



NBS TECHNICAL NOTE **854**

U.S. DEPARTMENT OF COMMERCE / National Bureau of Standards

A System of Fortran IV Computer Programs for Crystal Structure Computations

QC
100
.U5753
no.854
1975
c.2

NATIONAL BUREAU OF STANDARDS

The National Bureau of Standards¹ was established by an act of Congress March 3, 1901. The Bureau's overall goal is to strengthen and advance the Nation's science and technology and facilitate their effective application for public benefit. To this end, the Bureau conducts research and provides: (1) a basis for the Nation's physical measurement system, (2) scientific and technological services for industry and government, (3) a technical basis for equity in trade, and (4) technical services to promote public safety. The Bureau consists of the Institute for Basic Standards, the Institute for Materials Research, the Institute for Applied Technology, the Institute for Computer Sciences and Technology, and the Office for Information Programs.

THE INSTITUTE FOR BASIC STANDARDS provides the central basis within the United States of a complete and consistent system of physical measurement; coordinates that system with measurement systems of other nations; and furnishes essential services leading to accurate and uniform physical measurements throughout the Nation's scientific community, industry, and commerce. The Institute consists of a Center for Radiation Research, an Office of Measurement Services and the following divisions:

Applied Mathematics — Electricity — Mechanics — Heat — Optical Physics — Nuclear Sciences² — Applied Radiation² — Quantum Electronics³ — Electromagnetics³ — Time and Frequency³ — Laboratory Astrophysics³ — Cryogenics³.

THE INSTITUTE FOR MATERIALS RESEARCH conducts materials research leading to improved methods of measurement, standards, and data on the properties of well-characterized materials needed by industry, commerce, educational institutions, and Government; provides advisory and research services to other Government agencies; and develops, produces, and distributes standard reference materials. The Institute consists of the Office of Standard Reference Materials and the following divisions:

Analytical Chemistry — Polymers — Metallurgy — Inorganic Materials — Reactor Radiation — Physical Chemistry.

THE INSTITUTE FOR APPLIED TECHNOLOGY provides technical services to promote the use of available technology and to facilitate technological innovation in industry and Government; cooperates with public and private organizations leading to the development of technological standards (including mandatory safety standards), codes and methods of test; and provides technical advice and services to Government agencies upon request. The Institute consists of a Center for Building Technology and the following divisions and offices:

Engineering and Product Standards — Weights and Measures — Invention and Innovation — Product Evaluation Technology — Electronic Technology — Technical Analysis — Measurement Engineering — Structures, Materials, and Life Safety⁴ — Building Environment⁴ — Technical Evaluation and Application⁴ — Fire Technology.

THE INSTITUTE FOR COMPUTER SCIENCES AND TECHNOLOGY conducts research and provides technical services designed to aid Government agencies in improving cost effectiveness in the conduct of their programs through the selection, acquisition, and effective utilization of automatic data processing equipment; and serves as the principal focus within the executive branch for the development of Federal standards for automatic data processing equipment, techniques, and computer languages. The Institute consists of the following divisions:

Computer Services — Systems and Software — Computer Systems Engineering — Information Technology.

THE OFFICE FOR INFORMATION PROGRAMS promotes optimum dissemination and accessibility of scientific information generated within NBS and other agencies of the Federal Government; promotes the development of the National Standard Reference Data System and a system of information analysis centers dealing with the broader aspects of the National Measurement System; provides appropriate services to ensure that the NBS staff has optimum accessibility to the scientific information of the world. The Office consists of the following organizational units:

Office of Standard Reference Data — Office of Information Activities — Office of Technical Publications — Library — Office of International Relations.

¹ Headquarters and Laboratories at Gaithersburg, Maryland, unless otherwise noted; mailing address Washington, D.C. 20234.

² Part of the Center for Radiation Research.

³ Located at Boulder, Colorado 80302.

⁴ Part of the Center for Building Technology.

at all.

2100

5753

854

275

1.2

A System of Fortran IV Computer Programs for Crystal Structure Computations

Larry W. Finger

Geophysical Laboratory
Carnegie Institution of Washington
Washington, D.C. 20008

and

² Technical note no. 854

E. Prince

^{U.S.}
... Institute for Materials Research
National Bureau of Standards
Washington, D.C. 20234



U.S. DEPARTMENT OF COMMERCE, Frederick B. Dent, *Secretary*
NATIONAL BUREAU OF STANDARDS, Richard W. Roberts, *Director*

Issued February 1975

National Bureau of Standards Technical Note 854

Nat. Bur. Stand. (U.S.), Tech. Note 854, 133 pages (Feb. 1975)

CODEN: NBTNAE

U.S. GOVERNMENT PRINTING OFFICE
WASHINGTON: 1975

For sale by the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402
(Order by SD Catalog No. C13.46:854). Price \$2.00

ABSTRACT

This report gives detailed descriptions and instructions for use of a system of programs for crystallographic calculations, including least-squares refinement with generalized systems of constraints, calculation of bond distances and angles with errors, Fourier synthesis, plotting of contours in Fourier maps, and preparation of structure factor tables for publication.

Key Words:

Computer programs; contour plotting; constrained refinement; crystallographic calculations; Fourier section; Fourier synthesis; least squares

This is also Paper Number 1651 from the Geophysical Laboratory, Carnegie Institution of Washington, Washington, D. C.

TABLE OF CONTENTS

	<u>Page</u>
RFINE4: A program for least squares refinement including general constraints.	1
General Description	1
File and Record Structure	1
Description of Routines	2
Common Blocks and Variables	11
Dependent Parameter Input	14
Details of Data Input	17
BONDAN: A program for computing bond distances, angles, and thermal ellipsoids, with errors.	27
FOURIER	29
LISTFC	32
CNTPLT	34
ARBSECT	37
References Cited	40
APPENDIX A - Overlay scheme for RFINE	41
APPENDIX B - BADTEA - alternate input for bond distances and angles, and thermal ellipsoids	42
APPENDIX C - Listings of programs.	56

These programs, although tested on many problems and several computing systems, may not give correct results in all circumstances. Therefore, neither the authors nor their institutions will guarantee the correctness of the program in all respects, but the authors will greatly appreciate being informed of discrepancies in the code or desirable options not currently included.

RFINE4: A program for least squares refinement
including general constraints

General Description

This program, called RFINE4, performs the calculations necessary to refine crystal structures using the techniques of full-matrix least-squares refinement. In addition, it can compute bond distances and angles or thermal ellipsoids so that these functions may be monitored throughout the various stages of a refinement. File control capabilities have been designed so that parameters may be saved at the end of a given computer run or, alternatively, virtually any parameter may be changed at almost any time.

A scheme of derivative modification and parameter restoration which eliminates the need for coding special subroutines to treat constrained parameters has been included in this program. This method will handle thermal and positional restrictions for atoms in positions of special symmetry and, in conjunction with the occupancy refinement capability, a multiposition, partially ordered structure may be constrained to a particular chemical composition. Provision has been made for incorporating parameters which are not members of the set used in conventional least-squares refinement. Any set of linear constraints may be specified, and also groups of atoms may be treated as rigid bodies both with respect to position and orientation (shape constraints) and with respect to thermal motion.

In its present form, the program allows a maximum of 60 atoms, 20 chemical species, 10 scale factors, 1320 parameter dependencies and 200 refined parameters for a structure in any space group. With the maximum number of parameters and no use of overlays the program requires approximately 65000 words of core storage. However more restricted problems can be operated in smaller core sizes, and the program can be further reduced in size by means of overlays. A suggested overlay structure is given in Appendix A. Some operating systems allow for dynamic allocation of core. Such provisions can be used to advantage.

File and Record Structure

In the following discussion a record is the unit of information formally defined as a logical record, i.e. the amount of information transferred in a single non-formatted read or write statement. This description is independent of any physical device which may be associated with the file and the program has been coded so as to operate fairly efficiently with any type of auxiliary storage currently available. Furthermore, a data set shall mean the collection of records needed to describe a structure. Any reference to file or data labels should not be confused with file control information for a particular computer system.

Master File. The file referred to as ISC1 and assigned to logical unit 10 is the main file of the program. This file consists of a data set containing all the information required to resume least-squares refinement. This data set has two label records, one or more structure factor records, a constraint relations record, a variance-covariance record, and a record containing variances of previously refined parameters (useful in large problems where the refinement must be "blocked"). The label records contain a 12-character alphanumeric identification tag, a cycle number and all the atom parameters, symmetry data and scattering factor information needed for this structure. The reflection data consist of the Miller indices, the observed structure factor on a relative scale, the standard deviation of F_{obs} , the value of $\sin^2\theta/\lambda^2$ for the reflection, an integer specifying which scale factor applies to this reflection, β --the extinction parameter, a flag to mark reflections which had an intensity less than the minimum observable, the diffractometer angles χ , ϕ and $\omega + \theta$ in radians, and the value of each of the scattering curves for this reflection. These quantities are packed into a buffer, starting with word 2, until another reflection would require the buffer to be larger than 1023 words. An end of reflection records marker, which is non-zero only in the last block, is contained in word 1. The information for a single reflection is never split between two records and all records, including the last which may be only partially filled, are the same length. The end of the reflection list is marked by a Miller index h having a value of 3000. If the number of scattering curves is N, the number of reflections per record (n) may be found from the integral part of $1022/(\text{N} + 12)$. The length of the record is then 1023 minus 1022 modulo n. The variance-covariance record contains the variance-covariance matrix for the previous cycle of refinement in packed, upper triangular format.

Intermediate File. This file, named ISC2 and assigned to logical unit 29, contains the structure factor records for the current structure. A distinct file allows the scattering factor information to be changed without reading the structure factors from cards.

Auxiliary Files. A file named ISC3 and assigned to logical unit 11 is used as an alternative structure factor input. A file named ISC4 and assigned to logical unit 12 is used to pass information to Fourier synthesis, structure factor tabulation and statistical analysis programs. A file named ISC5 and assigned to logical unit 28 is used for temporary storage of constraint relationships.

System Files. This program uses a file named IN, logical unit 5, as a card read file, a file named IOUT, logical unit 6, as the print file, and a file named IPUN, logical unit 1, as the punch file. These assignments may be changed for a particular system by a block data subprogram.

Description of Routines

Main Program. The main program serves as a driver for the least-squares section. It reads one card which contains a 12-character label.

If a new data set is being constructed, this label will be inserted into that file. Control is then transferred to subroutine RFINE. If the updated information is written back to file ISCL, the subroutine exits normally. In that event, the main program prints a message stating that the file has been updated.

Subroutine RFINE. This routine is the primary one for the structure factor and least-squares calculation and is responsible for controlling the functions computed and the parameters used.

When this routine is first entered, initialization is accomplished and the main cycle loop is entered. The first step is to read the title and control cards for the cycle. If this is the first cycle of the current run, the new parameter indicators from the control card are interrogated and if all are non-zero, signifying that all parameters are to be loaded from cards, the data set on file ISCL is presumed not to exist; however, if any of the indicators are zero, the first two records of that data set are loaded into memory. Next, any new parameters required are read from cards. As new parameters are read, the values are printed.

If the unit cell parameters are to be changed, that card is read and the direct space metric tensor is prepared. This is a 3×3 symmetric matrix whose elements are the scalar products of the unit cell vectors. This matrix is then inverted using subroutine SYMINV described below. The inverse matrix is then the reciprocal space metric tensor and the determinant of the original matrix is the square of the unit cell volume. Note: If the unit cell parameters are to be changed, the structure factors must also be changed if the effects of the cell data are to be applied to the values of $\sin \theta/\lambda$.

New symmetry cards, if required, are now read. Each card lists an equivalent position in very nearly the same form as Vol. I of the International Tables with only one major difference; positions related by a center of inversion or lattice centering must not be included since they are internally generated. Using this scheme, all space groups may be generated by using a maximum of 24 cards. Each symmetry data card is transformed into matrices R and T satisfying the equation

$$X' = RX + T$$

with X' equal to the vector of transformed coordinates, X is the position vector with components, xyz, R is a 3×3 rotational matrix and T is a vector describing the translation associated with this symmetry operation.

At this point in the program, new scattering factor coefficients are read, if desired. We must emphasize two points of caution concerning the changing of the scattering factors. First, since the blocking of structure factors depends upon the number of scattering factors used, if that number is changed, new structure factors must be read. Violation of this rule will lead to unpredictable, but probably catastrophic, results. The second rule requires that the scattering factors be changed

only when file ISC2 is being written, that is, either on the first cycle of a given run or when new structure factors are being read from cards. If this restriction is violated, the new curves are loaded to core and subsequently included in the data set for this structure, but they are never used to compute scattering factors for the reflections.

The new atom parameters, if required, are now read from cards. The scale factors are read first, followed by the extinction parameters and the atom cards. The atom parameters needed are an identification label of 6 characters, an equipoint fraction which is the multiplicity of the position occupied by this atom divided by the multiplicity of an atom in the general position of this space group, the total occupancy of the site (usually one), the occupancy of species A (needed if more than one species present in this site), the identification of scattering factor(s) to be applied to this atom, fractional coordinates for the atom, and temperature factor information, as well as third and fourth cumulant parameters, consistent with the temperature factor type card described below. The forms of the cumulant expressions used in this program are:

$$F = \sum_j f_j \exp[i(2\pi \sum_k h_k x_k^j - \sum_{klm} \sum_k h_k h_l h_m c_{klm} - \sum_{kl} (h_k h_l \beta_{kl}^j - \sum_{mn} \sum_j h_j h_l h_m h_n h_{klmn}^j))]]$$

atoms

x_k^j is the k^{th} fractional coordinate of atom j , β is the array of anisotropic thermal coefficients, and c and d are the arrays of third and fourth cumulant coefficients. After the atom parameter cards have been read, the special parameter cards are read. The first card gives the total number of special parameters (up to 60). Then one card for each special parameter contains its name, three integers specifying its type, and its initial value.

At this point in the program, the parameter refinement selection information is read. A parameter of the model is varied in the least-squares refinement if its associated indicator is one; parameters with zero indicators are changed only if they are linked to refined parameters by dependency cards. If new parameter selection information is read, constraint data are also read. If no dependency relationships exist for this structure, a blank card must be included in the data deck. The method used to treat parameter constraints is from Finger (1969) and essentially consists of the application of the chain rule to the derivatives of the structure factor with respect to the parameters of the model. The user must determine the dependent parameters of the model using the rules of Levy (1956) for thermal coefficients or the equations of Finger (1969) for chemical constraints and then prepare the data cards. The program currently will not allow the constraining of the total occupancy for a site with only one species present; however, this may be accomplished by including a null scattering curve which is made the second species present. The amount of the first species may then be refined and constrained.

