=Y(IP2)
IF(X2.NE.X1.AND.Y2.NE.Y1) GO TO 20
X2=X(IP1)
Y2=Y(IP1)
20 RETURN
15 CONTINUE
X2=X(IP1)*W1+X(IP2)*W2
Y2=Y(IP1)*W1+Y(IP2)*W2
RETURN
END

```

```

SUBROUTINE FNDPT(X1,Y1,ITRI,X2,Y2,DP)
COMMON/IX/X(200)
COMMON/IY/Y(200)
COMMON/IF/IP(3,350)
COMMON/IDEPH/DEPTH(200)
COMMON/NUMB/NVRTX,NTRI,LIST,IPUNCH,NEHBV
COMMON/CUTOFF/NIBP,NFLX,IP1,IP2
IFLG=0
I1=IP(1,ITRI)
I2=IP(2,ITRI)
I3=IP(3,ITRI)
DO 10 I=1,3
IF(I.EQ.1) GO TO 9
IF(I.EQ.2) GO TO 8
IP1=I2
IP2=I3
CALL BETH(DP,DEPTH(IP1),DEPTH(IP2),IYES)
IF(IYES.EQ.0) GO TO 10
GO TO 7
9 IP1=I1
IP2=I2
CALL BETH(DP,DEPTH(IP1),DEPTH(IP2),IYES)
IF(IYES.EQ.0) GO TO 10
GO TO 7
8 IP1=I1
IP2=I3
CALL BETH(DP,DEPTH(IP1),DEPTH(IP2),IYES)
IF(IYES.EQ.0) GO TO 10
7 CALL INTERS(DP,X2,Y2,X1,Y1)
DX=(X1-X2)**2.
DY=(Y1-Y2)**2.
IF(DX.LT.1.0E-13.AND.DY.LT.1.0E-13) GO TO 10
RETURN
10 CONTINUE
WRITE(6,50)ITRI,X1,Y1,DP
50 FORMAT(*0*,*WE ARE LOST IN TRI.*,I5,2X,*FROM POINT*,2F7.3,2X,*DEPT
vH*,F6.3)
IFLG=1000
RETURN
ENO

```



```

SUBROUTINE PLOT(X,Y,NPTS,XSTRT,XSIZE,YSIZE,NOIV,NFL,NDEC,YMAX)
DIMENSION A(120),IX(200),IY(200),SYM(5),FRHT(3),TLAB(3),SB(30)
DIMENSION X(1),Y(1)
DATA SYM/1H ,1H*,1H0,1H-,1HX,1HI/

C
C
C AN ALL PURPOSE PRINTER PLOT ROUTINE WRITTEN IN STANDARD FORTRAN.
C
C X AND Y ARE COORDINATES OF POINTS TO BE PLOTTED,
C NPTS ARE NUMBER OF POINTS TO BE PLOTTED.
C XSIZE IS THE SIZE OF THE PLOT IN INCHES IN THE X DIRECTION.
C LIKEWISE FOR YSIZE.
C XSTRT IS THE VALUE OF THE MINIMUM X VALUE.
C NOIV IS THE NUMBER OF PARTITIONS THE X AXIS WILL BE DIVIDED INTO
C AND LABELED.
C NFL IS THE FIELD LENGTH OF THE LABEL IN F FORMAT.
C NDEC IS THE NUMBER OF DECIMAL POINTS THERE WILL BE IN THE FIELD
C LENGTH.
C YMAX IS CALCULATE,
C
C CALL SCALE(X,Y,IX,IY,NPTS,XSIZE,YSIZE,YPTS,XMIN,XMAX,XPTS,YMAX)
C
C JX=IFIX(XSTRT/.1)
C IYPTS=IFIX(YPTS)
C IXPTS=IFIX(XPTS)
C IXTCT=IXPTS+JX
C NSKP=JX-NFL-1
C
C TOP LABEL.
C
C NCHR=23
C ENCOUE(23,105,TLA8)
105 FORMAT(23HNEW BOUNDARY ELEVATIONS)
C CALL TLB(TL#8,NCHR,IXPTS,JX)
C
C SIDELABEL SET IN SUBROUTINE SLB.
C CALL SLB(SB,IS,IE,IYPTS)
C
C ENCOOE(ZI,100,FRHT)NSKP,NFL,NDEC
100 FORMAT(5H(1H ,I2,4HA1,F,I1,1H.,I1,7H,110A1})
DO 6 I=1,JX
6 A(I)=SYM(1)
DO 1 I=JX,110
1 A(I)=SYM(4)
WRITE(6,5)(A(I),I=1,110)
5 FORMAT(1H ,110A1)
IC=1
DO 3 I=1,IYPTS
DO 2 IJ=1,110
2 A(IJ)=SYM(1)
IF(I.LT.IS.OR.I.GT.IE) GO TO 13
A(1)=SB(IC)

```

```

SUBROUTINE TOP (NDIV, XMIN, XMAX, A, NFL, NDEC, ISTRT, NXPTS)
DIMENSION A(1), FRMT(3)
MRKS=NDIV+1
AINT=(XMAX-XMIN)/FLOAT(NDIV)
DO 1 I=1, MRKS
J=I-1
1 A(I)=FLCAT(J)*AINT+XMIN
RT=FLCAT(ISTRT)-FLOAT(NFL)/2.
SKP=FLOAT(NXPTS)/FLOAT(NDIV)-FLOAT(NFL)
IRT=JFIX(RT)
NSKP=JFIX(SKP)
ENCCDE(22,100,FRMT)IRT,MRKS,NFL,NDEC,NSKP
100 FORMAT(5H(1H,,I2,2HX,,I2,2H(F,I1,1H.,I1,1H.,I2,3HX)))
WRITE(6,FRMT)(A(I),I=1,MRKS)
RETURN
END

```

```

SUBROUTINE FILL(IT,A)
DIMENSION A(3,3)
COMMON/ IIP/ IP(3,350)
COMMON/ IY/ Y(200)
COMMON/ IX/ X(200)
I1=IP(1,IT)
I2=IP(2,IT)
I3=IP(3,IT)
A(1,1)=X(I1)
A(1,2)=Y(I1)
A(1,3)=1.
A(2,1)=X(I2)
A(2,2)=Y(I2)
A(2,3)=1.
A(3,1)=X(I3)
A(3,2)=Y(I3)
A(3,3)=1.
RETURN
ENO

```

```

SUBROUTINE SCALE (X, Y, IX, IY, NPTS, XSIZE, YSIZE, YPTS, XMIN, XMAX, XPTS, YX
*)
DIMENSION X(1), Y(1), IX(1), IY(1)
XMIN=X(1)
YMIN=Y(1)
XMAX=X(1)
YMAX=Y(1)
DO 2 I=2, NPTS
XMIN=AMIN1(XMIN, X(I))
YMIN=AMIN1(YMIN, Y(I))
XMAX=AMAX1(XMAX, X(I))
YMAX=AMAX1(YMAX, Y(I))
2 CONTINUE
IF (YX.GT.0.) YMAX=YX
XPTS=XSIZE/.1
YPTS=YSIZE/.167
XRANGE=XMAX-XMIN
YRANGE=YMAX-YMIN
XRES=XPTS/XRANGE
YRES=YPTS/YRANGE
DO 10 I=1, NPTS
IX(I)=IFIX((X(I)-XMIN)*XRES)
10 IY(I)=IFIX((Y(I)-YMIN)*YRES)
RETURN
ENO

```

```

    IC=IC+1
13 CONTINUE
    A(JX)=SYH(6)
    IFLG=0
    A(110)=SYH(6)
    DO 4 J=1,NPTS
    IF(IY(J).NE.I) GO TO 4
    N=IX(J)+JX
    A(N)=SYH(2)
    YLAB=Y(J)
    IFLG=1
    4 CONTINUE
    IF(IFLG.EQ.0) GO TO 11
    WRITE(6,FRMT)(A(L),L=1,NSKP),YLAB,(A(L),L=JX,110)
    GO TO 12
11 WRITE(6,5)(A(L),L=1,110)
12 CONTINUE
    3 CONTINUE
    DO 8 I=1,JX
    8 A(I)=SYH(1)
    DO 9 I=JX,110
    9 A(I)=SYH(4)
    WRITE(6,5)(A(I),I=1,110)
    CALL TOP(INDIV,XMIN,XMAX,A,NFL,NDEC,JX,IXPTS)
C
c
c
    NCHR=22
    ENCODE(22,205,TLAB)
205 FORMAT(22HSURFACE ELEVATIONS CH.)
    CALL TLB(TLAB,NCHR,IXPTS,JX)
    RETURN
    END

```