At this point, all structural data except the observed structure factors have been read. If these are to be read, a data card containing a FORMAT specification is read. Two optional cards may be read, one to specify the wavelength if it is needed for the computation of extinction corrections and the other to specify an "ignorance factor", ρ , to be used in computing weights according to the formula

$$w = 1/[\sigma^2 + (\rho F_{\text{obs}})^2].$$

Subsequently, the subroutine INPUT is called to read and process a reflection card. The data are then added to a buffer which, if full, is output on file ISC2. If the old structure factors are desired and this is the first cycle of a given computer run, the buffer is filled from file ISC1, the scattering factors are recomputed if necessary and the buffer is written on file ISC2. If this is not the first cycle of a given run, the old structure factors are read from file ISC2. After the data for a reflection have been obtained, the calculated structure factor and partial derivatives are computed in subroutine SFAC, the results tested to determine if this reflection should be used in the normal equations matrix, and the contributions of this reflection to the residuals are calculated. Next, the structure factors are printed, if desired, with the rejected data marked with a single asterisk in the right margin. In addition, the reflections having intensities less than the minimum observable value are marked with a single asterisk next to the value of F_{obs} and a double asterisk in the right margin.

If the reflection is to be included in the matrices, subroutine MATRIX is entered; then the next observation is processed. As soon as the end of the reflection list is encountered, the residuals for this cycle are printed. Next, the normal equations matrices are converted to correlation matrices to prevent overflow or underflow of the determinant during the matrix inversion, which is accomplished by subroutine SYMINV, adapted from Busing and Levy (1962). If the matrix is non-singular, the inverse is converted to a variance-covariance matrix and the parameter shifts are computed. Subroutine RESET is entered to compute the new values of any dependent parameters. The ratios of the parameter shifts to the standard deviations are tested to find the largest absolute value and the magnitudes of the ratios are averaged. At this point in the program, the correlation matrix, if requested, is printed. The twenty off-diagonal elements of the correlation matrix with largest absolute values are always printed. Then the optional bond functions are computed by routine BODAN1 and the thermal functions by routine ELVIB1.

Finally, a run continuation card is read. If column 1 is non-zero, another cycle is to be performed. However, if this column is blank or zero, the program prepares to terminate. If the new values for the parameters are not to be saved, the program exits. On the other hand, if these parameters are to be kept, a new label record is written on ISC1, the structure factor records are copied from ISC2 to ISC1 and the variance-covariance record is output. The current values of all parameters may be punched on cards. This routine then returns control to the main program.

Subroutine BODAN1. This subroutine uses the symmetry operators supplied on cards combined with the action of centers of symmetry, if present, and the effects of multiple lattice points and cell translations to generate all atomic locations within a spherical shell centered on each atom in the asymmetric unit. The search for the contents of this shell is done efficiently by enclosing the central atom with a unit cell shaped parallelpiped tangent to the sphere. For each location inside this box, a table of generated positions is checked to determine if this location is unique and if it is, the bond distance is computed. If this is within the desired range, the distance and coordinates are printed and this location is added to the table of generated positions.

If bond angles are also desired, each atom in the asymmetric unit is used as the central atom with the atom positions generated in the bond distance calculation considered. The peripheral atoms are identified only by their alphanumeric tag and a number which points to an entry in the bond distance output where the coordinates of the generated atom are listed. Caution--if the maximum bond distance is large, very many angles will be generated.

Subroutine ELVIB1. For each anisotropic atom, the equivalent isotropic temperature factor of Hamilton (1959), the root-mean-square (rms) amplitudes of vibration (in Å) of the principal axes and the orientations of these axes with respect to the direct cell axes are computed, or if the temperature factor matrix of an atom is nonpositive-definite, this is reported. This routine will also compute the thermal corrections to bonds using the formulae of Busing and Levy (1964). To assist the interpretation of the orientations of thermal ellipsoids relative to the bonding, the rms amplitude of the ellipsoid in the direction of the bond is computed and printed. BODAN1 is used to generate the necessary atomic locations.

Subroutine INPUT. This subroutine reads a reflection data card, computes $\sin^2\theta/\lambda^2$, evaluates the scattering factors for this observation and computes σ_F for the observation. Maximum and minimum values of F_{obs} and $\sin^2\theta/\lambda^2$, are determined in this routine.

Subroutine MATRIX. This subroutine calculates the derivatives of the residual from the derivatives of the calculated structure factor and accumulates the sums required in the normal equations matrices.

Subroutine MODIFY. This routine applies the equations

$$\frac{\partial A}{\partial p_n} = \sum_m \frac{\partial A}{\partial p_m} \frac{\partial p_m}{\partial p_n}$$

and

$$\frac{\partial B}{\partial p_n} = \sum_m \frac{\partial B}{\partial p_m} \frac{\partial p_m}{\partial p_n}$$

to the calculated derivatives. A and B are the real and imaginary portions of the calculated structure factor, p_n is the independent parameter, p_m

represents a dependent parameter, the summation is over all the dependencies, the unprimed derivative denotes the one calculated without regard for dependencies and the primed derivative is needed to form the least-squares matrices.

Subroutine RCALC. This subroutine accumulates the terms needed to calculate the discrepancy factors which are computed for all reflections and separately for those data used in the refinement. A weighted residual, R_w which is computed using the formula

$$R_w^2 = \frac{\sum w (|F_o| - |F_c|)^2}{\sum w |F_o|^2}$$

for refinement on F or

$$R_w^2 = \frac{\sum w (|F_o|^2 - |F_c|^2)^2}{\sum w |F_o|^4}$$

for refinement on F^2 , is determined for each class of data. In addition, the conventional discrepancy index

$$R = \frac{\sum ||F_o| - |F_c||}{\sum |F_o|}$$

is computed for all reflections in each class. In addition, the ranges of variation of F and $\sin^2\theta/\lambda^2$ are each divided into eight subranges and the sums needed for R are accumulated. (Note: the maximum and minimum values are dynamically determined during any cycle in which new structure factors are read and the distribution of residuals for such a cycle will be meaningless.) If the weighting scheme is correct, the expression $(1/s) \sum w (F_o - F_c)^2$, where the sum is taken over a subset of the full data set containing s reflections, should be independent of the composition of the subset. If we divide this expression by the constant $(1/t) \sum w F_o^2$, where t is the total number of reflections in the data set and the sum is taken over the entire set, and take the square root of the quotient, the result should also be independent of the composition of the subset. This number, which can be considered the average contribution to weighted R for reflections in the subset (Note that the expression is equal to weighted R if $s=t$.) is printed in the output for each subset.

Subroutine RESET. This subroutine is entered once for special parameters and once for each atom to compute the updated values of all dependent parameters. Linear relationships and rigid-body parameters are computed directly. Other non-linear systems of constraints may be handled by the user through subroutine SPVAL, supplied as a dummy.

Subroutine SFAC. This subroutine computes the structure factor and partial derivatives with the symmetry operators applied to reciprocal space; i.e. the Miller indices are transformed rather than the atomic coordinates. If H^T represents the transpose of the vector of Miller indices and X'_{nj}

represents the j th symmetry transformed coordinate for the n th atom, then the argument of the trigonometric functions needed to calculate the contribution of this atom to the structure factor may be written as $H^T X'_{nj}$. Utilizing the expression for X' from page 3,

$$H^T X' = H^T (RX + T) = H^T RX + H^T T.$$

The final form is the method used in this subroutine.

As the routine is entered for each reflection, the matrix products $H^T R_j = H_j^T$ and $H^T T_j$ are computed and saved. Then the structure factors and partial derivatives are accumulated. If 3rd and 4th cumulant terms are absent, the structure factor

$$F = \sum_n a_n f_n \sum_j T_{nj} P_{nj}$$

with

$$P_{nj} = \exp [2\pi i (H_j^T X_n + H^T T_j)]$$

and

$$T_{nj} = \exp (-H_j^T \beta_n H'_j)$$

for anisotropic atoms or

$$T_{nj} = \exp (-B_n \sin^2 \theta / \lambda^2)$$

for isotropic atoms, the n summation is over the atoms in the asymmetric unit, the j summation is over the symmetry operators, a_n is an occupancy term, f_n is the value of the scattering curve for the n th atom, i is $\sqrt{-1}$ and β_n is the matrix of anisotropic thermal coefficients. When anomalous dispersion is included, the scattering factor becomes

$$f_n = f_{on} + f'_n + if''_n$$

with f_{on} the wave length independent part, f'_n the real part of the anomalous dispersion and f''_n the imaginary part. Including this expression in the structure factor equation, applying Euler's rule and writing F in the form $F = A + iB$, we find that

$$A = \sum_n \left[a_n (f_{on} + f'_n) \sum_j T_{nj} \cos 2\pi (H_j^T X_n + H^T T_j) - a_n f''_n \sum_j T_{nj} \sin 2\pi (H_j^T X_n + H^T T_j) \right]$$

and

$$B = \sum_n \left[a_n (f_{o_n} + f'_n) \sum_j \sin 2\pi (H'_j T_{X_n} + H^T T_j) \right. \\ \left. + a_n f''_n \sum_j \cos 2\pi (H'_j T_{X_n} + H^T T_j) \right].$$

The required partial derivatives are found by differentiating each of the above equations with respect to the components of X_n and β_j . After all sums have been accumulated, the subroutine MODIFY is called to perform any chainrule operations required. If this is to function properly, all derivatives must be calculated although the refinement indicators would suggest that certain derivatives are not needed.

Subroutine SFAC also includes an entry point named EXCALC which calculates the extinction factor of Zachariasen (1967) as extended by Coppens and Hamilton (1970), and revised by Nelmes and Thornley (1973). Using this scheme, the structure factor is corrected for extinction by the relationship

$$F_c^* = F_c y^{1/2} \\ y = (1 + \beta(\theta) F_c^2 r^*)^{-1/2} \\ \beta(\theta) = \begin{cases} \frac{-2 e^4}{m^2 c^4 V^2 A \sin 2\theta} \frac{(1 + \cos^4 2\theta)}{(1 + \cos^2 2\theta)} \frac{dA}{d\mu} & \text{for x-rays} \\ \frac{\lambda^2}{V^2 A \sin 2\theta} \frac{dA}{d\mu} & \text{for neutrons} \end{cases}$$

λ is the wavelength, V is the cell volume, A is the transmission factor, μ is the linear absorption coefficient, and e , m and c have their usual meanings. The program allows three different forms for the extinction; a) isotropic with r^* refined, b) Type I anisotropic with $r^* = (D^2 ZD)^{-1/2}$ with z_{ij} refined and c) Type II anisotropic with $r^* = (N^2 W N)^{-1/2}$ with W_{ij} refined. If $\bar{p}$ is a unit vector parallel to the incident beam and $\bar{s}$ is a unit vector parallel to the diffracted beam, $\bar{D}$ is a unit vector parallel to $\bar{p} \times \bar{s}$ and $\bar{N} = \bar{p} \times \bar{D}$. The reference coordinate system for Z and W is attached to the crystal and has its x -axis parallel to the incident beam and its z axis vertical when all diffractometer angles are 0.

Subroutine SYMINV. The method used by this matrix inversion routine has been described by Busing and Levy (1962) and was coded by Mr. James Mundstock of the Numerical Analysis Center of the University of Minnesota.

Subroutine REJECT. This routine may be used to exclude reflections from the normal equations matrices for other than the standard reasons. If a reflection is to be rejected, the variable NREJ in Common Block /F/ should be set to one.

Subroutine WEIGHT. This routine may be used to compute a non-standard weighting scheme. Upon entry, the information contained in the standard deviation field of the structure factor card will be in the variable WT in Common Block /F/. This variable must be set to the desired weight information when the routine is exited.

Subroutine RDEGN. This subroutine reads the dependent parameter information from cards, and rearranges the array of relationships in ascending order first of independent atom and parameter designators and then of dependent atom and parameter designators. Special parameters are arbitrarily assigned atom number 0.

Subroutine DERIVS. This subroutine is entered once at the beginning of each cycle. It computes the current values of derivatives of conventional parameters with respect to rigid body parameters. (Other non-linear derivatives may be supplied by the user through subroutine SPDERI). If any independent parameters are themselves actually dependent on other parameters (such as when the values of the elements of the rigid-body motion tensors are restricted by symmetry) the derivatives with respect to the true independent parameters are computed. Then the independent parameter designators are replaced by their row indices in the normal equations matrix, and the array is packed to eliminate any redundant relations.

Subroutine PAREXT. This subroutine reads the special parameter cards, and prints the names and initial values of the parameters.

Subroutine TRNFRM. This subroutine is entered once at the beginning of a run to compute the transformation matrices required to convert parameters from the crystal system to a standard orthonormal coordinate system and back again.

Subroutine FILLIN. This subroutine stores special parameter values in the proper positions in rigid-body parameter arrays.

Function ERRCAL. This function subroutine determines the standard deviation of a dependent parameter according to the approximate formula

$$\sigma_k' = \left(\sum_{i=1}^n \sum_{j=1}^n \frac{\partial P_k}{\partial P_i} \frac{\partial P_k}{\partial P_j} \sigma_{ij} \right)^{1/2},$$

where n is the number of refined parameters and σ_{ij} is the covariance of the ith refined parameter with the jth refined parameter.

Subroutine EULER. This subroutine computes an orthogonal matrix which is necessary to transform parameters from a general orthonormal coordinate system to the standard orthonormal coordinate system defined by x parallel to $\underline{a}$ and z parallel to $\underline{c}^*$. The relative orientations are defined by Eulerian angles ϕ, χ , and ω . Here ω is the angle through which the special coordinate system must be rotated clockwise, as viewed down the positive z axis of the standard system, about the z axis of

the standard system to bring the z axis of the special system into the x-z plane of the standard system; χ is a clockwise rotation about the y axis of the standard system (viewed down the positive y axis) to bring the z axes of the two systems into coincidence; ϕ is a clockwise rotation about the common z axis to bring the x and y axes into coincidence. Three additional entry points, DTDPHI, DTDCHI, and DTDOMG compute the derivatives of the elements of the transformation with respect to ϕ , χ , and ω respectively.