```

SUBROUTINE SLB(SB,IS,IE,IYPTS)
DIMENSION SE?(1)
NCHR=27
SB(1)=1HD
SB(2)=1HI
SB(3)=1HS
SB(4)=1HT
SB(5)=1H.
SB(6)=1H
SB(7)=1HA
SB(8)=1HL
SB(9)=1HO
SB(10)=1HN
SB(11)=1HG
SB(12)=1H
SB(13)=1HB
SB(14)=1HO
SB(15)=1HU
SB(16)=1HN
SB(17)=1HC
SB(18)=1HA
SB(19)=1HR
SB(20)=1HY
SB(21)=1H
SB(22)=1H1
SB(23)=1H0
SB(24)=1H
SB(25)=1HK
SB(26)=1HM
SB(27)=1H.
IH=IYPTS/2
JH=NCHR/2
IS=IH-JH
IE=IS+NCHR-1
RETURN
ENO

```

```

FUNCTION JFIX(R)
JFIX=IFIX(R)
D=R-FLOAT(JFIX)
IF(D.GE..5) JFIX=JFIX+1
RETURN
END

```

```

SUBROUTINE ISBNDRY(I,NO)
COMMON/CUTOFF/IBP,NFLX,JJ1,JJ2
COMMON/BOUND/I9(75),BV(75),NBV

```

c
c
c
c
c
c
c

```

SUBROUTINE TO TELL US IF WE ARE AT A BOUNDARY POINT, AND
WHAT TYPE OF BOUNDARY POINT.

```

```

NO=0, NOT A BOUNDARY POINT.
NO=-1, DIRICHLET BOUNDARY POINT, ON OPEN BOUNDARY.
NO=1, ONSHORE BOUNDARY POINT INCLUDING ISLAND.

```

```

NIBP=IBP
IF(NIBP.LT.0) NIBP=-IBP
IST=NFLX+NIBP+1
IEND=NIBP+NFLX
IS=NIBP+1
IF(IEND.EQ.0) GO TO 4
IF(NIBP.EQ.0) GO TO 2
0 0 1 J=1,NIBP
K=IB(J)
IF(I.EQ.K) GO TO 8
1 CONTINUE
2 IF(NFLX.EQ.0) GO TO 4
0 0 3 J=IS,IEND
K=IB(J)
IF(I.EQ.K) GO TO 7
3 CONTINUE
4 DO 5 J=IST,NBV
K=IB(J)
IF(I.EQ.K) GO TO 6
5 CONTINUE
NO=0
RETURN
6 NO=-1
RETURN
7 NO=1
RETURN
8 NO=1
RETURN
END

```

```

SUBROUTINE TLB(TLA9,NCHR,IXPTS,JX)
DIMENSION FRMT(3),TLAB(3)
JHALF=NCHR/2
IHALF=IXPTS/2
NSKP=JX+IHALF-JHALF
NC=10
ENCODE(16,100,FRMT)NSKP,NC
WRITE(6,FRMT)TLAB(1),TLAB(2),TLAB(3)
100 FORMAT(5H(1H,,I2,4HX,3A,I2,1H))
RETURN
END

```

```

SUBROUTINE SCS(I1,I2,S,CS,OS)
COMMON/IX/X(200)
COMMON/IY/Y(200)
DX=X(I2)-X(I1)
DY=Y(I2)-Y(I1)
DS=(DX*DX+DY*DY)**.5
S=DY/DS
CS=DX/DS
RETURN
END

```

```

C SUBROUTINE MATRIX(DSHAPEX,DSHAPEY,K,NVRTX,NTRI,IFILE,MASL)
SUBROUTINE TO FORM GLOBAL MATRIX AND RIGHT HAND SIDE
DIMENSION DSHAPEX(1),DSHAPEY(1)
COMMON/IHEIGHT/N(200)
COMMON/ICNST/CONST1,CONST2
COMMON/CUTOFF/NISP,NFLX,NO,JNO
COMMON/IGRAD/DALPHAX,DALPHAY,DDEPTHX,DDEPTHY,DDELTA,DELTA,AREA
COMMON/INCRK/VALP(4500)
COMMON/INT/INTP(4500)
COMMON/IRHS/RHS(1200)
COMMON/IIP/IP(3,350)
COMMON/WIND/TAUX,TAUY,CURL
NROW=NVRTX
DO 1 I=1,3
  II=IP(I,K)
C
C
  IF(N(II).EQ.-1) GO TO 1
  IF(N(II).EQ.1) GO TO 1
  IF(NO.EQ.-1) GO TO 4
  IF(IFILE)3,3,4
3 DO 2 J=1,3
  JJ=IP(J,K)
  CALL MNSRT(II,JJ,INTP,NB,NROW,MASL)
  VALP(NB)=VALP(NB)+(+CONST2*(DSHAPEX(I)*DSHAPEX(J)+DSHAPEY(I)*DSHAPEY(J))
  +1./3.*(DSHAPEX(I)*DDEPTHX-DSHAPEX(J)*DDEPTHY))*AREA
2 CONTINUE
4 CONTINUE
  CHK=CONST1*(DALPHAY*DDEPTHX-DALPHAX*DDEPTHY)/3,
  CHK1=CONST1*CONST2*(DSHAPEX(I)*DALPHAX+DSHAPEY(I)*DALPHAY)
  RHS(II)=RHS(II)+(-CHK-CHK1-1./3.*CURL)*AREA
1 CONTINUE
900 FORMAT(*0*,*TRI.*,I3,5X,*VRTX.*,I5 *5X9*JACOBO**F1004)
RETURN
ENO

```

```

103 CONTINUE
102 CONTINUE
  WRITE(6,200) 11,12
200 FORMAT(*0*,*WE ARE LOST ALONG POINTS*,2I5,2X,*CAN NOT FIND BOUNDAR
  Y TRIANGLE IN MATRIX ASSEMBLY ROUTINE*)
  GO TO 101
C
C   WE HAVE FOUND TRIANGLE, NOW TO GET GRADIENTS
C
104 00 106 L=1,3
  H=IP(L,K)
  A(L,1)=X(H)
  A(L,2)=Y(H)
  A(L,3)=1.
106 CONTINUE
  CALL ALPHX(K,DALPHX,DALPHY,ALPHA,SA,ALPH)
  CALL ALPHX(K,DDELTX,DDELTY,DELTA,SD,ALPH)
  CALL SCS(I1,I2,S,CS,DS)
  HMEAN=- (DEPTH(I1)+DEPTH(I2))/2.
  DDELTS=CS*DDELTX+S*DDELTY
  DALPHN=-S*DALPHX+CS*DALPHY
  DALPHS=CS*DALPHX+S*DALPHY
  TS=CS*TAUX+TAUY*S
C
  DO 107 L=1,3
  0 0 108 M=1,3
1 0 8 B(M)=0.
  B(L)=1.
  CALL GRAD(B(1),S(2),S(3),DSHPX(L),DSHPY(L),CSHPE(L))
107 CONTINUE
C
C   NOW ADD TO-GLOBAL MATRIX
C
  II=I1
109 IF(NEHBV.GT.1) GO TO 111
  IF(IFILE)609,609,111
609 00 112 L=1,3
  JJ=IP(L,K)
  CALL MNSRT(II,JJ,INTP,NB,NVRTX,MASL)
  DSHPN=-S*DSHPX(L)+CS*DSHPY(L)
  DSHPS=CS*DSHPX(L)+S*DSHPY(L)
  VALP(NB)=VALP(NB)-(CONST2*(DSHPN+DSHPS)-HMEAN*DSHPS) ● OS/20
112 CONTINUE
111 CONTINUE
C
C   NOW ADD CONTRIBUTION TO RHS
C
  RHS(II)=RHS(II)-(CONST1*DDELTS-CONST1*CONST2*(DALPHN+DALPHS)-TS)*D
  CS/2.
  IF(II.EQ.I2) GO TO 101
  II=I2
  GO TO 1.09
101 CONTINUE

```



```

SUBROUTINE BASS (VALP, RHS)
DIMENSION VALP(1), RHS(1)
DIMENSION DSHPX(3), DSHPY(3), CSHPE(3)
COMMON/ICNST/CONST1, CONST2
COMMON/INT/INTP (4500)
COMMON/LSCOEF/SA(4), SD(4)
COMMON/DELTA/DELTA(200)
COMMON/IALPHA/ALPHA(200)
COMMON/IDEPH/DEPTH(200)
COMMON/IY/Y(200)
COMMON/IIP/IP(3,350)
COMMON/IA/A(3,3)
COMMON/IB/B(3)
COMMON/IX/X(200)
COMMON/NUMB/NVRTX, NTRI, IFILE, MASL, NEWBV
COMMON/BOUND/IB(75), BV(75), NBV
COMMON/IALP/ALPH(3)
COMMON/WIND/TAUX, TAUY, CURL
COMMON/CUTOFF/NISP, NFLX, JJ1, JJ2

```

C
C
C
C