Subroutine MULMM. This subroutine forms the product of two 3 x 3 matrices. An alternate entry, MULMV, multiplies a three component column vector by a 3 x 3 matrix.

Subroutine TFM. This subroutine has two entry points. TFM2 transforms a second cumulant tensor in an orthonormal system to a set of anisotropic temperature factors in the crystal system. TFM3 does the same for a third cumulant tensor.

Subroutine TRNSPS. This subroutine generates the transpose of a 3 x 3 matrix.

Function IPAK. This function packs 4 integer variables into a single computer word. The version given is appropriate only to the UNIVAC 1108. Other versions must be used for other machines. If the integer word length of the machine is shorter than 32 bits other adjustments must be made.

Functions SKTLS, D2KDT, D2KDL, and D2KDS. These functions compute the second cumulants for an atom and their derivatives with respect to the rigid body motion parameters T , L , and S .

Functions TKTLS, D3KDL, and D3KDS. compute the third cumulants and their derivatives with respect to L and S .

Subroutine CORECT. This subroutine applies libration corrections to the atomic positions in a rigid body.

Function DETERM and subroutine SOLVE are used by CORECT. Subroutine VXV forms the vector product of two vectors. Functions AIJ, BIJK, CIJKL, DIJKLM, EIJ, FIJ, AXA, AXAXB, PIJKLM, EL4. are a set of functions used in the rigid body relations.

Common Blocks and Variables

1. Common Block /LSMAT/

B(200)	Normal equations vector
IEXT	Extinction type indicator
IPARA (1000)	Atom Parameter refinement indicators
MRANK	Order of the normal equations matrices
KCYL	Cycle number for the data set
LABEL (3)	12 character label for the data set

JSCRF (10)	Refinement switches for scale factors
NRSF	Number of scale factors refined
SIGMA	Standard deviation of a parameter
MDEGN	Twice the number of constraint relationships
A(22740)	Constraints array and normal equations matrix or inverse. The dimensions are a maximum. The actual number for a given problem is given by the expression $MDEGN + (MRANK * (MRANK + 1)) / 2$. If, as on the UNIVAC 1108, the operating system allows dynamic core allocation, this number can be determined at run time.

2. Common Block /A/:

BETA(6,60)	Temperature factor coefficients
G(3,3)	Real space metric tensor
ISOT(60)	Temperature factor type indicators
NATOM	Number of atoms in the asymmetric unit
TAG(2,60)	Alphanumeric atom tags or labels
TITLE(18)	Alphanumeric title information
XYZ(3,60)	Atomic positions
PI	Value of π
CR(10,60)	Third cumulant coefficients
DR(15,60)	Fourth cumulant coefficients

3. Common Block /C/:

CELLP(3,4)	Coordinates of lattice points
ICENT	Centric indicator
JCELL	Number of lattice points
NSYM	Number of symmetry operators
RMAT(3,3,24)	Rotational symmetry operators
TRANS(3,24)	Translational symmetry operators

4. Common Block /D/:

ACALC	Real part of calculated structure factor
AIND(60)	Individual atom contributions to ACALC
ANOM(2,20)	Anomalous dispersion corrections
BCALC	Imaginary part of calculated structure factor
BIND(60)	Individual atom contributions to BCALC
DADB(6,60)	Derivatives of ACALC with respect to temperature factors
DADO(60)	Derivatives of ACALC with respect to occupancy
DADX(3,60)	Derivatives of ACALC with respect to position
DBDB(6,60)	Derivatives of BCALC with respect to temperature factor
DBDO(60)	Derivatives of BCALC with respect to occupancy
DBDX(3,60)	Derivatives of BCALC with respect to position

H(3)	Miller indices in real representation
IH(3)	Miller indices in integer representation
ISCAT(2,60)	Table used to select atomic scattering factor
ISCL	Number of scale factor for this reflection
MFSEL	Function selector
OCCA(60)	Occupancy of species A
OCCUP(60)	Total occupancy of site
SCALE(10)	Scale factors
SCAT(20)	Values of scattering factor for current reflection
SITE(60)	Equipoint fraction for atom site
DADC(10,60)	Derivatives of ACALC with respect to 3rd cumulant
DBDC(10,60)	Derivatives of BCALC with respect to 3rd cumulant
DADD(15,60)	Derivatives of ACALC with respect to 4th cumulant
DBDD(15,60)	Derivatives of BCALC with respect to 4th cumulant
AMINUS	ACALC for opposite absolute orientation
BMINUS	BCALC for opposite absolute orientation
DRDE(6)	Derivatives of r^* (extinction factor) with respect to coefficients of tensor
NDEGN	Number of constraint relationships

5. Common Block /E/:

DMAX	Maximum bond distance
DMIN	Minimum bond distance
RECELL(6)	Reciprocal cell lengths and cosines
EXANG(3)	ϕ , χ and $\Theta + \omega$ (in radians) for current reflection

6. Common Block /F/:

DELTA	Weighted residual for current reflection
FCALC	Calculated structure factor
FOBS	Observed structure factor
FOMAX	Maximum observed structure factor
FOMIN	Minimum observed structure factor
IREJ	Rejection mode indicator
MREF	Refinement mode indicator
MREJ	Minimum observable indicator
NREJ	Used to indicate whether or not a reflection is rejected
NUMBER(36)	Counters for subdivisions of R factors
RDEN(36)	Denominators for R factors
RHO	Current value of $\sin^2\theta/\lambda^2$
RHOMN	Minimum value of RHO
RHOMX	Maximum value of RHO
RNUM(36)	Numerators for R factors

WT	Weight for current reflection
EXBETA	Factor $\beta(\theta)$ for extinction correction
EXX	Factor $\beta(\theta)F^2r^*$ used in extinction
EXY	$(1 + EXX)^{-1/2}$
FISGN	Absolute orientation parameter
IFSGN	Orientation determination indicator
EXTIN(6)	Extinction parameter matrix
KEXTRF(60)	Refinement switches for extinction parameters
DELMAX	Maximum permitted value of $\Delta F/\sigma_F$

7. Common Block /G/:

BUFF(1023)	Array used primarily for blocking structure factor records
FCURVE(9,20)	Scattering curve coefficients
FRMT(18)	Variable format specification for reading structure factors
IWT	Weight calculation type indicator
NSCAT	Number of scattering factors
BETFAC	Used in extinction correction
WVLNTH	Wavelength of radiation
WTFAC	"Ignorance factor" in computation of weights

8. Common Block /TAPE/:

IN	Logical unit number of the card read unit (5)
INN	Logical unit number of the structure factor input unit (5 or 11)
IOUT	Logical unit number of the print file (6)
ISC1	Logical unit number of the least-squares file (10)
ISC2	Logical unit number of the intermediate file (29)
ISC3	Logical unit number of the auxillary file (11)
ISC4	Logical unit number of the Fourier file (12)
ISC5	Logical unit number for saving constraints list (28)
IPUN	Logical unit number for punch file (1)

Dependent Parameter Input

In certain structures, the parameters of the model may not be independently variable. If they are merely constrained to have a fixed value, there are no difficulties as the refinement selection variable for this parameter is set to zero. However, if a parameter of the model is required to be equal to a linear combination of variable quantities, the situation is greatly complicated. In the least-squares refinement of such a structure, the contribution of the dependent parameter to the derivative of the structure factor with respect to the independent variable must be computed if the shifts are to be properly evaluated.

Similarly, the correct value of the dependent parameter must be restored at the end of the cycle if the structure factors are to be properly computed in the next cycle. This program utilizes a new algorithm to perform the derivative modification and parameter restoration. The method of preparing the input data cards will be shown with the aid of examples.

Example 1: Atom 6 is an anisotropic atom on a 3-fold axis parallel to c. Employing the rules of Levy (1956), the following relationships are required for this atom:

$$\beta_{13} = \beta_{23} = 0$$

$$\beta_{11} = \beta_{22} = 2 \beta_{12}$$

The first equations relate parameters to a constant and thus may be ignored. However, this is not the case for the second, and since β_{11} must be the independent variable, the following equations are applied as constraints to the least-squares solutions:

$$\beta_{22} = \beta_{11}$$

$$\beta_{12} = 1/2 \beta_{11}.$$

The resulting Parameter Constraint Cards (See page 24) for this situation would be:

<u>Dependent</u>	<u>Independent</u>	<u>Constant</u>	<u>Comments (not on card)</u>
6 6	6 5	1.0	$\beta_{22} = \beta_{11}$ for atom 6
6 8	6 5	0.5	$\beta_{12} = 0.5 \beta_{11}$
0			End of list

Example 2: Grunerite has four independent sites (atoms 1 to 4) for Fe and Mg, but the total amount of each is known from the chemical analysis. Therefore, we want to refine the values of the Mg-occupancies for the first three atoms and constrain the fourth to agree with the bulk chemistry. In the notation of Finger (1969), the constraining equation is

$$\sum_m b_m a_{mn} = C_n$$

with b_m the multiplicity of the m th site, a_{mn} the fractional occupancy for the n th species in the m th site, and C_n the total number of atoms of species n per unit cell. In grunerite, sites 1 through 4 have multiplicities 4, 4, 2, and 4 respectively and there are two formula units per unit cell. If we constrain the formula to be $\text{Fe}_{6.2}\text{Mg}_{0.8}\text{Si}_8\text{O}_{22}(\text{OH})_2$ and substitute into the above equation, we find that

$$4a_{1Mg} + 4a_{2Mg} + 2a_{3Mg} + 4a_{4Mg} = 1.6$$

Solving for a_{4Mg} ,

$$a_{4Mg} = 0.4 - a_{1Mg} - a_{2Mg} - 1/2 a_{3Mg}.$$

The Parameter Dependency Cards needed to constrain this chemistry would be:

Dependent	Independent	Constant	Comments (not on card)
4 1	0 0	0.40	Initialization
4 1	1 1	-1.0	Site 1 dependence
4 1	2 1	-1.0	Site 2
4 1	3 1	-0.5	Site 3
0			End of list

Alternatively, the latest version allows up to 5 independent parameters to affect one dependent one on the same card, so the first four cards above may be replaced by the card as follows:

4 1 0 0 0.40 1 1 -1.0 2 1 -1.0 3 1 -0.5

Note that when occupancies are constrained, the dependent value must first be initialized with a card containing zeros in the independent parameter fields.

Example 3: Like many chemical groups, phosphate groups often have thermal vibration that can be represented by the motions of a rigid body, which can be expressed as the elements of the $\underline{T}$, $\underline{L}$, and $\underline{S}$ tensors introduced by Schomaker and Trueblood (1969). Expressions for the second and third cumulants of the probability distribution functions for individual atoms (Johnson, 1969) as functions of the elements of $\underline{T}$ and $\underline{L}$ are given by Prince and Finger (1973), and the corresponding expressions including $\underline{S}$ can be readily derived (Prince, unpublished but given as a FORTRAN expression in this program). If atom 3 is an oxygen atom of a phosphate group and special parameters 1 through 24 are 3 coordinates of the origin to which the motions are referred, 6 elements of $\underline{T}$, 6 elements of $\underline{L}$, and 9 elements of $\underline{S}$, the constraint cards will be set up as follows: First, because of the so called "trace of $\underline{S}$ singularity", the three diagonal elements of $\underline{S}$ are not independent, and S_{33} can be set equal to $-S_{11} - S_{22}$ by means of the card 0 18 0 16 -1. 0 17 -1. The anisotropic temperature factors may depend on all of the rigid body elements, so there must be six cards of the form

3 5	0 4	0.	0-24	0.
3 6	0 4	0.	0-24	0.
3 7	0 4	0.	0-24	0.
3 8	0 4	0.	0-24	0.
3 9	0 4	0.	0-24	0.
3 10	0 4	0.	0-24	0.

Here the minus sign before the 24 indicates that the dependent parameter depends on special parameters 4 through 24 inclusive. The coefficients are given as zeros because, being non-linear, they change from cycle to cycle and are therefore computed in each cycle according to the current values of the refined parameters. Third cumulants are independent of $\underline{T}$, but may be dependent on any element of $\underline{L}$ or $\underline{S}$. Therefore a typical constraint card for a third cumulant would have the form

3 12 0 10 -0. 0-24 0.

The program uses the information on the constraint cards to allocate space in any array and then, in non-linear cases, fills in the space at the beginning of each cycle. Therefore if a given relationship is not listed it will never be used whether or not its value is actually zero. Because of symmetry some relationships, particularly those involving $\underline{T}$, may be identically zero. It will save space and almost certainly time to omit these from the list.

Details of Data Input

1. File Name Card: Columns 1-12 contain an alphanumeric label to be written into a new data set. This label will be printed when the file is read.
2. Title Card: Any desired Hollerith information in columns 1-72. This information appears at the top of most pages of the output.
3. Control Card:

<u>Column</u>	<u>Variable</u>	<u>Description</u>
1	MFSEL	Function selector 0 - Structure factors only 1 - Least-squares refinement
2	MSF	Structure factor output selector 0 - No structure factor output 1 - Printed structure factors 2 - Printed and written (for a Fourier program) on file ISC4 3 - Written on file ISC4
3	MCORR	Correlation matrix* 0 - Not printed 1 - Printed
4	MBODAN	Bond distance, angle selector 0 - None computed 1 - Distances only 2 - Distances and angles computed
5	MELVIB	Ellipsoids of vibration 0 - None computed

*The values of the 20 largest off-diagonal correlation coefficients will be printed for every least-squares cycle.

3. Control Card (Cont.):

<u>Column</u>	<u>Variable</u>	<u>Description</u>
		1 - Ellipsoids computed for anisotropic atoms 2 - Ellipsoids and thermal corrections to bonds computed
6	MREF	Refinement type indicator 0 - Refine on F_2 1 - Refine on F^2
7	IFILE	Rewrite data set indicator 0 - Data set rewritten if this is the last cycle of the current run 1 - Data set not rewritten 2 - Data set rewritten. On input the standard deviations of parameters refined in previous cycles will be read in. 3 - Data set not rewritten. Standard deviations read in.
8	NEW(1)	If non-zero, read new cell parameters*
9	NEW(2)	If non-zero, read new bond distance limits
10	NEW(3)	If non-zero, read new symmetry operators
11	NEW(4)	If non-zero, read new scattering factors†
12	NEW(5)	If non-zero, read new scale factors and atom parameters. If equal to one, all atoms will be read. If equal to two, only selected atoms will be read. If equal to 3 only scale and extinction will be read. If equal to 4 only special parameters will be read.
13	NEW(6)	If non-zero, read temperature factor type card
14	NEW(7)	If non-zero, read parameter selection card(s) and parameter dependency card(s)
15	NEW(8)	If non-zero, read new structure factors. Values 1, 2, and 3 correspond to various options for the order of the list, as explained below.