```

NOWIMPOSE THE NO FLUX BOUNDARY CONDITIONS,
BEGIN WITH ISLAND.

```

```

IF (NISP.EQ.0.AND.NFLX.EQ.0) RETURN
IF (NISP.EQ.0) GO TO 1
ISTART=1
ISTOP=NISP-1
GO TO 2
1 ISTART=1
  ISTOP=NFLX-1
  GO TO 2
3 ISTART=NISP+1
  ISTOP=NISP+NFLX-1
2 CONTINUE

```

C
C
C

```

NOWLOCATE BOUNDARY SIDE.

```

```

DO 101 I=ISTART,ISTOP
J=I+1
I1=IB(I)
I2=IB(J)

```

C
G
C

```

NOW LOCATE THE TRIANGLE WE ARE IN

```

```

DO 102 K=1,NTRI
KF=0
JF=0
DO 103 L=1,3
II=IP(L,K)
IF (II.EQ.I1) JF=L
IF (II.EQ.I2) KF=L
IF (KF.NE.0.AND.JF.NE.0) GO TO 104

```



```

SUBROUTINE SLVK(NROW,NCOL,ERRCR,INTP,VALP)
C.....SOLUTION OF LINEAR SYSTEM AFTER QUP DECOMPOSITION
C.....KNIU THORTHOGGNAL LIST STRAGE SCHEME
C.....
C.....NROW IS NUMBER OF ROWS IN MATRIX
C.....NCOL IS NUMBER OF COLUMNS IN MATRIX
C.....ERROR IS A N INTEGER VARIABLE RETURNED AS 1
C.....IF AN ERRCR OCCURS (ATTEMPTED DIVISION BY ZERO)
C.....OTHERWISE 2
C.....INTP IS A N INTEGR ARRAY OF LENGTH MSZ*((44/(NUMBER OF BITS
C.....PER INTEGER WORD)+1)...(SEE HINIT)
C.....VALP IS A REAL ARRAY OF LENGTH MSZ
C.....THE RIGHT HANO SIDE MUST BE STORED IN (VALP(I),I=1,2,...,NROW)
C.....AND THE SOLUTION IS RETURNED IN (VALP(I),I=NROW+1,NROW+2,...
C.....,NROW+NCOL)
C.....
C.....CAN ACCEPT A MATRIX WITH BOTH PERMUTED ROWS AND PERMUTED COLS
C.....**31APR75
      INTEGER INTP(1),ERROR
      REAL VALP(1)
      IP=IUP(INTP,1)
      IVS1=LEFT(INTP,NROW+1)+NROW
      VALP(IVS1)=VALP(IP)
      I=1
      80 IF(I-NCOL) 10,20,20
      10 I=I+1
      IP=IUP(INTP,I)
      IM1=I-1
      SUM=1.0
C.....ROW SCAN FROM COL 1 TO COL IM1
      ILFT=IP
      50 ILFT=LEFT(INTP,ILFT)
      KCOLS=ICOL(INTP,ILFT)
      IF(KCOLS) 60,60,30
      30 KCOLA=ICOL(INTP,KCOLS+NROW)
      IF(KCOLA-IM1) 70,70,50
      70 KCOLV=KCOLS+NROW
      SUM=SUM+VALP(ILFT)*VALP(KCOLV)
      GOTO 50
      60 IV=LEFT(INTP,I+NROW)+NROW
      VALP(IV)=VALP(IP)-SUM
      GOTO 80
      20 IP=IUP(INTP,NCOL)
      NB=NBOX(IP,LEFT(INTP,NCOL+NROW),NROW,INTP)
      IF(NB) 100,100,110
      100 ERROR=1
      RETURN
      110 NV=LEFT(INTP,NROW+NCOL)+NROW
      VALP(NV)=VALP(NV)/VALP(NB)
C.....COLUMN SCAN FROM ROW NCOL-1 TO ROW I
      I=NCOL
      170 IF(I-1) 150,150,160
      160 I=I-1

      IF(NIBP.EQ.0) GO TO 201
      J=NIBP-1
      IF(ISTOP.EQ.J) GO TO 3
      201 CALL SETB(RHS,VALP)
      RETURN
      END

```

```

SUBROUTINE DCPK(NROW,NCOL,SING,RANK,FILL, SMALL,INTP,VALP,MASL)
C.....OLUP DECOMPOSITION OF A REAL MATRIX
C.....KNUTH ORTHOGONAL LIST STORAGE
C.....
C.....NROW IS NUMBER OF ROWS IN MATRIX
C.....NCOL IS NUMBER OF COLUMNS IN MATRIX
C.....ROW SCALE FACTORS ARE STORED IN ROWBASE VALUES TEMPORARILY
C.....SING IS AN INTEGER VARIABLE RETURNING 1 IF MATRIX IS SINGULAR
C.....MEANING THAT RANK IS LESS THAN NCOL ...SING RETURNS 2 OTHERWISE
C.....RANK IS AN INTEGER VARIABLE RETURNING THE ROW RANK OF THE MATR
C.....FILL IS AN INTEGER VARIABLE RETURNING THE NUMBER OF ORIGINALLY
C.....ZERO MATRIX ELEMENTS THAT BECAME NONZERO DURING DECOMPOSITION
C.....MINUS THE NUMBER OF INITIALLY NONZERO ELEMENTS THAT BECAME
C.....ZERO DURING THE DECOMPOSITION PROCESS
C.....SMALL IS A REAL CONSTANT THAT SPECIFIES THE SMALLEST ABSOLUTE
C.....VALUE OF AN ELEMENT RELATIVE TO THE LARGEST ABSOLUTE VALUE
C.....OF ANY ELEMENT IN ITS ROW BEFORE DECOMPOSITION (THE ROW NORM)
C.....THAT WILL BE REPRESENTED BY MATRIX STORAGE ELEMENT
C.....INTP IS AN INTEGER ARRAY OF LENGTH MSZ*(44/(INTEGER NORD LENGT
C.....INBITS))+1....(SEE INIT SUBROUTINE)
C.....MASL IS A VARIABLE INITIALIZE BY MINIT
C.....ROWS AND COLUMNS ARE PERMUTED VIA ROW+COL BASES
C***** #***
C.....**31MAR76
C.....
      REAL VALP(1)
      INTEGER INTP(1), SING, RANK, FILL
      FILL=0
C.....FIND SCALE FOR EACH ROW=1.0/(MAX ABS VALUE IN ROW)
      I=C
      90 IF(I-NROW) 10,20,20
      10 I=I+1
      ROWNR=0.0
C.....START ROW I SCAN
      ILFT=I
      50 ILFT=LEFT(INTP,ILFT)
      IF( ICCL(INTP,ILFT)) 30,30,40
      40 ABV=ABS(VALP(ILFT))
      IF(ABV-ROWNR) 50,50,60
      60 ROWNR=ABV
      GOTC 50
      30 IF(ROWNR-SMALL) 70,70,80
      70 VALP(I)=0.0
      GOTC 90
      80 VALP(I)=1.0/ROWNR
      GOTC 90
      20 NH1=NCOL-1
C.....START COLUMN SCAN
      K=0
      240 IF(K-NH1) 100,110,110
      100 K=K+1
C.....SCAN LOWER RIGHT SUBMATRIX FOR COLUMN WITH LEAST NUMBER OF
C.....NONZERO ELEMENTS BY AT LEAST ONE

```

```

SUBROUTINE PACK(I,J,VALP,VAL,INTP,NROW,MASL)
DIMENSION VALP(1),INTP(1)
CALL MNSRT(I,J,INTP,NB,NROW,MASL)
IF(MASL.EQ.-1) GO TO 10
VALP(NB)=VAL
RETURN
10 WRITE(6,5)I,J
5 FORMAT(*0*,*OVERFLOW OF VALP AT ENTRY*,I5,*,*,I3)
RETURN
END

```

```

      GOTO 650
C.....TOOSMALL SO DELETE
690 CALL MDLET(IP,ICJRS,NROW,INTP,MASL)
      FILL=FILL-1
      GOTO 650
C.....NO MATCH SO FILL IM ONE
660 VAL=EM*VALP(JP)
C.....UNLESSTOOSMALL TO STORE
      IF(ABS(VAL)*SKALE-SMALL) 650,650,710
710 FILL=FILL+1
      CALL MNSRT(IP,ICJFS,INTP,NB,NROW,MASL)
C.....DEJECTMEMORU OVERFLOW
      IF(NB) 720,720,730
730 VALP(NB)=VAL
      GOTO 650
C.....MEMORY OVERFLOW
C.....USER DETECTS THIS CONDITION IN CALLING PRIGRAM
C.....BY TESTING WHETHER MASL.LE.O
720 K=1
      GOTO 180
110 IF(NBOX(IUP(INTP,NCCL),LEFT(INTP,NCOL+NROW),NROW,INTP))500,500,510
C.....RANK IS NCOL-1 IF DIAGONAL IS ZERO
500 K=NCCL
      GOTO 180
510 RANK=NCOL
      SING=2
      RETURN
      END

```