For all zero values in columns 8-15, the old values are read from file ISCl or the values in memory are used. The above integers are required for all cycles.

16-20	DMIN	Minimum bond distance in Angstroms. Needed only if NEW(2) $\neq$ 0.
21-25	DMAX	Maximum bond distance in Angstroms. Needed only if NEW(2) $\neq$ 0.

*Note that if the new cell parameters will affect $\sin\theta/\lambda$, and therefore the atomic scattering factors for various reflections, structure factors must be read in.

†Warning: New scattering factor curves must be read only in the first cycle of a given computer run or when new structure factors are being read in, or they will never be used in computation.

3. Control Card (Cont.):

<u>Column</u>	<u>Variable</u>	<u>Description</u>
26	ICENT	Centric indicator, needed only if NEW(3) $\neq$ 0 0 - Centric 1 - Acentric
27	ICELL	Cell type indicator, needed only if NEW(3) $\neq$ 0 0 - Primitive cell 1 - A-centered cell 2 - B-centered cell 3 - C-centered cell 4 - I-centered cell 5 - F-centered cell 6 - R-centered cell
28	MANOD	Anomalous dispersion indicator, needed only if NEW(4) $\neq$ 0 0 - No corrections are to be used 1 - Include anomalous dispersion corrections
29-30	NSCAT	Number of scattering curves. This is needed only if NEW(4) $\neq$ 0. (0 < NSCAT < 21)
31-32	NATOM	Number of atoms in asymmetric unit. This is needed only if NEW(5) $\neq$ 0. (0 < NATOM < 61)
33-34	NSF	Number of scale factors. This is needed only if NEW(5) $\neq$ 0. (0 < NSF < 11)
35	NEWEXT	Extinction change indicator (needed only if NEW(5) $\neq$ 0) 0 - New extinction parameters not read 1 - Extinction parameters read from cards
36	IWT	Weight type, needed only if NEW(8) $\neq$ 0. 0 - Standard deviation of F on cards 1 - Standard deviation of F ² on cards 2 - Weight on cards 3 - Sigma for F is to be computed in WEIGHT 4 - Compute weight in subroutine WEIGHT 5 - Standard deviation of F on cards will be altered by "ignorance factor" by $\sigma = (\sigma^2 + (pF)^2)^{1/2}$
37	INN	Structure factor source indicator, needed if NEW(8) $\neq$ 0. 0 - Structure factors on cards 1 - New structure factors from file ISC3
38	IREJ	Rejection parameter, needed only if NEW(8) $\neq$ 0. 0,5 - No reflections rejected 1,6 - Reject if I less than the minimum obs. 2,7 - Reject if I less than the minimum obs. or $ F_o - F_c /\sigma_F$ greater than DELMAX 3,8 - Reject if $ F_o - F_c /\sigma_F$ greater than DELMAX In both of these cases weights will be altered by $w' = w(1 - 3x^4 + 2x^6)$, where $x = F_o - F_c /(\sigma_F * \text{DELMAX})$ 4,9 - Use special routine REJECT

3. Control Card (Cont.):

<u>Column</u>	<u>Variable</u>	<u>Description</u>
NOTE: Values of IREJ from 5 to 9 allow the rejection mode to be changed even though NEW(8) = 0.		
39-43	DELMAX	Maximum allowable difference between observed and calculated structure factors on an absolute scale. This is needed only if NEW(8) $\neq$ 0 and IREJ is 2 or 3, or if IREJ is 7 or 8.
44-53	JSCRF	Scale factor refinement switches (needed only if NEW(7) $\neq$ 0)
54-59	KEXTRF	Extinction factor refinement switches (needed only if NEW(7) $\neq$ 0)
60	JXPAR	Extra parameter indicator 0 - No extra parameters 1 - Extra parameters will be read (needed only if NEW(5) $\neq$ 0)
61	IFSGN	Orientation determination parameter 0 - Do not determine the orientation 1 - Change to orientation with lower weighted <u>r</u> (needed only if NEW(7) $\neq$ 0)

4. Cell Card: Needed only if NEW(1) $\neq$ 0.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-8	A(1)	<u>a</u> axis length in angstroms
9-16	A(2)	<u>b</u> axis length
17-24	A(3)	<u>c</u> axis length
25-32	A(4)	Alpha in degrees
33-40	A(5)	Beta in degrees
41-48	A(6)	Gamma in degrees

5. Symmetry Cards: Needed only if NEW(3) $\neq$ 0.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-3	JTNS(1)	Translational part of <u>x'</u>
5-6	IRMAT(1,1)	First positional part of <u>x'</u>
8-9	IRMAT(2,1)	Second positional part of <u>x'</u>
11-13	JTNS(2)	Translational part of <u>y'</u>
15-16	IRMAT(1,2)	First positional part of <u>y'</u>
18-19	IRMAT(2,2)	Second positional part of <u>y'</u>
21-23	JTNS(3)	Translational part of <u>z'</u>
25-26	IRMAT(1,3)	First positional part of <u>z'</u>
28-29	IRMAT(2,3)	Second positional part of <u>z'</u>
34	IEF	End flag, non-zero on last card only 0 - Another symmetry card follows 1 - This is the last card

The translational operators are of the following form:

bbb 1/2 1/3 2/3 1/4 3/4 1/6 or 5/6. The positional operators are of the form bW = W or -W with W equal to X, Y, or Z and b signifies a blank. The symmetry position X Y Z must be included.

6. Scattering Factor Cards: Needed only if NEW(4) $\neq$ 0.

<u>Columns</u>	<u>Description</u>	
1-8	a ₁	These coefficients must satisfy the equation
9-16	b ₁	
17-24	a ₂	$f(x) = c + \sum_{i=1}^4 a_i \exp(-b_i x^2)$
25-32	b ₂	
33-40	a ₃	
41-48	b ₃	
49-56	a ₄	with $x = \sin\theta/\lambda$
57-64	b ₄	
65-72	c	
73-80	Identification	

Coefficients for scattering curves of this form have been tabulated by Cromer and Waber (1965) for relativistic Dirac-Slater wave functions, by Cromer and Mann (1968) for Hartree-Fock wave functions and by Doyle and Turner (1968) for relativistic Hartree-Fock wave functions. If anomalous dispersion coefficients are being used (MANOD = 1), the above card is followed by one with the real part of the anomalous dispersion in col. 1-8 and the imaginary part in col. 9-16. Coefficients for the hydrogen atom are given by Forsyth and Wells (1959).

NOTE: The scattering curves should be changed only on the first cycle of a given computer run or when NEW(8) = 1. New structure factors must be read (NEW(8) = 1) if the number of scattering curves is to be changed.

7. Scale Factor Cards: Needed only if NEW(5) $\neq$ 0.

The NSF scale factors are punched with 8 columns per value and 9 values per card and should be the values needed to place the calculated structure factors on the same scale as the observed.

8. Extinction Cards: Needed only if NEW(5) $\neq$ 0 and NEWEXT $\neq$ 0. Format (6E12.6)

<u>Columns</u>	<u>Value</u>
1-12	r* for isotropic extinction or r* ₁₁ for anisotropic
13-24	r* ₂₂
25-36	r* ₃₃
37-48	r* ₁₂
49-60	r* ₁₃
61-72	r* ₂₃

9. Atom Parameter Cards: Needed only if NEW(5) $\neq$ 0.

If NEW(5) = 1, the entire atom list is read with two cards per atom.
If NEW(5) = 2, the Atom Number is read with Format (I2) followed by the two cards for that atom. Card reading is terminated by a blank Atom Number card.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
Card 1-6	TAG	Alphanumeric identifier
7-12	SITE	Equipoint fraction
13-18	OCCUP	Total occupancy of site
19-24	OCCA	Occupancy of species A in this site Needed only if multiple occupancy
Card 2 1-2	ISCAT(1)	Number of scattering curve for species A
3-4	ISCAT(2)	Number of scattering curve for species B (blank if single element in site).
9-15	XYZ(1)	$\underline{x}$ of atom in fractional coordinates
16-22	XYZ(2)	$\underline{y}$
23-29	XYZ(3)	$\underline{z}$
30-36	BETA(1)	$\underline{B}$ for an isotropic atom <u>or</u> β_{11} for an anisotropic atom
37-43	BETA(2)	β_{22}
44-50	BETA(3)	β_{33}
51-57	BETA(4)	β_{12}
58-64	BETA(5)	β_{13}
65-71	BETA(6)	β_{23}
73	IEF	Indicator of third cumulant
Card 3 -	Needed if IEF $\neq$ 0.	
1-8	C ₁₁₁	
9-16	C ₂₂₂	
17-24	C ₃₃₃	
25-32	C ₁₁₂	
33-40	C ₁₂₂	
41-48	C ₁₁₃	
49-56	C ₁₃₃	
57-64	C ₂₂₃	
65-72	C ₂₃₃	
73-78	C ₁₂₃	
80	IEF ³	Fourth cumulant ind.

Card 4-5 - Needed if IEF $\neq$ 0.

Punch d_{1111} , d_{2222} , d_{3333} , d_{1112} , d_{1113} , d_{1122} , d_{1133} , d_{1222} , d_{1223} , d_{1233} , d_{1333} , d_{2223} , d_{2233} , d_{2333} in order with 8 columns per value.

10. Special parameter cards: Needed only if NEW(5) $\neq$ 0 and JXPAR $\neq$ 0.

Card 1: Columns 3-4 contain the number of special parameters, NPAR.

If NPAR>0 the succeeding cards contain the names, initial values, and identifiers according to the following form.

Columns 1-8	Name of parameter, up to 8 alphanumeric characters.
Columns 9-10	Type of parameter, 0-linear function with coefficient given on constraint card. 1-rigid body system 2-defined by user in subroutines SPVAL and SPDERI
Columns 11-12	Integer indicating which rigid-body system, if more than one, this parameter refers to.
Column 13-14	Parameter designator. If the type is 1 the code is as follows 1-X coordinate of origin (in crystal axes system) 2-Y coordinate of origin 3-Z coordinate of origin 4- ω angle for transformation to standard, orthonormal coordinate system 5- χ angle for transformation 6- ϕ angle for transformation 7-X coordinate of an atom in the special system 8-Y coordinate of an atom 9-Z coordinate of an atom 10-T ₁₁ 11-T ₂₂ 12-T ₃₃ 13-T ₁₂ 14-T ₁₃ 15-T ₂₃ 16-L ₁₁ 17-L ₂₂ 18-L ₃₃ 19-L ₁₂ 20-L ₁₃ 21-L ₂₃ 22-S ₁₁ 23-S ₂₂ 24-S ₃₃ 25-S ₁₂ 26-S ₁₃ 27-S ₂₃ 28-S ₂₁ 29-S ₃₁ 30-S ₃₂

Columns 15-24 initial value of this parameter.

11. Extinction and Temperature Factor Type Card: Needed only if NEW(5) or NEW(6) $\neq$ 0.

Column 1 contains the extinction factor code:

0 - Isotropic, do not change

1 - Anisotropic Type I (mosaic spread dominates)

- 2 - Anisotropic Type II (domain size dominates)
- 3 - Now Isotropic, change to Type I
- 4 - Now Isotropic, change to Type II
- 5 - Now Type I, change to Isotropic
- 6 - Now Type II, change to Isotropic
- 7 - Now Type I, change to Type II
- 8 - Now Type II, change to Type I

The temperature factor type code is punched with one column per atom beginning in Col. 2 with the following code:

- 0 - Now isotropic, do not change
- 1 - Now anisotropic, do not change
- 2 - Now isotropic, change to anisotropic
- 3 - Now anisotropic, change to isotropic
- 4 - Now 3rd cumulant, do not change
- 5 - Now anisotropic, change to 3rd cumulant
- 6 - Now 3rd cumulant, change to anisotropic
- 7 - Now 4th cumulant, do not change
- 8 - Now 3rd cumulant, change to 4th
- 9 - Now 4th cumulant, change to 3rd

12. Parameter Selection Cards. Needed only if NEW(7) $\neq$ 0. If JXPAR $\neq$ 0 the first card contains refinement selection for the special parameters in the first NPAR columns. A zero in a column means that the corresponding parameter will not be refined and a one means that it will. After this cards with the refinement indicators for the conventional parameters punched in columns 1-80. If the number of atom parameters is such that more than 80 values are required, the parameter selection information should be continued in column 1 of the next card. The order of parameters is:

- a) occupancy - If single occupancy, the total occupancy is refined. If multiple occupancy, the occupancy of species A is refined.
- b) x coordinate
- c) y coordinate
- d) z coordinate
- e) thermal parameters, one for isotropic atoms, six for anisotropic atoms. The thermal coefficients occur in the same order as on the Atom Parameter Card 2.
- f) 3rd and 4th cumulant parameters (if needed).

13. Parameter Constraint Cards(s): Needed only if NEW(7) $\neq$ 0.

a)	<u>Columns</u>	<u>Description</u>
	1-3	Integer specifying the dependent atom number.
	5-6	Dependent parameter number. This number is 1 for occupancy, 2-4 for x through z respectively, 5 for <u>B</u> or β_{11} , and 6, 7, 8, 9, 10 for β_{22} , β_{33} , β_{12} , β_{13} and β_{23} respectively. Values of 11 to 20 treat 3rd cumulant parameters and 21-35 are for the 4th cumulants.

13. Parameter Constraint Cards(s) (Cont.):

a)	<u>Columns</u>	<u>Description</u>
	7-9	Atom number of first independent parameter. Special parameters are arbitrarily indicated as atom number 0.
	10-12	Parameter number of first independent parameter. Atom 0 parameter 0 designates an initializing constant in a linear constraint function.
	13-20	Coefficient of first relationship.
	21-23	Atom number of second independent parameter
	24-26	Second independent parameter number
	27-34	Second coefficient
	35-37	Third independent atom number
	38-40	Third independent parameter number.
	41-48	Third coefficient
	49-51	Fourth independent atom number
	52-54	Fourth independent parameter number
	55-62	Fourth coefficient
	63-65	Fifth independent atom number
	66-68	Fifth independent parameter number
	69-76	Fifth coefficient.

If the independent atom number is zero, designating a special parameter, and the constraints are non linear, the second and fourth independent parameter numbers may be negative to denote the end of an inclusive list beginning with the first (third) independent parameter number.

b) One (1) blank card or a card with zero in column 3.

14. Structure Factor Cards: Needed only if NEW(8) $\neq$ 0.

- a) Format Card: This card contains the format of the input structure factor data. The number and order of variables on a card (or tape record) depends on the value of NEW(8), as explained in detail below. All records must contain at least four integer fields, for the indices and an observed/unobserved indicator, and two floating point fields for F_{obs} and σ_F or other weight information. They may contain other information, such as a scale factor group identifier, the factor $\beta(\theta)$ used in extinction corrections, and the setting angles, needed for anisotropic extinction corrections.
- b) Only if IWT=5 include a card with the "ignorance factor" punched as a real number in the first 8 columns.
- c) Only if NEW(8)=3 include the wavelength in Å in the first 8 columns. For neutron data only an approximation to $\beta(\theta)$ will be computed according to the formula $\beta(\theta) = [(2\lambda^2/(V^2\sin^2\theta))] \times 10^8$, where V is the unit cell volume in Å³. The refined quantity then will be the product $\bar{T}r^*$, with $\bar{T}$ assumed to be approximately constant.

- d) Data Cards in a form consistent with Format Card: If NEW(8)=1 the list is in this order.

<u>Variable</u>	<u>Description</u>
IH(1)	$\underline{h}$ for reflection
IH(2)	$\underline{k}$
IH(3)	$\underline{l}$
FOBS	Observed structure factor
SIGMA	Weight information consistent with IWT on Control Card
EXBETA	Factor $\beta(\theta)$ for extinction
I	Number of scale factor for this reflection. If zero, the scale factor is the same as the preceding reflection. Scale factor 1 is assumed for the first reflection.
MREJ	Minimum Observable Parameter
	1 - Intensity above minimum observable.
	2 - Intensity below minimum observable.
IEF	End-of-list marker, zero on all data cards
TTH	2θ These angles are needed only if anisotropic
OMEG	ω extinction is to be calculated and must
CHI	χ conform to the diffractometer conventions
PHI	ϕ given by Busing and Levy (1967, p. 458).

If NEW(8) = 2 the input list is IH(1), IH(2), IH(3), MREJ,I,FOBS,EXBETA, SIGMA, with the same meanings as above. The end of the data must be marked by an end-of-file.

If NEW(8) = 3 the list is IH(1), IH(2), IH(3), MREJ,FOBS,SIGMA. EXBETA is computed, and again the end of data must be marked by an end-of-file.

- e) End-of-list card - A card with a non-zero value in the field of variable IEF or an end-of-file card appropriate to the system.

15. Run Continuation and Parameter Punch Card: Needed for all cycles.

<u>Column</u>	<u>Variable</u>	<u>Description</u>
1	ICONT	0 - No more cycles. The data set on file ISCI will be updated if IFILE from the Control Card is zero
2	JPUN	1 - Read a new title card and start another cycle 0 - Do not punch any atom parameters 1 - Punch atom cards in form required by 'X-RAY67' 2 - Punch atom cards in form required by this program
3-4	ISCI	3 - Punch atom cards in both forms If this field is non-zero its value will be substituted as the unit number for the binary master file, making it possible to try new courses of refinement without destroying previous stages.

BONDAN: A program for computing bond distances, angles,
and thermal ellipsoids, with errors

This program uses the master binary file created by RFINE to compute bond distances and angles, and also thermal ellipsoids, with associated standard deviations. If the rigid body model is used, the atomic positions of the rigid body will be corrected for libration before calculation of distances and angles. The program will also accept input from cards by means of the program BADTEA. The complete description of BADTEA is included in Appendix B. The details of data input are as follows:

1. Input format indicator card

Col. 1-2 1-input from cards via BADTEA.
 2-input from binary file created by RFINE.

If the input format indicator is 1, see appendix B for further input.

If the input format indicator is 2, the card input continues as follows.

2. Title Card: Any desired hollerith information in columns 1-72.

3. Search Card: Format(I2,3A4)

If column 2 is zero or blank, a search of the data tape will be made to find a data set with a label the same as columns 3-14. The error calculation will be performed on that data set. If column 2 is non-zero, the first data set on the tape will be used in the error calculation.

4. Parameter Card: Format(2I1,3F8.0)

<u>Column</u>	<u>Variable</u>	<u>Description</u>
1	MBODAN	Bond distance, angle selector 0 - None computed 1 - Distances only 2 - Distances and angles computed
2	MELVIB	Thermal ellipsoid selector 0 - No ellipsoids computed 1 - Thermal ellipsoids computed for anisotropic atoms
3-10	DLIMIT(1)	Minimum bond distance output
11-18	DLIMIT(2)	Maximum bond distance used in angles output
19-26	DLIMIT(3)	Maximum bond distance output

5. Cell variance-covariance matrix: Format(6E12.6)

This matrix is the matrix output by the lattice constant program of C. W. Burnham.

<u>Column</u>	<u>Description</u>
Card 1	
1-12	Variance of <u>a</u> (in angstroms**2)
13-24	Covariance of <u>a</u> with <u>b</u>
25-36	Covariance of <u>a</u> with <u>c</u>
37-48	Covariance of <u>a</u> with alpha (in angstrom-radians)
49-60	Covariance of <u>a</u> with beta
61-72	Covariance of <u>a</u> with gamma
Card 2	
1-12	Variance of <u>b</u>
13-24	Covariance of <u>b</u> with <u>c</u>
25-36	Covariance of <u>b</u> with alpha
37-48	Covariance of <u>b</u> with beta
49-60	Covariance of <u>b</u> with gamma
61-72	Variance of <u>c</u>
Card 3	
1-12	Covariance of <u>c</u> with alpha
13-24	Covariance of <u>c</u> with beta
25-36	Covariance of <u>c</u> with gamma
37-48	Variance of alpha (in radians**2)
49-60	Covariance of alpha with beta
61-72	Covariance of alpha with gamma
Card 4	
1-12	Variance of beta
13-24	Covariance of beta with gamma
25-36	Variance of gamma

If the errors in the cell constants have a small effect on the distances, the last 4 cards may be replaced by blanks.

FOURIER

This program uses the binary structure factor file created by RFINE (ISC4-unit 12) as input for a Fourier synthesis. The map is written on unit 11 for input to the plotting program CNTPLT or the arbitrary section program ARBSECT. The details of data input are as follows:

1. Title Card: Any desired alphanumeric information in columns 1-72. This information heads all map sections.
2. Parameter Card: Format (6I1, 2X, 9I4, 3F8 0.4)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1	ITYPE	Map type indicator 0 - Fourier map 1 - Difference Fourier
2.	ISECT	Section parameter 0 - $\underline{x}$ across, $\underline{y}$ down and $\underline{z}$ sections 1 - $\underline{x}$ " " $\underline{z}$ " " $\underline{y}$ " 2 - $\underline{y}$ " " $\underline{x}$ " " $\underline{z}$ " 3 - $\underline{y}$ " " $\underline{z}$ " " $\underline{x}$ " 4 - $\underline{z}$ " " $\underline{y}$ " " $\underline{x}$ " 5 - $\underline{z}$ " " $\underline{x}$ " " $\underline{y}$ "
3	INCENT	Centric indicator 0 - Centric 1 - Acentric
4	KREJ	0 - Ignore rejection flag and include all reflections. 1 - Do not include any reflections with the rejection flag set.
5	IPLT	If non-zero, map sections will be written to unit S2 for plotting or calculation of an arbitrary section.
6	LSPC	If zero, the lines of the map will be double spaced. A non-zero value indicates single spacing.
9-12	IX	Number of divisions along horizontal axis (>0)
13-16	IXI	Initial point
17-20	IXF	Final point
21-24	IY	Number of division along vertical axis (>0)
25-28	IYI	Initial line
29-32	IYF	Final line
33-36	IZ	Number of divisions along section axis (>0)
37-40	IZI	Initial section
41-44	IZF	Final section
45-52	EXXAG	Map exaggeration desired
53-60	F000	Number of electrons in unit cell for Fourier.

2. Parameter Card (cont.):

61-68	TMULT	Zero for difference Fourier. Multiplicity of a general reflection
-------	-------	--

3. Multiplicity Card: Format (12F6.0)

<u>Columns</u>	<u>Description</u>
1-6	Multiplicity of h00 or 0k0
7-12	Multiplicity of 00l
13-18	Multiplicity of hk0
19-24	Multiplicity of h0l
25-30	Multiplicity of 0kl
31-36	Multiplicity of hh0
37-42	Multiplicity of h0h
43-48	Multiplicity of 0kk
49-54	Multiplicity of hhh
55-60	Multiplicity of hhl
61-66	Multiplicity of hkk or hkh
67-72	Multiplicity of hkl

C. Size of Program:

This program uses the array FBUF in common block ABLE as pooled storage. The size of this array, S, is governed by the map to be calculated and may be estimated using:

$$S = 3N_{\text{ref}} + 2(h'_{\text{max}} + 2)(2k'_{\text{max}} + 1) + 2(h'_{\text{max}} + 1)(P_x + 1)$$

where N_{ref} is the number of reflections included, h'_{max} is the maximum value of the index associated with the horizontal axis, k'_{max} is the maximum value of the index associated with the axis plotted down the page, and P_x is the number of points calculated in the horizontal direction. If the Fourier sections are to be saved for later plotting, S should be increased by $P_x P_y$. If the computer operating system supports dynamic core allocation, the program may be converted to automatically request the proper memory size.

D. Output:

Each map point is converted to a four-digit integer before printing with zero values replaced by blanks. Each point will occupy an area 4 columns by 1 or 2 rows depending upon the spacing selected. For most printers, the area is 0.4 x 1/6 inches for single spacing or 0.4 x 1/3 inches for double spacing of the lines. If the map requires more than 30 points, the section will be printed in strips with 30 points per strip.

E. Additional Problems:

If additional maps are to be run using the same structure factor list, a complete set of cards beginning with the Title Card should be included. An end-of-file in the card stream terminates the program.

LISTFC

This program is an adaption of the XRAY67 program LIST FC (Stewart et al., 1967). It has been altered to stand alone and read the structure factor file (ISC4 - unit 12) created by RFINE. The output of the program has been changed so that the "phase in millicycles" has been replaced by sigma (Fobs). Input is as follows:

Card 1.

Col. 1-6 compound identification; Col. 7-78 any title.

Card 2.

Col. 14 (1)/(2)/(3) for h index varies (most)/(next most)/(least) rapidly

15 Same for k index

16 Same for l index

(Note that the sum and product of Cols. 14, 15, and 16 must equal 6.)

17-20 Number of lines per list page.

21 (blank)/(A) for (DO)/(DO NOT) internally change the value of the number of lines in order to make the bottom of the last page as even as possible.

22-24 Number of list columns per page. Note that the product of the number of lines and the number of columns cannot exceed 2000. That is no more than 3000 items for the number of reflections and headings (including spaces) per page.

26 Number of blank print columns before the LISTFC column.

28 Number of print columns for most rapidly changing index.

30 Number of print columns for F_{obs}

32 Number of print columns for F_{calc}

34 Number of print columns for σ_F

36 Special flag for unobserved reflections (blank=*)

38 Special flag for severely extinct reflections (blank=E)

40 Special flag for special reflection (JCODE=4)

The next eight fields are (blank)/(1) for (do not)/do

42 Print symbol for unobserved or severely extinct reflections.

This symbol switch adds one print column

44 For centric structures, attach sign of A to F_{calc}

46 Double space the lines

48 Restore each LISTFC page to the top of the printer page

50 Print title at the top of each printer page

52 Punch a set of "FCARD" cards

56 Print a minus sign on F_{obs} for unobserved reflections

58 Write a separate copy of FC list on unit 7

62 Number of times to try to get headings at the top of all columns

64 (1)/(2)/(3) for headings separated by (no blank
 lines)/(1 blank line above)/(1 above and 1
 below)(blank=3)

65-72 factor F_s are to be multiplied by (blank=10)

73-80 factor σ_s are to be multiplied by (blank=10)

Note that all F and σ values are printed as integers,
 so that scale factor must be sufficient to preserve a
 sufficient number of significant figures.

CNTPLT is a contour plotting program for Fourier maps and other similar functions. The routines contained in this program have been derived from multiple sources with the original version of subroutine ICONT written by S. H. Zisk and N. M. Brenner of M.I.T. Lincoln Lab. Subroutine INTPLT uses the rational polynomial spline interpolation of D. V. Ahuja, I.B.M. Systems Journal, p. 208-217, (1968). The other routines have been modified from code prepared by G. Ford, Purdue University.

The present version of these routines have been written to be as machine independent as possible. It is believed that only the call to the plotter function PLOTS (Sequence No. A5300) and the two functions MARK and UNMARK called by ICONT are machine specific. This is the main contribution of the present author (LWF).

Method

The main contouring subroutine, ICONT, takes the function values at the grid points of the map and computes the coordinates of the intersection of a specified contour line with the lines of the grid. Linear interpolation is used in this process. The second contouring subroutine, CPLOT, coordinates the drawing of the contours and produces any desired contour labels. The third contouring routine, INTPLT, produces a smooth curve through the intersections located by ICONT. Rational cubic polynomials are used to fit a spline-like curve through neighboring points. Two such curves meet smoothly because the first and second derivatives are single valued along the composite curve. The plotter line is drawn as a series of straight line segments with the number of such segments specified by the user.

The main program includes various options which allow labeling of plot sections and/or grid points, drawing of the bounding parallelogram, and other similar functions.

Input

The values of the function to be plotted are read from a binary input file (unit 10) with each section occupying two records. The first contains the variables MA, MB, JZ, MZ where MA and MB are the number of grid points along x and y respectively. The second record contains the data for the map section at JZ/MZ. These data are assumed to be in real form and are packed in an array which is MAXMB. The output file produced by program FOURIER is in this form.