```

      IP=IUP(INTP,I)
      IP1=I+1
      SUM=0.0
C.....ROWS ACN FROM COL IP1 TO COL NCOL
      ILFT=IP
200 ILFT=LEFT(INTP,ILFT)
      KCOLS=ICOL(INTP,ILFT)
      IF(KCOLS) 180,180,190
190 KCOLA=ICOL(INTP,KCOLS+NROW)
      IF(KCOLA-IP1) 200,310,320
320 IF(KCOLA-NCOL) 310*310,200
310 KCOLV=KCOLS+NROW
      SUM=SUM+VALP(ILFT)*VALP(KCOLV)
      GOTO 200
180 NB=NBOX(IP,LEFT(INTP,I+NROW),NROW,INTP)
      IF(NB) 100,100,220
220 IV=LEFT(INTP,I+NROW)+NROW
      VALP(IV)=(VALP(IV)-SUM)/VALP(NB)
      GOTO 170
150 ERRCR=2
      RETURN
      END

```

```

SUBROUTINE SUP(INTP,NBOX,IUP)
INTEGER INTP(1)
CALL PAC(INTP(NBOX),20,35,IUP)
RETURN
END

```

```

      NEMAX=NCOL+1
      NPIV=0
      KA=K-1
620  IF(KA-NCOL)800,810,810
800  KA=KA+1
      CALL FVSL1(KA,NROW,NCOL,INTP,VALP,IPIV,NE)
      IF(NE) 820,820,830
830  IF(NE-NEMAX) 840,820,820
840  NPIV=IPIV
      NEMAX=NE
      GOTO 820
810  IF(NPIV)180,180,190
C.....NO PIVOT C N K-TH COLUMN
180  RANK=K-1
      SING=1
      RETURN
C.....PIVOT ON IPIV
190  KP=IRCH(INTP,NPIV)
      KC=ICOL(INTP,NPIV)
C.....ROW INTERCHANGE IF PIVOT NOT IN ROW K
      CALL MRXA(K,IROW(INTP,KP),NROW,INTP)
C.....COLUMN INTERCHANGE IF PIVOT NOT IN COLUMN K
      CALL MCXA(K,ICOL(INTP,KC+NROW),NROW,INTP)
      PIVCT=VALP(NPIV)
      I=K
230  IF(I-NROW)220,240,240
220  I=I+1
      IP=I+(INTP,I)
      NB=NEOX(IP,LEFT(INTP,K+NROW),NROW,INTP)
      IF(NB) 230,230,250
250  EM=-VALF(NB)/PIVOT
      VALF(NB)=-EM
C.....START SCAN OF PIVOT ROW IN STORED ORDER
      JP=KP
      SKALE=VALP(IP)
650  JP=LEFT(INTP,JP)
      ICJPS=ICOL(INTP,JP)
      IF(ICJPS) 230,230,E10
610  ICJPA=ICOL(INTP,ICJPS+NROW)
      IF(ICJPA-K) 650,550,630
630  IF(ICJPA-NCOL)640,640,650
C.....TRY TO FIND ACTUAL SAME COLUMN IN WORKROW
640  JR=IP
600  JR=LEFT(INTP,JR)
      ICJRS=ICOL(INTP,JR)
      IF(ICJRS) 660,660,670
670  ICJRA=ICOL(INTP,ICJRS+NROW)
      IF(ICJRA-ICJPA) 600,650,600
C.....FIND MATCH
680  VAL=VALP(JR)+EM*VALP(JP)
      IF(ABS(VAL)*SKALE-SMALL 1 690,690,700
C.....STORE RESULT
700  VALF(JR)=VAL

```

```

      Subroutine MNSRT(KROW,KCOL,INTP,NB,NROW,MASL)
C.....INSERTS A MATRIX STORAGE ELEMENT AT ROW KROW AND COLUMN KCOL
C.....UNLESS THERE IS ALREADY AN ELEMENT ALLOCATED IN WHICH CASE
C.....THAT ELEMENT NUMBER IS RETURNED IN NB
C.....INTP IS AN INTEGER ARRAY
C.....(SEE MINIT)
C.....NB IS THE NEW ELEMENT NUMBER
C.....NROW IS THE NUMBER OF ROWS IN THE MATRIX
C.....MASL IS AN INTEGER VARIABLE INITIALIZED BY MINIT
C.....MASL=-1 IMPLIES OVERFLOW IN WHICH CASE NB
C.....RETURNS -1

```

```

C.Q..* * * * *
      INTEGER INTP(1)
      IRGT=KROW
    30 ILFT=LEFT(INTP,IRGT)
      IF (ICCL(INTP,ILFT)-KCOL) 50,20,90
    90 IRGT=ILFT
      GOTO 30
    50 IBLW=NROW+KCOL
    150 IABV=IUP(INTP,IBLW)
      IF (IRCW(INTP,IABV)-KROW) 130,20,120
    120 IBLW=IABV
      GOTO 150
    130 IF (MASL) 60,60,70
    60 NB=-1
      RETURN
    70 NB=MASL
      MASL=LEFT(INTP,MASL)
      CALL SLEFT(INTP,IRGT,NB)
      CALL SLEFT(INTP,NB,ILFT)
      CALL SUP(INTP,IBLW,NB)
      CALL SUP(INTP,NB,IABV)
      CALL SROW(INTP,NB,KROW)
      CALL SCOL(INTP,NB,KCOL)
      RETURN
    20 NB=ILFT
      RETURN
      END

```

```

      SUBROUTINE SCOL (INTP,NBOX,ICCL)
      INTEGER INTP(1)
      CALL PAC(INTP(NBOX),48,59,ICCL)
      RETURN
      END

```

```

      SUBROUTINE SRCW (INTP,NBOX,IRCW)
      INTEGER INTP(1)
      CALL PAC(INTP(NBOX),36,47,IRCW)
      RETURN
      END

```

```

      FUNCTION LEFT (INTP,NBOX)
      INTEGER INTP(1)
      CALL UNPAC(INTP(NBOX),4,19,LEFT)
      RETURN
      END

```

```

FUNCTION IUP(INTP,NBOX)
INTEGER ITP(1)
CALL UNPAC(INTP(NBOX),20,35,IUP)
RETURN
END

```

```

FUNCTION ICCL(INTP,NBOX)
INTEGER ITP(1)
CALL UNPAC(INTP(NBOX),48,59,ICOL)
RETURN
END

```

```

FUNCTION IRCW(INTP,NBOX)
INTEGER ITP(1)
CALL UNPAC(INTP(NBOX),36,47,IROW)
RETURN
END

```

```

SUBROUTINE MOLET(KROW,KCOL,NROW,INTP,MASL)
C.....DELETES MATRIX STORAGE ELEMENT AT IROW,ICCL IF ONE EXISTS
C.....NROW IS THE NUMBER OF ROWS IN THE MATRIX
C.....INTP IS AN INTEGER ARRAY (SEE MINIT)
C.....MASL IS AN INTEGER VARIABLE INITIALIZED BY MINIT
C.....*****020176*****
C.....
INTEGER ITP(1)
IABV0=NROW+KCOL
ILFT0=KROW
30 ILFT=LEFT(INTP,ILFT0)
IC=ICCL(INTP,ILFT)
IF(IC) 10,10s20
20 IF(IC-KCOL) 70,40,70
70 ILFT0=ILFT
GOTO 30
40 IABV=IUP(INTP,IABV0)
IR=IROW(INTP,IABV)
IF(IR) 10,10,50
50 IF(IR-KROW) 60,60s50
80 IABV0=IABV
GOTO 40
60 ILFT1=LEFT(INTP,ILFT)
CALL SLEFT(INTP,ILFT0,ILFT1)
IABV1=IUP(INTP,IABV)
CALL SUP(INTP,IABV0,IABV1)
CALL SLEFT(INTP,IABV,MASL)
MASL=IABV
10 RETURN
END

```

```

FUNCTION IRCW(INTP,NBOX)
INTEGER ITP(1)
CALL UNPAC(INTP(NBOX),36,47,IROW)
RETURN
END

```

```

        FUNCTION NBOX(KROW,KCOL,NROW,INTP)
C.....GETSMATRIX STORAGE ELEMENTNUMBER IF ONE EXISTSFORROWKROW
C.....ANDCOLUMN KCOL
C.....NROWIS HE NUMBER OF ROWSIN THE MATRIX
C.....INTP IS AN INTEGERARRAY (SEE HINIT)
C.....NBOX RETURNS THEELEMENTNUMBER UNLESS ONE DOESNT EXIST
C.....INWHICH CASE IT RETURNS -1
C.....
        INTEGER INTP(1)
        ILFT=KROW
    30 ILFT=LEFT(INTP,ILFT)
        IF(ICCL (INTP,ILFT)-KCOL) 10,20,30
    10 NBOX=-1
        RETURN
    20 NBOX=ILFT
        RETURN
        END

```