Input

1. Title Card: Format (20A4)
2. Control Card: Format (F5.0, I5, 3F5.0, 6I5, F5.0, 2I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	TLEHGT	Plotting height of title in inches. If ≤ 0 , no title will be plotted
6-10	NLABL	Number of vertex labels to be plotted
11-15	A	Width of plot (in inches) parallel to <u>x</u> -axis of Fourier. If $A > 0$, an 11' plotter is assumed. If a 30" machine is available, A should be less than zero.
16-20	B	Length of plot (in inches) parallel to <u>y</u> -axis of Fourier which is parallel to plotter <u>x</u> -axis.
21-25	ALP	Angle between Fourier axes (in degrees)
26-30	NA	Number of grid points parallel to Fourier <u>x</u> -axis
31-35	NB	Number of grid points parallel to Fourier <u>y</u> -axis
36-40	NP	Number of interpolation points per spline. The default value is 4.
41-45	NCONT	Number of sets of contour levels (NCONT ≤ 10)
46-50	NLINE	Number of line vertices specified (NLINE ≤ 20)
51-55	NCROSS	Number of crosses to be placed on plot (NCROSS ≤ 20)
56-60	SCROSS	Size of cross (in inches)
61-65	NSECT	Number of sets of sections specified
66-70	NZ	Grid spacing of section levels.

3. Contour Card(s): Format (3F5.0,I5)
There should be NCONT of these cards.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	SBEG	Height of initial contour
6-10	CSTEP	Step between contours
11-15	SLIM	Height of final contour
16-20	NSIG	Number of digits after decimal point in contour label. If NSIG < 0 , contours will not be labelled.

4. Line Vertex Card(s): Format (16F5.0)

The positions of the line vertices in map grid coordinates should be punched. A line will be drawn from point i to point i+1 if $x_{i+1} > 0$. No line will be drawn if $x_{i+1} < 0$. Omit these cards if NLINE ≤ 0 .
Note: The first grid point is (1,1), not (0,0). i.e. add (1,1) to scaled coordinates.

5. Cross Card(s): Format (16F5.0)

The map grid coordinates of the crosses should be punched sequentially. Omit these cards if NCROSS $\leq$ 0.

6. Section Selection Cards: Format (3I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	INITZ	Sections from INITZ
6-10	ISTEPZ	to IFINZ in steps
11-15	IFINZ	of ISTEPZ will selected and contoured.

There should be NSECT of these cards.

7. Vertex Label Card(s): Format (5F5.0,A6)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	WX	x-grid coordinate
6-10	WY	y-grid coordinate
11-15	DX	Plotter x-axis offset
16-20	DY	Plotter y-axis offset
21-25	HGT	Label height in inches
26-31	LABL	Alphanumeric label

There should be NLABL of these cards.

Tape output for Calcomp plotter is on Unit 12.

ARBSECT

This program calculates an arbitrary section of a Fourier map from a complete set of sections calculated in regular intervals parallel to the crystallographic axes. The input sections may be computed with the regular Fourier program and are assumed to be in file No. 11. The plane of the output section is specified by the coordinates of the plane to be calculated.

Program ARBSECT has several options available. If only a fraction of the unit cell is used as input, it will calculate the electron density in the accessible portion only with the remainder replaced by asterisks in the printout. However, if the map for a complete unit-translation has been computed, the program will use the translation symmetry to calculate a complete section. No other symmetry operations are used. Other options include (a) describing the points used to define the plane in terms of map or fractional coordinates as desired, (b) saving the resulting section in file 12 for later plotting, (c) computing the entire section or selecting a portion of it, and (d) calculating and printing the geometry including axial lengths and interaxial angle, of the output section.

Method

The input coordinates of the three points defining the plane are initially converted to map coordinates if necessary. The coefficients of the plane in the equation $a_1x + a_2y + a_3z + a_4 = 0$ may be found from the determinant equation

$$\begin{vmatrix} x & y & z & 1 \\ x_1 & y_1 & z_1 & 1 \\ x_2 & y_2 & z_2 & 1 \\ x_3 & y_3 & z_3 & 1 \end{vmatrix} = 0$$

where x_i , y_i , and z_i are the coordinates of the i 'th point. This plane will have a line of intersection with each section of the original map. For the values of y and z corresponding to each line and section of the output map, the x -coordinate of this point in the plane is determined. A cubic function of the form $ax^3 + bx^2 + cx + d$ is fitted to the four adjacent grid points on the line, and the value of this function at the intersection point is used for the output at that y and z . This process is repeated until all output points have been determined.

Input

The input map sections are read from file 11 and the resulting map is output to file 12. These assignments may be changed by redefining variables ISC and ISC1 respectively.

1. Title Card - Format (18A4)

Columns 1-72 of this card may contain any desired information.

2. Control Card - Format (8I3)

<u>columns</u>	<u>Variable</u>	<u>Description</u>
1-3	IO	If IO $\neq$ 0, the output section will be written on Unit 12.
6	IZO	Section number of output
9	ISPC	If ISPC = 0 the output map will be single spaced; double spaced if ISPC=1.
12	IMRK	If IMRK=0, the y- and z- limits of the input sections will be used as the x-, and y-limits, respectively, of the output section. If IMRK $\neq$ 0, these values are read from this card.
13-15	IYI	Initial value of x in transformed section
16-18	IYF	Final value of x in transformed section
19-21	IZI	Initial value of y in transformed section
22-24	IZF	Final value of y in transformed section

3. Cell Card - Format (6F8.0)

<u>Columns</u>	<u>Description</u>
1-8	Length (in A) of cell axis across page in original section
9-16	Length of cell axis down page in original section
17-24	Length of cell axis out of page in original section
25-32	Angle (in degrees) between axis 1 and 2
33-40	Angle between axes 1 and 3
41-48	Angle between axes 2 and 3

The above length and axes are required only if the program is to compute and print the axial length and interaxial angle of the transformed section. If not, this card may be blank.

4. Plane Card - Format (9F8.0, I2)

<u>Columns</u>	<u>Description</u>
1-8	x- coordinate of first point
9-16	y- " " " "
17-24	z- " " " "
25-32	x- " " second "
33-40	y- " " " "
41-48	z- " " " "
49-56	x- " " third "
57-64	y- " " " "

4. Plane Card - (Cont.)

<u>Columns</u>	<u>Description</u>
65-72	z- coordinate of third point
74	Coordinate type indicator. If zero, the coordinates are given in grid spacings. If non-zero, the points are given in fractional coordinates.

Additional arbitrary slices may be computed by supplying additional data decks beginning with the Title Card.

Form of Input Sections

The input Fourier sections are read from Unit 11 with unformatted reads. There must be two records per section as follows:

Record 1:

<u>Word</u>	<u>Variable</u>	<u>Description</u>
1	JXA	Number of grid points calculated parallel to x
2	JYA	Number of grid points calculated parallel to y
3	KZC	Section number
4	IZ	Number of sections per unit cell
5	IX	Number of intervals per unit cell parallel to x
6	IXI	Initial grid points parallel to x
7	IXF	Final grid point parallel to x
8	IY	Number of intervals per unit cell parallel to y
9	JYI	Initial grid point parallel to y
10	JYF	Final grid point parallel to y
11	JZI	Initial grid point parallel to z
12	JZF	Final grid point parallel to z

Record 2:

This record consists of the JXA*JYA values of the map in this section. These real values must be packed in an array with the x coordinate as the first subscript and y as the second subscript.

REFERENCES CITED

- Busing, W. R., and H. A. Levy (1962) A procedure for inverting large matrices. Comm. ACM, 5, 45-46.
- _____ and _____ (1964) The effect of thermal motion on the estimation of bond lengths from diffraction measurements. Acta Crystallogr., 17, 142-146.
- _____ and _____ (1967) Angle calculations for 3- and 4-circle x-ray and neutron diffractometers. Acta Crystallogr., 22, 457-464.
- Coppens, P., and W. C. Hamilton (1970) Anisotropic extinction corrections in the Zachariasen approximation. Acta Crystallogr., A26, 71-83.
- Cromer, D. T., and J. T. Waber (1965) Scattering factors computed from relativistic Dirac-Slater wave functions. (Acta Crystallogr., 18, 104-109.
- _____ and J. B. Mann (1968) X-ray scattering factors computed from numerical Hartree-Fock wave functions. Acta Crystallogr., A24, 321-324.
- Doyle, P. A., and P. S. Turner (1968) Relativistic Hartree-Fock X-ray and electron scattering factors. Acta Crystallogr., A24, 390-397.
- Finger, L. W. (1969) Determination of cation distribution by least-squares refinement of single-crystal X-ray data. Carnegie Inst. Wash. Year Book 67, 216-217.
- Forsyth, J. B., and M. Wells (1959). On an analytic approximation to the atomic scattering factor. Acta Crystallogr., 12, 412.
- Hamilton, W. C. (1959) On the isotropic temperature factor equivalent to a given anisotropic temperature factor. Acta crystallogr., 12, 609-610.
- Levy, H. A. (1956) Symmetry relations among coefficients of the anisotropic temperature factor. Acta Crystallogr., 9, 679.
- Nelmes, R. J., and Thornley, F. R. (1973) Anisotropic extinction in a synthetic boracite. To be published.
- Zachariasen, W. H. (1967) A general theory of x-ray diffraction in crystals. Acta Crystallogr., 23, 558-564.

Appendix A
Overlay scheme for RFINE

When program RFINE is run under operating systems which charge according to the product of core allocation and CPU time, substantial savings can be achieved by using an overlay structure which causes only that portion of the program which is actually needed to be resident in core. Furthermore, there can be large savings if the core allocated for the dependency list and the normal equations matrix can be adjusted as appropriate to a particular problem. On UNIVAC machines operating under EXEC 8 this latter function is accomplished dynamically at run time by means of the subroutine CORSZ, which makes use of executive requests ER MCOORE\$ and ER LCOORE\$. On other machines which don't have a similar function capability, this can be achieved by a run time recompilation of the short main program, with the dimension of the array A in common block LSMAT appropriately adjusted.

The program has been run successfully with a structure consisting of a main stem and three overlay segments as follows:

Main stem: main program, subroutines RFINE and CORSZ.

Overlay 1: Subroutines RESET, DERIVS, RDEGN, and PAREXT plus auxilliary functions called by them, including DIJKLM, DETERM, EL4, PIJKLM, BIIJK, CIJKL, AIJ, VXV, SOLVE, EIJ, FIJ, IPAK, PDEGN, D3KDS, D2KDS, P3KDL, P2KDL, D2KDT, TKTLS, TFM, SKTLS, CORECT, MULMM, TRNSPS, EULER, FILLIN, SPVAL, ERRCAL.

Overlay 2: Subroutines INPUT, SFAC, RCALC, MATRIX, MODIFY, and SYMINV.

Overlay 3: Subroutines TRNFRM, BODAN1, and ELVIB1.

Appendix B

BADTEA-Alternate input for bond distances and angles, and thermal ellipsoids

A. IDENTIFICATION

TITLE: Crystallographic error analysis

NAME: U M BADTEA

PROGRAMMER: Larry W. Finger

DATE: December 27, 1965 (revised November 1968)

B. PURPOSE

U M BADTEA (University of Minnesota program for computing Bond angles and Distances, and Thermal Ellipsoids with error Analysis) will calculate bond distances, bond angles, thermal ellipsoids and the errors associated with each computed value. The program was converted to Fortran IV with the assistance of C. T. Prewitt.

C. USAGE

1. Input deck order:

Title card
Cell card
Function card
Symmetry card(s)
*Standard Deviations of cell parameters
*Correlation matrix of cell parameters
Atom cards
*Temperature Factor Standard Deviations
*Temperature Factor Correlation matrix
*Atomic Position Standard Deviations
*Atomic Position Correlation Matrix

*These data may not be needed. The next section describes in detail the conditions requiring these input data. All input from Atom Cards to the end of the deck may come from a modified ORFFF tape.

2. Description of input deck:

a. Title Card

FORMAT (18A4)

Columns

Description

1 - 72

Identifier for problem. This should be any title which identifies the compound.

b. Cell Card

FORMAT (6F10.5)

Columns	Description
1 - 10	<u>a</u> axis length, in Å
11 - 20	<u>b</u> axis length
21 - 30	<u>c</u> axis length
31 - 40	α in degrees
41 - 50	β
51 - 60	γ

c. Function Card

FORMAT (5I4, 3X,A1,6X, 3F10.5)

Columns	Description
1 - 4	Number of atoms in asymmetric unit (≤ 60)
5 - 8	Centric Indicator 0 - Structure is centric 1 - Structure is non-centric
9 - 12	Bond Distance, Angle Parameter 0 - No angles or distances calculated 1 - Distances only 2 - Angles and Distances
13 - 16	Ellipsoid Indicator 0 - None calculated 1 - Ellipsoids calculated for anisotropic atoms
17 - 20	Error Indicator 0 - Errors not calculated 1 - Errors calculated. 2 - Errors calculated with structure information read from modified ORFFE tape.
24	Lattice Type Code - This column should be punched with a P, A, B, C, F, I, or R depending on the lattice type.
31 - 40	Minimum bond distance to be printed
41 - 50	Maximum distance used in angle calculation.
51 - 60	Maximum bond distance to be printed.

d. Symmetry Cards

FORMAT (3(A3,2(1X,A2),1X),I4)

Columns	Description
1 - 3	Translational part of <u>x'</u>
5 - 6	First positional part of <u>x'</u>
8 - 9	Second positional part of <u>x'</u>
11 - 13	Translational part of <u>y'</u>
15 - 16	First positional part of <u>y'</u>
18 - 19	Second positional part of <u>y'</u>
21 - 23	Translational part of <u>z'</u>
25 - 26	First positional part of <u>z'</u>
28 - 29	Second positional part of <u>z'</u>

Columns

Description

34

End of Symmetry Deck Indicator

Blank - more symmetry cards follow

1 - this is the last card

Note: The translational parts of the symmetry operators are of the form: $bbb \frac{1}{2} \frac{1}{3} \frac{2}{3} \frac{1}{4} \frac{3}{4} \frac{1}{6}$ or $\frac{5}{6}$ where b signifies a blank. The positional parts are of the form: $bw + w - w$ where w may be X, Y or Z. Symmetric positions which are related by a center of inversion or a multiple lattice point must not be included since these positions are internally generated. However, position $\underline{x} \underline{y} \underline{z}$ must be included and must be first.

e. Standard Deviations of Cell Parameters FORMAT (6F10.8)

This card and the cards in section f. below are needed only if errors are to be calculated.

Columns

Description

1 - 10	Standard Deviation of $\underline{a}$
11 - 20	Standard Deviation of $\underline{b}$
21 - 30	Standard Deviation of $\underline{c}$
31 - 40	Standard Deviation of α in degrees
41 - 50	Standard Deviation of β
51 - 60	Standard Deviation of γ

f. Cell Parameter Correlation Matrix FORMAT (6F8.5)

Columns

Correlation Coefficient of

Card 1:		
1 - 8	$\underline{a}$ with $\underline{a}$	(1.0)
Card 2:		
1 - 8	$\underline{a}$ with $\underline{b}$	
9 - 16	$\underline{b}$ with $\underline{b}$	(1.0)
Card 3:		
1 - 8	$\underline{a}$ with $\underline{c}$	
9 - 16	$\underline{b}$ with $\underline{c}$	
17 - 24	$\underline{c}$ with $\underline{c}$	(1.0)
Card 4:		
1 - 8	$\underline{a}$ with α	
9 - 16	$\underline{b}$ with α	
17 - 24	$\underline{c}$ with α	
25 - 32	α with α	(1.0)
Card 5:		
1 - 8	$\underline{a}$ with β	
9 - 16	$\underline{b}$ with β	
17 - 24	$\underline{c}$ with β	
25 - 32	α with β	
33 - 40	β with β	(1.0)

Cell Parameter Correlation Matrix (Cont).

Columns Correlation Coefficient of

Card 6:

1 - 8	$\underline{a}$ with γ	
9 - 16	$\underline{b}$ with γ	
17 - 24	$\underline{c}$ with γ	
25 - 32	α with γ	
33 - 40	β with γ	
41 - 48	γ with γ	(1.0)

g. Atom Cards FORMAT (2A3, 7X, 3F7.5, I2/6F8.5)

There should be a set of 2 atom cards for each atom in the asymmetric unit.

Position Card:

Columns	Description
1 - 6	Identification for atom
14 - 20	$\underline{x}$ in fractional coordinates
21 - 27	$\underline{y}$ in fractional coordinates
28 - 34	$\underline{z}$ in fractional coordinates
36	Temperature factor type
	0 - isotropic
	1 - anisotropic

Temperature factor card:

1 - 8	β_{11} or B
9 - 16	β_{22}
17 - 24	β_{33}
25 - 32	β_{12}
33 - 40	β_{13}
41 - 48	β_{23}

The anisotropic coefficients should be those for which the temperature factor expression is

$$\exp [-(h^2\beta_{11} + k^2\beta_{22} + l^2\beta_{33} + 2hk\beta_{12} + 2hl\beta_{13} + 2kl\beta_{23})].$$

h. Temperature Factor Standard Deviations FORMAT (6F10.8)

These cards are needed only for anisotropic atoms when ellipsoids and errors are to be calculated.

Columns	Description
1 - 10	Standard Deviation of β_{11}
11 - 20	Standard Deviation of β_{22}
21 - 30	Standard Deviation of β_{33}

Temperature Factor Standard Deviations (Cont)

Columns	Description
31 - 40	Standard Deviation of β_{12}
41 - 50	Standard Deviation of β_{13}
51 - 60	Standard Deviation of β_{23}

1. Temperature Factor Correlation Matrix FORMAT (6 F8.5)

These cards are needed only for anisotropic atoms when ellipsoids and errors are to be calculated.

Columns	Correlation Coefficient of
---------	----------------------------

Card 1:		
1 - 8	β_{11} with β_{11}	(1.0)
Card 2:		
1 - 8	β_{11} with β_{22}	
9 - 16	β_{22} with β_{22}	(1.0)
Card 3:		
1 - 8	β_{11} with β_{33}	
9 - 16	β_{22} with β_{33}	
17 - 24	β_{33} with β_{33}	(1.0)
Card 4:		
1 - 8	β_{11} with β_{12}	
9 - 16	β_{22} with β_{12}	
17 - 24	β_{33} with β_{12}	
25 - 32	β_{12} with β_{12}	(1.0)
Card 5:		
1 - 8	β_{11} with β_{13}	
9 - 16	β_{22} with β_{13}	
17 - 24	β_{33} with β_{13}	
25 - 32	β_{12} with β_{13}	
33 - 40	β_{13} with β_{13}	(1.0)
Card 6:		
1 - 8	β_{11} with β_{23}	
9 - 16	β_{22} with β_{23}	
17 - 24	β_{33} with β_{23}	
25 - 32	β_{12} with β_{23}	
33 - 40	β_{13} with β_{23}	
41 - 48	β_{23} with β_{23}	(1.0)

Each anisotropic atom has a Standard Deviations card and a Correlation Matrix.

j. Standard Deviations of Atomic Positions FORMAT (3F10.8)

These cards are needed only if bond distances or angles are to be calculated with errors.

Standard Deviations of Atomic Positions (Cont)

Columns	Description
1 - 10	Standard deviation of $\underline{x}$
11 - 20	Standard deviation of $\underline{y}$
21 - 30	Standard deviation of $\underline{z}$

There should be one card of this type for each atom in the input list.

k. Atomic Positions Correlation Matrix FORMAT (10F8.5)

These cards are needed only if bond distances or angles are to be calculated with errors. The lower triangle of this matrix is read by rows with each row starting on a new card. When a row contains more than ten elements, it should be continued on the next card.

Columns	Correlation Coefficient of
Card 1:	
1 - 8	$\underline{x}$ of atom 1 with $\underline{x}$ of atom 1 (1.0)
Card 2:	
1 - 8	$\underline{x}$ of atom 1 with $\underline{y}$ of atom 1
9 - 16	$\underline{y}$ of atom 1 with $\underline{y}$ of atom 1 (1.0)
Card 3:	
1 - 8	$\underline{x}$ of atom 1 with $\underline{z}$ of atom 1
9 - 16	$\underline{y}$ of atom 1 with $\underline{x}$ of atom 2
17 - 24	$\underline{z}$ of atom 1 with $\underline{z}$ of atom 1 (1.0)
Card 4:	
1 - 8	$\underline{x}$ of atom 1 with $\underline{x}$ of atom 2
9 - 16	$\underline{y}$ of atom 1 with $\underline{x}$ of atom 2
17 - 24	$\underline{x}$ of atom 1 with $\underline{x}$ of atom 2
25 - 32	$\underline{x}$ of atom 2 with $\underline{x}$ of atom 2 (1.0)

This scheme should be continued until all elements of the matrix have been punched.

D. METHOD

1. Bond distances:

If X is a column matrix of fractional atomic coordinates for an atom in the asymmetric unit and Y is the column matrix of the coordinates of a symmetry related atom, then Y and X satisfy the following equation:

$$Y = RX + T \quad (1)$$

where R is a rotation-like operation in that it involves axis interchanges and T is a translation operation which includes

glide and screw components as well as origin shifts. Defining Z as a column matrix whose coefficients are the differences in fractional coordinates between an atom at X and an atom at Y , then

$$Z = X - Y \quad (2)$$

If G is defined as the real space metric tensor which has elements

$$g_{ij} = \underline{a}_i \cdot \underline{a}_j \quad (3)$$

where the $\underline{a}$'s are the real space axis vectors, then G is the following matrix:

$$G = \begin{pmatrix} a^2 & ab \cos \gamma & ac \cos \beta \\ ab \cos \gamma & b^2 & bc \cos \alpha \\ ac \cos \beta & bc \cos \alpha & c^2 \end{pmatrix} \quad (4)$$

If Z^T denotes the transpose of Z which involves an interchange of the rows and columns of Z , it may be shown that the square of the bond distance, s^2 , between the atoms is determined by the following matrix equation:

$$s^2 = Z^T G Z \quad (5)$$

In the program, all atoms within a spherical shell centered on each atom in the asymmetric unit are located and the distances are calculated. The size of the spherical shell is determined by the minimum and maximum distances to be considered which are input parameters. The search for the contents of the shell is made efficient by enclosing the central atom with a unit cell shaped parallelôpiped tangent to the sphere with all atomic locations outside this parallelôpiped excluded. The position of those atoms which lie within the spherical shell are stored in a table. This table also includes the atom number and the number of the R matrix used to generate this position which is needed to properly compute the partial derivatives of the bond distance with respect to the positional coordinates. These two numbers are stored in packed form in the same storage location. Each time a new atom is generated, this table is searched to determine whether this atom has already been included. This search assures that atoms in special positions are properly treated although they may be generated in several different ways.

2. Bond angles:

All possible bond angles about each atom in the asymmetric unit are computed using the table of positions prepared during the bond distance calculation. Each pair of atoms from this table is checked to determine whether their distances from the central atom are within the limits, and if so, the bond angle is computed. If

X denotes the column matrix of the central atom with Y_1 and Y_2 denoting the column matrices of the peripheral atoms, the bond angle Θ for the angle $Y_1 - X - Y_2$ can be shown to satisfy the following relationship:

$$\cos \Theta = \frac{(Y_1 - X)^T G (Y_2 - X)}{S_{1X} S_{2X}} \quad (6)$$

Where G is the real space metric tensor (see equation (4))

S_{1X} is the bond distance from the atom of X to the atom at Y_1 and

S_{2X} is the bond distance from the atom at X to the atom at Y_2 .

3. Ellipsoids of Vibration:

The conversion of anisotropic thermal coefficients is a problem of finding the characteristic values and characteristic vectors of a particular matrix. Note that characteristic value, proper value, principal value and eigenvalue are equivalent terms. The matrix equation that must be solved is the following:

$$(B - \lambda G^{-1})Q = 0 \quad (7)$$

where B is the matrix of anisotropic temperature coefficients

λ is a characteristic value of the equation

G^{-1} is the reciprocal space metric tensor with elements

$g_{ij}^{-1} = \frac{b_i}{\text{vectors}} \cdot \frac{b_j}{\text{and}}$ where the b 's are the reciprocal space axis

Q is a column matrix of the coefficients of the characteristic vector. This is a vector in reciprocal space.

If equation (7) is premultiplied by G, it is transformed into the standard form of a characteristic value problem.

$$(GB - \lambda I)Q = 0 \quad (8)$$

where I is the identity matrix and

G is the real space metric tensor defined in equations (3) and (4).

Equation (8) is a set of homogeneous equations of order 3 which have a solution if the determinant of the coefficients is zero. Thus the characteristic values may be found from the equation:

$$\det (GB - \lambda I) = 0 \quad (9)$$

Solution of this equation gives three values of λ which satisfy equation (8). In order to have a meaningful physical situation, it is necessary that the λ 's which are the roots of equation (9) be real and positive. If they are not, the set of temperature coefficients is said to be non-positive definite. This is sometimes referred to as complex amplitudes of vibration or negative temperature factors.

Each of the roots of equation (9) can then be inserted into equation (8) and the resulting equation solved for the characteristic vector by the method of cofactors. After the coefficients of Q are determined, they may be used to form the reciprocal space vector $\underline{q}$ and the angle, θ_i , between this vector $\underline{q}$ and the real space axis vector $\underline{a}_i$ may be found by forming the dot product of the two vectors:

$$\underline{a}_i \cdot \underline{q} = |\underline{a}_i| |\underline{q}| \cos \theta_i \quad (10)$$

This equation may be simplified since

$$\underline{a}_i \cdot \underline{q} = \underline{a}_i \cdot (q_1 \underline{b}_1 + q_2 \underline{b}_2 + q_3 \underline{b}_3) \quad (11)$$

and

$$\underline{a}_i \cdot \underline{b}_j = w_{ij} = \begin{matrix} 1 & \text{for } i = j \\ 0 & \text{for } i \neq j \end{matrix} \quad (12)$$

thus

$$\underline{a}_i \cdot \underline{q} = q_i \quad (13)$$

Equation (12) is the definition of the reciprocal space axis vectors. Equation (10) can now be rewritten

$$\cos \theta_i = \frac{q_i}{|\underline{a}_i| |\underline{q}|} \quad (14)$$

The root-mean-square amplitude of vibration along the i 'th characteristic vector is called μ_i and is found from the i 'th root, λ_i of equation (9) by the following relationship:

$$\mu_i = (\lambda_i / 2\pi^2)^{1/2} \quad (15)$$

4. Error Analysis:

If y is a computed value which is a function of experimentally determined variables $x_1, x_2, \dots, x_n$ such that:

$$y = y(x_1, x_2, \dots, x_n) \quad (16)$$

then the variance of y , denoted by σ_y^2 is found from the equation

$$\sigma_y^2 = \sum_{i=1}^n \sum_{j=1}^n \frac{\partial y}{\partial x_i} \frac{\partial y}{\partial x_j} \text{cov}(x_i, x_j) \quad (17)$$

where $\text{cov}(x_i, x_j)$ is the ij 'th element in the variance-covariance matrix of the x 's.

In crystallographic calculations, the variables for which the variance-covariance matrix elements are known include the unit cell parameters, the atomic positions and the temperature factor coefficients. If the dependence of the bond distance on temperature factors is neglected, as is done in this program, the error in the bond distance will depend only on the cell parameters and the atomic positions. Similarly the ellipsoids will depend only on the unit cell parameters and the temperature factor coefficients. Thus, for crystallographic problems, equation (17) may be rewritten in the form:

$$\begin{aligned} \sigma_y^2 = & \sum_{i=1} \sum_{j=1} \frac{\partial y}{\partial a_i} \frac{\partial y}{\partial a_j} \text{cov}(a_i, a_j) \\ & + \sum_{i=1}^m \sum_{j=1}^m \frac{\partial y}{\partial z_i} \frac{\partial y}{\partial z_j} \text{cov}(z_i, z_j) \end{aligned} \quad (18)$$

where the a 's are the unit cell parameters and the z 's are the atomic parameters. The variance-covariance matrix is the inverse of the normal equations least squares matrix. The error formula in equation (18) is a "full matrix" error formula. The so-called "diagonal" form includes only the terms in equation (18) which have $i=j$. This approximation usually gives a smaller error. All partial derivatives required for computing the errors are analytically evaluated in this program. This procedure is better than numerical differentiation because it is more accurate, easier and faster to do and allows singularities in the derivatives to be detected easier. The necessary derivatives are evaluated using the chain rule of derivatives.