```

SUBROUTINE SLEFT (INTP,NBOX,LEFT)
INTEGER INTP(1)
CALL FAC (INTP(NBOX),4,19,LEFT)
RETURN
END

```

```

SUBROUTINE MRXA (KRA,JRA,NROW,INTP)
INTEGER INTP(1)
IF (KRA-JRA) 10,20,10
20 RETURN
10 KRS=IUP (INTP,KRA)
   JRS=IUP (INTP,JRA)
   CALL SUP (INTP,KRA,JRS)
   CALL SUP (INTP,JRA,KRS)
   CALL SROW (INTP,JRS,KRA)
   CALL SROW (INTP,KRS,JRA)
   RETURN
END

```

```

SUBROUTINE LOFIT(VAL,S,AVAR,LIST,NPTS)
COMMON/IRMS/B(200)
COMMON/IDDEPTH/D(200)
COMMON/HEIGHT/STNDV(200)
DIMENSION A(4,4)
DIMENSION VAL(1),S(1),C(4),IPS(1)
C
C   LEAST SQUARES FIT TO THIRD ORDER POLYNOMIAL IN Z.
C
C   S ARE THE COEFFICIENTS, LIST IS THE LISTINGS OPTION.
C
      NCOEF=4
      DO 2 I=1,NCOEF
        B(I)=0.
      DO 3 J=1,NCOEF
3    A(I,J)=0.
2    CONTINUE
      DO 4 I=1,NPTS
        C(1)=D(I)*D(I)*D(I)
        C(2)=D(I)*D(I)
        C(3)=D(I)
        C(4)=1.
      DO 11 J=1,NCOEF
      DO 7 K=J,NCOEF
7    A(J,K)=A(J,K)+C(J)*C(K)
11   B(J)=B(J)+VAL(I)*C(J)
4    CONTINUE
C
C   NOW TO FILL THE OTHER HALF OF THE MATRIX
      DO 8 I=1,NCOEF
      DO 9 J=1,NCOEF
9    A(J,I)=A(I,J)
8    CONTINUE
      CALL INVR(A,4,8,1,DETERM,4,4)
      GO 306 I=1,4
      S(I)=B(I)
306   CONTINUE
      IF(LIST.EQ.0) GO TO 101
      WRITE(6,20) (S(I),I=1,NCOEF)
20   FORMAT(*1*,*COEFFICIENTS ARE*,2X,5F10.4)
      IF(LIST.LT.0) GO TO 101
      WRITE(6,45)
45   FORMAT(*0*,*GLOBAL LAEEL*,10X,*DEPTH*,10X,*ALPHA*,10X,*DEVIATION*,
        *10X,*VARIANCE*,/)
      GO TO 144
201  WRITE(6,145)
145  FORMAT(*0*,*GLOBAL LAEEL*,10X,*DEPTH*,10X,*CELTAS10X!*OEVI*1 10X*,10
        *10X,*VARIANCE*,/)
144  CONTINUE
101  TOT=0.
      DO 13 I=1,NPTS
        ALP=S(1)*C(1)*D(I)*D(I)+S(2)*D(I)*D(I)+S(3)*D(I)+S(4)
        SD=VAL(I)-ALP

        STNDV(I)=SD
        VAR=SD*SD
        TOT=TOT+VAR
        IF(LIST.EQ.0) GO TO 102
        WRITE(6,35) I,D(I),VAL(I),SD,VAR
35   FORMAT(* *,I7,13X,F8.2,7X,F10.4,6X, F9.3*10X*F9.3)
102  CONTINUE
13   CONTINUE
      AVAR=TOT/FLCAT(NPTS)
      AVAR=AVAR*.5
      IF(LIST.EQ.0) GO TO 103
      WRITE(6,30) AVAR
30   FORMAT(*0*,*MEAN STANDARD DEVIATION MAGNITUDE IS*,2X,F8.3)
103  CONTINUE
      RETURN
      END

```



```

SUBROUTINE MCXA(KCA,JCA,NROW,INTP)
INTEGER INTP(1)
IF(KCA-JCA) 10,20,10
20 RETURN
10 KCS=LEFT(INTP,KCA+NROW)
   JCS=LEFT(INTP,JCA+NROW)
   CALL SLEFT(INTP,JCA+NROW,KCS)
   CALL SLEFT(INTP,KCA+NROW,JCS)
   CALL SCCL(INTP,KCS+NROW,JCA)
   CALL SCCL(INTP,JCS+NROW,KCA)
RETURN
END

```

```

SUBROUTINE SLCPE(X1,Y1,X2,Y2,SLOP,DIST)
DY=Y2-Y1
DX=X2-X1
IF(DX.EQ.0)DX=.00000001
SLCP=CY/DX
DIST=((DX*DX)+(DY*DY))*.5
RETURN
END

```

```

SUBROUTINE FINDSID(VAL1,VAL2,VAL3,VAL,IP1,IP2,IFLG)
DIMENSION IP1(2),IP2(2)
IFLG=0
J=1
IF(VAL1.EQ.VAL) GO TO 11
IF(VAL2.EQ.VAL) GO TO 12
IF(VAL3.EQ.VAL) GO TO 13
6 IF(VAL.LT.VAL1.AND.VAL.GT.VAL2) GO TO 1
IF(VAL.GT.VAL1.AND.VAL.LT.VAL2) GO TO 1
7 IF(VAL.LT.VAL2.AND.VAL.GT.VAL3) GO TO 2
IF(VAL.GT.VAL2.AND.VAL.LT.VAL3) GO TO 2
8 IF(VAL.LT.VAL1.AND.VAL.GT.VAL3) GO TO 3
IF(VAL.GT.VAL1.AND.VAL.LT.VAL3) GO TO 3
IF(IFLG.EQ.1) GO TO 4
WRITE(6,5)
5 FORMAT(*1*,*WE HAVE SCREWED UP IN FINDING THE TRIANGLE SIDE*)
GO TO 4
11 IP1(1)=1
   IP2(1)=2
   J=2
   IFLG=1
   GO TO 7
12 IP1(1)=1
   IP2(1)=2
   J=2
   IFLG=1
   GO TO 8
13 IP1(1)=2
   IP2(1)=3
   J=2
   IFLG=1
   GO TO 6
1 CONTINUE
IP1(J)=1
IP2(J)=2
IF(J.GT.1) GO TO 4
J=J+1
IFLG=0
GO TO 7
2 IP1(J)=2
   IP2(J)=3
   IF(J.GT.1) GO TO 4

```

```

J=J+1
IFLG=0
GO TO 8
3 IP1(J)=1
  IP2(J)=3
  IFLG=0
4 RETURN
END

```

```

SUBROUTINE SWITCH(A,B)
C=A
A=B
B=C
RETURN
END

```

```

SUBROUTINE FINDPT(VAL1,VAL2,VAL,X1,Y1,X2,Y2,X,Y,SLPE)
ISWITCH=0
IF(X2.GT.X1) GO TO 1
ISWITCH=1
CALL SWITCH(VAL1,VAL2)
CALL SWITCH(X1,X2)
CALL SWITCH(Y1,Y2)
1 CONTINUE
DIST12=VAL1-VAL2
DIST=VAL1-VAL
RATIO=DIST/DIST12
DIST12=X1-X2
DIST=Y1-Y2
DIST12=(DIST12**2+DIST**2)**.5
DIST=RATIO*DIST12
IF(X1.EQ.X2) GO TO 11
ANGLE=ATAN(SLPE)
DX=DIST*COS(ANGLE)
DY=DIST*SLPE
GO TO 12
11 CONTINUE
DX=0.
IF(Y1.GT.Y2)DIST=-DIST
DY=DIST
12 CONTINUE
X=X1+DX
Y=Y1+DY
IF(ISWITCH.EQ.0) GO TO 2
CALL SWITCH(VAL1,VAL2)
CALL SWITCH(X1,X2)
CALL SWITCH(Y1,Y2)
2 RETURN
END

```

```

SUBROUTINE CHECK(VAL1,VAL2,VAL3,VAL,ICLK,IP1,IP2)
ICLK=1
IF(VAL1.EQ.VAL2.AND.VAL1.EQ.VAL) GO TO 1
IF(VAL2.EQ.VAL3.AND.VAL2.EQ.VAL) GO TO 2
IF(VAL1.EQ.VAL3.AND.VAL1.EQ.VAL) GO TO 3
ICLK=0
IP1=0
IP2=0
GO TO 4
1 IP1=1
  IP2=2
  GO TO 4
2 IP1=2
  IP2=3
  GO TO 4
3 IP1=1
  IP2=3
4 RETURN
END

```

```

SUBROUTINE KONTRI(X,Y,IP,CON,NTRI,NVRTX,CON,VALUE,NPEN)
DIMENSION X(1),Y(1),IP(3,1),CON(1),VALUE(1),X1(2),Y1(2),II(2),JJ
V(2),AX(2),AY(2)
C
C THIS IS A LINEAR CONTOURING ROUTINE USING THE TRIANGLES
C X AND Y ARE COORDINATES OF THE TRIANGLE VERTICES
C IP IS THE MATRIX(3 x NTRI) CONTAINING THE GLOBAL LABELS OF EACH
C TRIANGLE VERTEX
C CON IS THE VECTOR CONTAINING THE CONTOUR INTERVALS.
C NTRI IS THE NUMBER OF TRIANGLES
C NVRTX IS THE NUMBER OF GLOBAL POINTS
C NCON IS THE NUMBER OF CONTOURS YOU HAVE. IF THIS IS LESS THAN
C ZERO, THEN YOU ARE READING IN THE CONTOUR INTERVALS WITH
C THE NUMBER OF INTERVALS EQUAL TO ABS(NCON). IF NCON IS
C POSITIVE, THEN THE PROGRAM WILL GENERATE THE CONTOUR INTERVALS
C BY DIVIDING THE RANGE OF VALUES EVENLY INTO NCON INTERVALS.
C VALUE IS THE VECTOR CONTAINING THE VALUES TO BE CONTOURED AT EACH
C VERTEX
C NPEN IS THE PEN NUMBER YOU WANT TO USE FOR CONTOURING
CALL STPEN(NPEN)
IF(NCON.LT.0) GO TO 3
VMAX=0.
VMIN=1000000.
DO 1 I=1,NVRTX
VMAX=AMAX1(VMAX,VALUE(I))
1 VMIN=AMIN1(VMIN,VALUE(I))
CALL CONINT(VMAX,VMIN,NCON,CON)
3 NCON=IABS(NCON)
N=1
11 I=IP(1,N)
J=IP(2,N)
K=IP(3,N)
ALARG=AMAX1(VALUE(I),VALUE(J),VALUE(K))
ASMAL=AMIN1(VALUE(I),VALUE(J),VALUE(K))
IFIR=1
DO 6 L=1,NCON
IF(CON(L).LT.ASMAL.OR.CON(L).GT.ALARG) GO TO 6
IF(IFIR.GT.1) GO TO 4
CALL SLCPE(X(I),Y(I),X(J),Y(J),S12,DIS12)
CALL SLCPE(X(J),Y(J),X(K),Y(K),S23,DIS23)
CALL SLCPE(X(I),Y(I),X(K),Y(K),S13,DIS13)
IFIR=2
4 CALL CHECK(VALUE(I),VALUE(J),VALUE(K),CON(L),ICLK,II,JJ)
IF(ICLK.EQ.0) GO TO 5
II=IP(II,N)
JJ=IP(JJ,N)
X1(1)=X(II)
Y1(1)=Y(II)
X1(2)=X(JJ)
Y1(2)=Y(JJ)
CALL STNPTS(2)
CALL SLLILI(X1,Y1)
GO TO 6

SUBROUTINE CONINT(VMAX,VMIN,INT,C)
DIMENSION C(1)
INT=INT+1
DIFF=VMAX-VMIN
AINT=DIFF/FLOAT(INT)
INT=INT-1
DO 1 I=1,INT
C(I)=VMIN+FLOAT(I)*AINT
1 CONTINUE
WRITE(6,2)
2 FORMAT(*1*,*CONTOUR INTERVALS ARE*)
DO 4 I=1,INT
4 WRITE(6,3)I,C(I)
3 FORMAT(*D*,I5,3X,F10.2)
RETURN
ENO

```

```

SUBROUTINE SETUP(ISTART,IPRINT,XSIZE,YSIZE,TLABEL, IAXIS,XMIN, XMAX,
YMIN,YMAX,NDIVX,NDIVY,XSTRT,YSTRT)
DIMENSION TLABEL(3)
C THIS IS A GENERAL SUBROUTINE TO SETUP AN NPS PROGRAM
C ISTART IS ZERO IF THIS IS THE FIRST TIME YOU CALL THE NPS ROUTINES
C IF YOU HAVE ALREADY CALLED PRNTO OR STCCON PREVIOUSLY, ISTART=1
C IPRINT=0 WILL CALL PRINTER PLOT
C IPRINT=1 WILL CALL STCCON
C XSIZE IS THE LENGTH OF PLOT IN INCHES IN X-DIRECTION
C YSIZE IS LENGTH OF PLOT IN INCHES IN Y-DIRECTION
C TLABEL IS ENCODED IN MAIN PROGRAM WITH 30 SPACES AND DIMENSION 3.
C IT WILL BE THE TOP LABEL OF PLOT.
C IF YOU WANT AXIS DRAWN UP AND LABELED, IAXIS IS 1, OTHERWISE IT
C IS ZERO.
C XMIN,YMIN,XMAX,YMAX, ARE THE MAXIMUM AND MINIMUM X AND Y VALUES
C TO BE USED TO LABEL THE AXIS AND SET UP THE SUBJECT SPACE.
C NDIVX AND NDIVY ARE THE NUMBER OF DIVISIONS YOU WANT THE AXIS
C LABELING TO SHOW
C
IF(ISTART.EQ.1) GO TO 2
IF(IPRINT.EQ.1) GO TO 1
CALL PRNTO
GO TO 2
1 CALL STCCON(48HCALCOMP PLOT OF WHATEVER NEEDS TO BE PLOTTED)
2 CONTINUE
CALL STPEN(1)
XADD=XSTRT+XSIZE
YADD=YSTRT+YSIZE
CALL STS2OB(XSTRT,XADD,YSTRT,YADD)
CALL STSUBJ(XMIN,XMAX,YMIN,YMAX)
CALL STNDIV(1,1)
CALL GOLILI
HEIGHT=XSIZE/30.
IF(HEIGHT.GT..49) HEIGHT=.49
CALL STCHSZ(HEIGHT)
CALL STNCHR(30)
CALL STLNOR(0.)
CALL TITLET(TLABEL)
CALL AXLILI
IF(IAXIS.EQ.0) GO TO 3
CALL STNDIV(NDIVX,NDIVY)
HEIGHT=HEIGHT/2.
CALL STCHSZ(HEIGHT)
CALL STNDEC(1)
CALL MODLIB
CALL MODLIL
3 RETURN
ENO

```

```

5 CALI. FINDSID(VALUE(I),VALUE(J),VALUE(K),CON(L),III,JJJ,IFLG)
  IF(IFLG.EQ.1) GO TO 6
  IA=III(1)
  II=III(2)
  JA=JJJ(1)
  JJ=JJJ(2)
  IF(IA.EQ.1.AND.JA.EQ.2) SLP1=S12
  IF(IA.EQ.2.AND.JA.EQ.1) SLP1=S12
  IF(II.EQ.1.AND.JJ.EQ.2) SLP2=S12
  IF(JJ.EQ.1.AND.II.EQ.2) SLP2=S12
  IF(IA.EQ.1.AND.JA.EQ.3) SLP1=S13
  IF(JA.EQ.1.AND.IA.EQ.3) SLP1=S13
  IF(II.EQ.1.AND.JJ.EQ.3) SLP2=S13
  IF(JJ.EQ.1.AND.II.EQ.3) SLP2=S13
  IF(IA.EQ.2.AND.JA.EQ.3) SLP1=S23
  IF(JA.EQ.2.AND.IA.EQ.3) SLP1=S23
  IF(II.EQ.2.AND.JJ.EQ.3) SLP2=S23
  IF(JJ.EQ.2.AND.II.EQ.3) SLP2=S23
  IA=IP(IA,N)
  II=IP(II,N)
  JA=IP(JA,N)
  JJ=IP(JJ,N)
  CALL FINDPT(VALUE(IA),VALUE(JA),CON(L),X(IA),Y(IA),X(JA),Y(JA),X1(
  V1),Y1(1),SLP1)
  CALL FINDPT(VALUE(II),VALUE(JJ),CON(L),X(II),Y(II),X(JJ),Y(JJ),X1(
  V2),Y1(2),SLP2)
  CALL STNPTS(2)
  CALL SLLILI(X1,Y1)
6 CONTINUE
  N=N+1
  IF(N.GT.NTRI) GO TO 7
  GO TO 11
7 RETURN
  END

```

```

SUBROUTINE VRTXLB(X,Y,VAL,NDEC,NVRTX,HEIGHT,HPEN)
DIMENSION X(1),Y(1),VAL(1)
THIS SUBROUTINE LABELS THE POINTS
C THE COORDINATES OF THE POINTS ARE GIVEN BY X AND Y
C THE VALUE AT EACH POINT IS GIVEN BY VAL
C
CALL STPEN(HPEN)
CALL STCHSZ(HEIGHT)
CALL STLNOR(0)
CALL STNDEC(NDEC)
DO 1 I=1,NVRTX
CALL STLNST(X(I),Y(I))
CALL DECVAL(VAL(I))
1 CONTINUE
RETURN
END

```

```

SUBROUTINE DRTRI(X,Y,IP,NTRI,NPEN,N)
DIMENSION X(1),Y(1),IP(3,1),N(1),ZXX(2),ZYY(2)

C
C
C
C
C
C
C
C
C
SUBROUTINE TO DRAW SUEROUTINES
X IS X-ARRAY
Y IS Y-ARRAY
1P IS A THREEBYNTRI MATRIX GIVING THE GLOBAL LABELS OF EACH VRTX
N IS A STORAGE ARRAY MAKING SURE WE DONT DRAW A LINE TWICE
N SHOULD BE LARGER THAN THE AMOUNT OF LINES YOU HAVE
NPEN IS THE PEN NUMBER YOU WANT TO USE

CALL STPEN(NPEN)
N(1)=0
M=1
LL=0
DO 1 I=1,NTRI
IX=1
IY=2
2 II=IP(IX,I)
IJ=IP(IY,I)
ZXX(1)=X(II)
ZYY(1)=Y(II)
ZXX(2)=X(IJ)
ZYY(2)=Y(IJ)
ICHECK=II*II+II+IJ*IJ+IJ+II*II+IJ*IJ+II+IJ
DO 4 L=1,M
IF(ICHECK.EQ.N(L)) GO TO 6
4 CONTINUE
M=M+1
IF(M.LT.301) GO TO 10
M=300
LL=LL+1
IF(LL.GT.300) LL=1
N(LL)=ICHECK
GO TO 11
10 CONTINUE
N(M)=ICHECK
11 CONTINUE
CALL STNPTS(2)
)4(RTXTTS LLAC

CALL STTXTR(1)
CALL SLLILI(ZXX,ZYY)
6 IF(IY.EQ.3) GO TO B,
IY=3
GO TO 2
B IF(IX.EQ.2) GO TO 1
IX=2
GO TO 2
1 CONTINUE
RETURN
END

```

```

SUBROUTINE DYE&LAN(BRT,BRC,CURL,BFRIC,CONST1)
COMMON IGRAD,DALPHAX,DALPHAY,DDEPTHX,DDEPTHY,DEX,DEY,AREA
BRT=- (DEY*DDEPTHX-DEX*DDEPTHY)
BRC=- (DALPHAY*DDEPTHX-DALPHAX*DDEPTHY)*CONST1
BFRIC=-BRT-BRC-CURL
RETURN
END

```

```

SUBROUTINE TRILABL(X,Y,IP,NTRI,HEIGHT,NPEN)
DIMENSION X(1),Y(1),IP(3,1)

THIS SUBROUTINE LABELS THE TRIANGLES
X AND Y ARE RESPECTIVE COORDINATES
IP IS THE 3 X NTRI MATRIX CONTAINING THE GLOBAL LABELS OF THE VRTX
NTRI IS THE NUMBER OF TRIANGLES
HEIGHT IS THE HEIGHT OF THE NUMBERS IN INCHES
NPEN IS THE PEN NUMBER

CALL STPEN(NPEN)
CALL STCHSZ(HEIGHT)
DO 1 I=1,NTRI
  II=IP(1,I)
  IJ=IP(2,I)
  IK=IP(3,I)
  EX=(X(II)+X(IJ)+X(IK))/3.
  EY=(Y(II)+Y(IJ)+Y(IK))/3.
  XSHIFT=(HEIGHT/4.)*1.25
  YSHIFT=(HEIGHT/7.)*1.5
  EX=EX-XSHIFT
  EY=EY-YSHIFT
  CALL STNDEC(0)
  CALL STLNST(EX,EY)
  CALL DECVAL(FLOAT(I))
1 CONTINUE
RETURN
END

SUBROUTINE BAROT(U,V,TOT)
COMMON/IGRAD/DALPHAX,DALPHAY,DDDEPTHX,DDDEPTHY,DEX,DEY,AREA
COMMON/SCALES/USCALE,OSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
U=-DEX*USCALE
V=DEX*USCALE
U=U*100.
V=V*100.
TOT=(U*U+V*V)**.5
RETURN
END

SUBROUTINE EKMAN(U,V,TOT)
COMMON/HIND/TX,TY,CURL
COMMON/SCALES/USCALE,HSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
C=(EDDY*Q*FO)**(-.5)
U=C*(TX+TY)*USCALE*FO*HSCALE*Q
V=C*(-TX+TY)*USCALE*FO*HSCALE*Q
U=U*10000.
V=V*10000.
TOT=(U*U+V*V)**.5
RETURN
END

SUBROUTINE BOTT(U,V,TOT)
COMMON/IGRAD/DALPHAX,DALPHAY,DDDEPTHX,DDDEPTHY,DEX,DEY,C
COMMON/SCALES/USCALE,OSCALE,ALSCALE,G,E,Q,GAMMA,FO,EDDY
C=G/(Fe+@)
U=C*(DALPHAY*C*OSCALE+DEY*FO*USCALE*Q*ALSCALE/G)/ALSCALE
V=C*(DALPHAX*E*DSCALE+DEX*FO*USCALE*ALSCALE*Q/G)/ALSCALE
U=U*100.
V=V*100.
TOT=(U*U+V*V)**.5
RETURN
END

```

```

SUBROUTINE SURF (UE,VE,UB,VB,U,V,TOT)
U=UE+US
V=VE+VB
TOT=(U*U+V*V)**.5
RETURN
ENO

```

```

* BITS I - J OF A ARE EXTRACTED
. IF I GT 5, N=60-(I-J-1)
. BITS I - 59, 0 - J OF A ARE EXTRACTED
. BIT J OF A ALWAYS GOES TO BIT 59 OF B
*
      ENTRY UNPAC
      VFD 42/0LUNPAC
      IFEQ *F,2
UNPAC  VFD 18/UNPAC      FTN ARGUMENT LINKAGE
      BSSZ 1
      SB7 1              B7 = 1
      SA2  A1+B7        GET ADDRESSES OF 1 - 9 IN X: - XL
      sb3  A2+B7
      SA4  A3+B7
R      MICRC 191,$X$
      ELSE
      IFNE *F,1,1
      ERR
      VFD 18/4
      BSSZ 1
UNPAC  R      MICRO 1,1,$B$
      ENOIF
      SA2  VRV.2        X2 = I
      SA3  VRV.3        X3 = J
      I X5  X3-X2        FIGURE NO. BITS - 1 TO EXTRACT FROM A
      PL   X5,J1
      SX5  X5+60
      SB6  X2-60
      SB5  X3+1
      SB7  X5
      MX0  1            MAKE MASK OF CORRECT LENGTH
      SA1  VRV.1        X1 = A
      AX0  B7
      LX0  -BE
      BX6  X0*X1        ALIGN MASK WITH CORRECT BITS OF A
      LX6  B5            EXTRACT BITS FROM A
      SA6  VRV.4        RIGHT-JUSTIFY THEM
      EQ   UNPAC        STORE IN B
      END              EXIT

```



```

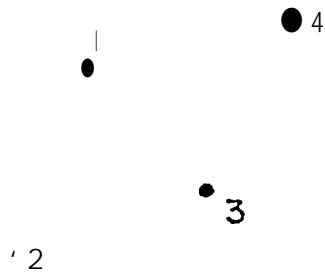
          ICENT PAC          CALL PAC(I,I,J,B)
● PACS THE N RIGHTMOST BITS OF 9 INTO A
. BITS ARE NUMBERED LEFT TO RIGHT FROM 0 - 59
* IF I LE J, N=J-I+1
. DESTINATION IS BITS I - J OF A
. IF I GT J, N=60-(I-J-1)
* DESTINATION IS BITS I - 59, 0 - J OF A
. BIT 59 OF B ALWAYS GOES TO 57 J OF A
. J. J. THOMAS 4/7/75

          ENTRY PAC
          VFD 42/0LPAC
          IFEQ ● F,2
          VFD 18/PAC          FTN ARGUMENT LINKAGE
PAC      BSSZ 1
          SB7 1              B7 = 1 (CONSTANT)
          SA2 A1+B7          GET ADDR SSES OF A - B IN X1 - X4
          SA3 A2+B7
          SA4 A3+B7
R        MICRO 1,1,$X5
          ELSE
          IFNE ● F?IP1
          ERR
          VFD 18/4          NOT CALLED BY RUN OR FTN
          BSSZ 1              RUN 2,3 ARGUMENT LINKAGE
          SB7 1              B7 = 1 (CONSTANT)
R        MICRO 1,1,$Z5
          ENDIF
          SA1 VRV.1          X1 = A
          SA2 VRV.2          X2 = I
          SA3 VRV.3          X3 = J
          SA4 VRV.4          X4 = B
          IX5 X3-X2          FIGURE NO. BITS - 1 TO PAC INTO A
          MX0 1
          PL X5,J1
          SX5 X5+60
J1       SB6 x5
          AX0 06              MAKE MASK OF CORRECT LENGTH IN RIGHT-MOST
          SB7 B6+B7          PART "OF WORD"
          LX0 $37
          BX4 X0*X4          EXTRACT BITS FROM B
          SB7 x3-59
          LX0 -87            ALIGN BITS FROM B AND MASK
          LX4 -B7            WITH CORRECT BITS OF A
          BX1 -X0*X1        INSERT BITS FROM B INTO A
          SX6 X1+X4
          SA6 A1              STORE A
          EO PAC             EXIT
          END
          ICENT UNPAC        CALL UNPAC(A,I,J,B)
" EXTRACTS N BITS A AND PLACES THEM
^ IN B, RIGHT-JUSTIFIED WITH ZERO FILL
* BITS ARE NUMBERED LEFT TO RIGHT FROM 0 - 59
* IF I LE J, N=J-I+1

```

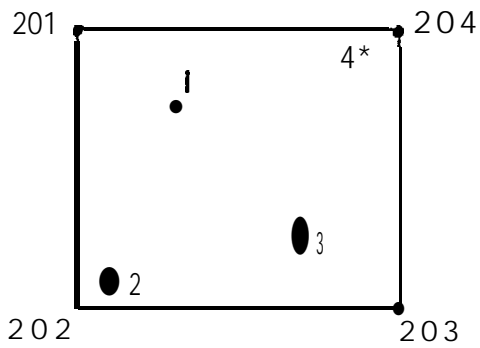

APPENDIX IV
 TRIANGLE SCHEME

The triangle routine used was originally devised by Smyth (1975) and later simplified by Galt. To demonstrate how it works, we use a simple 4 station example, shown below:



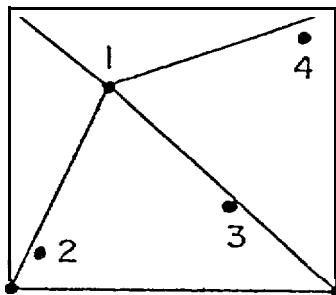
The 4 stations to be triangulated.

The first step is to enclose the region of interest by a rectangle:



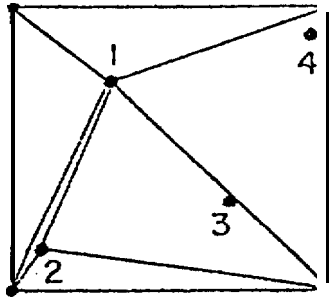
Rectangle defined by artificial points 201, 202, 203, and 204 enclose region of interest.

Next, take the first point and use that to subdivide the rectangle:



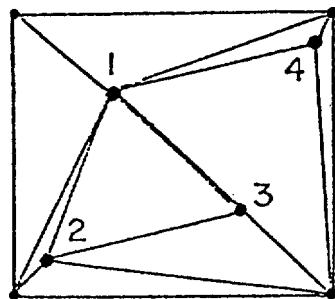
First subdivision of the initial triangle.

The second point is then used to subdivide the triangle it is in:



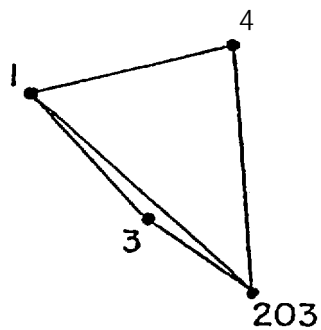
Second point used to subdivide the triangle.

After all of the points have been used to subdivide the larger triangles they lie in, we have:

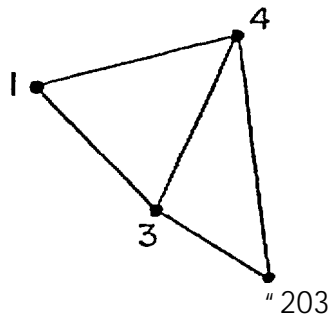


Mesh after all the subdivisions have been made.

Next, several sweeps are made to check the "goodness" of pairs of triangles. For example, the pair of triangles:

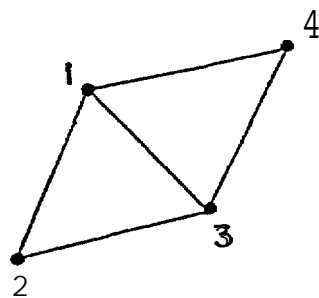


is checked to see if the triangles would be more equilateral if subdivided in the following way:



From tests run on a set of 130 stations and about 200 triangles, it was found that after about five sweeps through the entire mesh, the method converged and yielded a "best" mesh.

The last step in generating the mesh is to eliminate all triangles with corner vertices (201, 202, 203, 204). The final mesh is shown below:



Final mesh.

The routine has been written to accommodate up to 200 stations including one set of interior boundary points (an island). If there are interior boundary points, they must be read in first and in clockwise order.

To evaluate:

$$N_2 \iint_D \phi_j \nabla^2 \phi_i \, dx dy, \quad (A1)$$

Begin by evaluating

$$N_2 \iint_D \phi_j \frac{\partial^2 \phi_i}{\partial x^2} \, dx dy.$$

First integrate

$$\int \phi_j \frac{\partial^2 \phi_i}{\partial x^2} \, dx \quad (A2)$$

by parts to get

$$\int \phi_j \frac{\partial^2 \phi_i}{\partial x^2} \, dx dy = \phi_j \frac{\partial \phi_i}{\partial x} \Big| - \int \frac{\partial \phi_j}{\partial x} \frac{\partial \phi_i}{\partial x} \, dx \quad (A3)$$

Now integrate by $\int dy$ to get

$$N_2 \iint_D \phi_j \frac{\partial^2 \phi_i}{\partial x^2} \, dx dy = N_2 \left[\int \phi_j \frac{\partial \phi_i}{\partial x} \, dy - \iint \frac{\partial \phi_j}{\partial x} \frac{\partial \phi_i}{\partial x} \, dx dy \right] \quad (A4)$$

The second term of (A1) can be integrated by parts also, to give

$$N_2 \iint_D \phi_j \frac{\partial^2 \phi_i}{\partial y^2} \, dx dy = N_2 \left[\int \phi_j \frac{\partial \phi_i}{\partial y} \, dx - \iint_D \frac{\partial \phi_j}{\partial y} \frac{\partial \phi_i}{\partial y} \, dy dx \right] \quad (A5)$$

Putting (A4) and (A5) together gives

$$\begin{aligned} N_2 \iint_D \phi_j \nabla^2 \phi_i \, dx dy = N_2 \left[\int \phi_j \frac{\partial \phi_i}{\partial x} \, dy + \int \phi_j \frac{\partial \phi_i}{\partial y} \, dx \right. \\ \left. - \iint_D \left[\frac{\partial \phi_j}{\partial x} \frac{\partial \phi_i}{\partial x} + \frac{\partial \phi_j}{\partial y} \frac{\partial \phi_i}{\partial y} \right] \, dx dy \right] \quad (A6) \end{aligned}$$

Now use the following substitution into the first two terms on the right-hand side:

$$dy = \frac{\partial y}{\partial s} \, ds, \quad dx = \frac{\partial x}{\partial s} \, ds, \quad (A7)$$

To integrate $\int_{\Delta} \phi dx dy$

$$\phi = Ax + By + C \text{ such that}$$

$$\phi = 1 \text{ at } (X, Y) \text{ and}$$

$$\phi = 0 \text{ at } (0,0) \text{ and } (b,0)$$

Begin by integrating Part I first:

$$\phi = \left(\frac{y}{y_2}\right)$$

$$\delta x = \frac{x_2 - b}{y_2} y + (b - x_2)$$

$$\begin{aligned} \int_{\Delta I} \phi dx dy &= \int_0^{y_2} \left(\frac{y}{y_2}\right) \left(\frac{x_2 - b}{y_2} y + [b - x_2]\right) dy \\ &= (b - x_2) y_2 \frac{1}{6}. \end{aligned}$$

Now to integrate Part II:

$$\phi = \frac{y}{y_2}$$

$$\delta x = \frac{x_2}{y_2} y + x_2$$

$$\begin{aligned} \int_{\Delta II} \phi dx dy &= \int_0^{y_2} \left(\frac{y}{y_2}\right) \left(-\frac{x_2}{y_2} y + x_2\right) dy \\ &= x_2 y_2 \frac{1}{6} \end{aligned}$$

The combined results give

$$\begin{aligned} \int_A \phi dx dy &= \frac{1}{6} y_2 (b - x_2 + x_2) = \frac{1}{6} y_2 b \\ &= \frac{1}{3} (\text{area of triangle}). \end{aligned}$$