E. OUTPUT

1. General Output:

The first output consists of the information contained on the Title Card. Then the real space axis lengths, the cosines of the real space angles, the reciprocal space axis lengths and the cosines of the real space angles, the reciprocal space axis lengths and the cosines of the reciprocal angles are printed. The real space cell volume is also printed. Then the lattice type and

centric indicator is printed followed by the symmetry operations. Next, if errors are to be calculated, the standard deviations of the cell parameters and the cell parameter correlation matrix are printed. Then the atomic positions and temperature factors are printed. If ellipsoids and errors are to be calculated, the standard deviations of the thermal parameters and temperature factors are printed. If ellipsoids and errors are to be calculated, the standard deviations of the atomic positions and the correlations matrix for the positions are then printed. This completes the general output.

2. Bond Distance and Angle Output:

For each atom in the asymmetric unit, all atoms within the bond distance limits are generated. These atoms are added to a table of generated positions. For each bond distance within the allowable range, the atom identifier, the fractional coordinates, the bond distance, the error, if calculated, and the number of this atom in the table are printed. In the bond angle section of the program, all atoms except those in the asymmetric unit will be referenced by this atom number rather than by coordinates. This number makes it easy to determine quickly what angle has been calculated.

The bond angle section output consists of the atom identifier and coordinates of the central atom which is one of those in the asymmetric unit. The peripheral atoms are each referenced by an atom identifier and an atom table number. The bond angle and its error, if calculated, complete the output for each angle.

3. Ellipsoid of Vibration Output:

For each anisotropic atom, the equivalent isotropic B and its error are calculated and printed. Then for each of the characteristic values, the r.m.s. amplitude of vibration and the angles that the associated characteristic vector makes with the real cell axes as well as the errors in these quantities are printed. No output occurs for isotropic atoms.

4. Page Estimates:

The main program will produce approximately one page of output plus $1/2$ page per atom if errors are to be calculated. The bond distance and angle subroutine will require about one page for each 60 distances or angles calculated. However, the user should keep the bond distance limits as small as possible since if n distances are within the limits, the number of angles computed will be approximately $1/2 n^2$. The ellipsoids of vibration subroutine will require one page for each three atoms.

F. PROGRAM ERRORS AND ERROR STOPS

1. There are two kinds of errors which return control to the monitor through a STOP statement. If a symmetry card cannot be interpreted because the information is not of the correct form or because it is punched in the wrong columns, the program executes a STOP 11 statement and returns to the monitor. The card in error will be the last symmetry card listed on the output. If the user attempts to read more than 24 symmetry cards, the program will return to monitor with a STOP 22 instruction. A different kind of error can occur in the bond distance calculation. If the distance limits are such that more than 1000 atom positions are generated, the program prints a diagnostic message and returns to the main program. This error does not terminate the program and ellipsoids of vibration may be calculated correctly after this condition occurs. However, bond angles will not be calculated.

G. COMMON VARIABLES AND DESCRIPTION

XYZ(3,60)	- Fractional coordinates of atoms in asymmetric unit
BETA(6,60)	- Temperature factor coefficients
A(3)	- Real cell axis lengths
ANG(3)	- Cosines of the real cell angles
AS(3)	- Reciprocal axis lengths
CS(3)	- Cosines of the reciprocal cell angles
ATOM(2,60)	- Atom identifiers
SIGA(6,6)	- Variance-covariance matrix for real cell parameters
SIGB(6,6,60)	- Variance-covariance matrix for thermal coefficients
RS(3,3,48)	- Rotational matrix part of symmetry operator
TS(3,48)	- Translational part of symmetry operator
TP(4,3)	- Location of lattice points in fractional coordinates
ITF(60)	- Temperature factor type indicator
CORR(16290)	- Variance-covariance matrix for atomic positions. This is stored in packed form.
XYZP(3,1000)	- Fractional coordinates of atoms generated in the bond distance subprogram.
IATP(1000)	- Atom identifier of atoms generated in bond distance calculation.
NA	- Number of atoms in asymmetric unit
NSS	- Number of symmetry operations
VOL	- Volume of real space unit cell
DLIMIT(3)	- Array of bond distance limits
PI	- The value of the constant π
G(3,3)	- Real space metric tensor
NLP	- Number of lattice points in the unit cell
IERR	- Error calculation indicator
TITLE(18)	- Alphanumeric title information

H. PROGRAM NAMES AND DESCRIPTION

1. U M BADTEA:

This is the main program which handles the input and calls the bond distance and ellipsoid of vibration programs.

2. BODAN(IBOD):

This subprogram calculates bond distances and errors and if the argument IBOD is equal to 2, calculates the bond angles and errors.

3. ELVIB:

This subprogram calculates the ellipsoid of vibration parameters and associated errors.

4. VARIAN(A,B,C,D,E,II):

This subprogram calculates the variance of a computed value where the partial derivatives of the value with respect to the cell parameters are stored in array B, the partial derivatives with respect to the structure parameters are stored in array C, the cell covariance matrix is stored in array D, the structure parameters covariance matrix is in array E, the argument II contains the atom number when the variance of ellipsoid parameters is calculated otherwise it contains 1 and the computed variance is output in argument A.

5. CELLD(B,A,AN,R,CS,VOL):

This subprogram computes the partial derivatives of the reciprocal cell parameters with respect to the real cell parameters. These derivatives are used in computing the ellipsoid errors. Array B contains the partial derivatives after execution. Arrays A, AN, R and CS are the input values of the real cell axis lengths, the real cell cosines, the reciprocal axis lengths and cosines of the reciprocal cell angles respectively. The argument VOL is the input value of the real cell volume.

6. DERDET(A,B,C):

This subprogram calculates the partial derivatives of matrix B with respect to the thermal coefficients and stores them in array A. Array C contains an intermediate set of partial derivatives.

7. CORRL(SIGZ,NN,II,JJ,CORR,KK,LL,MM):

This subprogram prepares the atomic positional correlation matrix for atoms II and JJ from the packed matrix CORR of rank MM and stores it at the KK,LL position of the array SIGZ which is of rank NN.

I. SYSTEM REQUIREMENTS

U M BADTEA requires two tape units, a standard input tape and a standard output tape. All input is BCD from Logical Unit Number 5 while output is BCD to Logical Unit Number 6. The program requires approximately 32K storage locations. If the modified ORFFE tape is to be used, it is read from logical unit 4.

Appendix C

LISTINGS OF PROGRAMS

Fortran listings of all programs and subprograms are included herein. Example runstreams, with the output they produce, are available on request from either author.


```

SUMAX=F0HIN,RHOMN,RHONK,(JSCREF(1),I=1,NSF),NRSE
9,NPAR,(PAR(1),,(PARNAM(J,I),J=L+2),IPAR(1),,(=1,NPAR),FISGN)RNFEL1750
O,IFSGN,EGGY,KEXTRF
RNFEL1760
READIISCL J
1((RANDOM(J,I),J=L+2),I=1,NSCAT),TEXT,EXTIN,((TAG(J,I),J=L+2),ISOT(1)RNFEL1770
2,((ISCAT(J,I),J=L+2),FOCAT(1),OCUP(1),SITE(1),TXZ(J,I),J=L+2),RNFEL1780
3,((SCAT(J,I),J=L+2),FOCAT(1),OCUP(1),SITE(1),TXZ(J,I),J=L+2),RNFEL1790
4,DEGA,(KDEGN(1),I=1,IOEGN)
RNFEL1800
NOEGN,LDGEM/2
WRITE(IUOUT,33)LABEL
C CHECK FOR NEW PARAMETERS
140 IF(NEW(1))150,180A,150
C READ NEW CELL PARAMETERS AND CALCULATE RECIPROCAL CELL
150 READ(IN,6)I(1),I=1,146)
WRITE(IUOUT,9)I(1),I=1,6)
IF(ABST(A(1))-90-O1=0.001115A,155,155
154 A(1)=0.0
GO TO 160
155 A(1)=COS(A(1)*PI/180,O)
160 CONTINUE
I=0
170 J=L+1
I=I+1
G(1,I)=A(1)*PI*2
G(1,I)=G(1,I)
G(3,I)=A(3)*PI*2
G(6)=G(3,I)
CALL SYMINV(B,3,4,0,A,1,0E-10,VOL,JRANK)
VOL=SQRT(VOL)
RECELL(1)=SORT(8(1))
RECELL(2)=SORT(8(4))
RECELL(3)=SORT(8(6))
RECELL(4)=8(13)/(RECELL(1)*RECELL(3))
RECELL(5)=8(15)/(RECELL(1)*RECELL(3))
RECELL(6)=8(12)/(RECELL(1)*RECELL(2))
EGGY(1)=4/(RECELL(1)*2)
EGGY(2)=4/(RECELL(2)*2)
EGGY(3)=4/(RECELL(3)*2)
EGGY(4)=4/(RECELL(1)*RECELL(2))
EGGY(5)=4/(RECELL(1)*RECELL(3))
EGGY(6)=4/(RECELL(2)*RECELL(3))
180 IF(FIRST,EGGY(1),EGGY(2),EGGY(3),EGGY(4),EGGY(5),EGGY(6),AND,NPAR,NE-O1CALL THNRM
C NEW BOND DISTANCE LIMITS
190 OMN=BUFF(1)
OMAX=BUFF(2)
200 IF(NEW(3))1210,420A,210
C NEW SYMMETRY OPERATORS
210 ICENT=18UFF(13)
RNFEL1740
WRITE(IUOUT,7)
220 CELLP(1,I)=0.0
JCELL=1
ICELL=18UFF(4)
IF(ICELL,230,320A,230)
240 IF(ICELL,322,322A,300)
JCELL=2
240 CELLP(1,I)=0.5
GO TO 320
250 CELLP(1,I)=0.0
GO TO 320
270
GO TO 320
280 CELLP(4,I)=0.5
JCELL=4
290 CELLP(1,I)=0.0
GO TO 320
300 JCELL=3
DO 310 I=2,3
CELLP(1,I)=FLOAT(I-1)/3.0
CELLP(2,I)=FLOAT(I-1)/3.0
310 CELLP(3,I)=CELLP(2,I)
C READ NEW SYMMETRY CARDS
320 NSYM=0
330 NSYM=NSYM+1
READ(IN,12)I(JTNS(I),(IRMAT(K,I),K=1,2),I=1,3),IEF
WRITE(IUOUT,13)I(JTNS(I),(IRMAT(K,I),K=1,2),I=1,3),IEF
IF(JTNS(I)-I)NS(J)340,350,340
340 WRITE(IUOUT,6A)NSYM
CALL EXIT
350 TRANS(I,NSYM)=TRS(J)
RMAT(J,I,NSYM)=0.0
DO 390 J=1,3
I=IRMAT(K,J)
DO 360 K=1,2
IF(ABST(I)-1)330A,370,360
360 CONTINUE
GO TO 342
370 IF(1-1AB5(KRMAT(I))390,380A,390)
380 RMAT(J,I,NSYM)=SIGN(1,KRMAT(I))
390 CONTINUE
400 IF(IEF,420,400A,420)
410 WRITE(IUOUT,68)
420 IF(NEW(4))430,460A,430
C READ NEW SCATTERING FACTORS
430 NSCAT=18UFF(6)
WRITE(IUOUT,31)I(1,I=1,4)
IF(NSCAT*(NSCAT-21))43A,432A,432
432 CALL EXIT
RNFEL2320
RNFEL2330
RNFEL2340
RNFEL2350
RNFEL2360
RNFEL2370
RNFEL2380
RNFEL2390
RNFEL2400
RNFEL2410
RNFEL2420
RNFEL2430
RNFEL2440
RNFEL2450
RNFEL2460
RNFEL2470
RNFEL2480
RNFEL2490
RNFEL2500
RNFEL2510
RNFEL2520
RNFEL2530
RNFEL2540
RNFEL2550
RNFEL2560
RNFEL2570
RNFEL2580
RNFEL2590
RNFEL2600
RNFEL2610
RNFEL2620
RNFEL2630
RNFEL2640
RNFEL2650
RNFEL2660
RNFEL2670
RNFEL2680
RNFEL2690
RNFEL2700
RNFEL2710
RNFEL2720
RNFEL2730
RNFEL2740
RNFEL2750
RNFEL2760
RNFEL2770
RNFEL2780
RNFEL2790
RNFEL2800
RNFEL2810
RNFEL2820
RNFEL2830
RNFEL2840
RNFEL2850
RNFEL2860
RNFEL2870
RNFEL2880
RNFEL2890

```

[illegible]

[illegible]


```

C      PUNCH 6TH CUMULANT
7095 WRITE(IIPUN,7095)(OR(J,I),J=1,15)
7096 FORMAT(10F6.6)
7097 CONTINUE
C      PUNCH THE SPECIAL PARAMETERS
WK(TETIPUN,90INPAR)
CALCULATE THE SPECIAL PARAMETERS
C      PUNCH THE EXTINCTION AND TEMPERATURE FACTOR TYPES
7100 WRITE(IIPUN,10EXTN,(11FBUFI(I),I=1,NATOM)
GO TO 7083
7086 WRITE(10UT,7087)NFLAG
7087 FORMAT(10X,WRUNG VALUE OF NFLAG,ACTUAL VALUE (5*,(3)
7088 CONTINUE
9970 IF(NSF=219980,9970,9970)
CCG=CCG+((SCATJ(J),J=1,2),ISOT(1),((SCAT(J,I),I=1,2),
CCG=CCG+((SCATJ(J),J=1,2),ISOT(1),((SCAT(J,I),I=1,2),
9971 N=1,NATOM,(SIG(I),SIG(XYZL(J,I),J=1,3),SIGR(J,I),J=1,6),I=1,
SM)
END FILE ISC4
9980 CONTINUE
C      END OF CALCULATION
4000 REMIND ISCI
C      END OF FILE SAVE UNIT
4010 LOGEN=2*MOEGN
WRITE(11SC1)
1KCYL=LABEL*RECELL,G*VOL,NSYM,NATOM,NSCAT,JCELL,MRANK,NPARA,NSF,OHIRFNE1300
2N,OMAX,DELMAX,ICENT,((IRMAT(I,J,K),I=1,3),J=1,3),K=1,NSYM),((TRANSRFNE1310
3(I,J),I=1,3),J=1,NSYM),((ICELL(I,J),I=1,3),J=1,JCELL),((IPARA(I),I=1,NSCAT)-IREJ,RFNE1320
41,NPARA),((FCURVE(I,J),I=1,9),J=1,NSCAT),ISCALE(I),I=1,NSF)-IREJ,RFNE1330
5ORAX,FOMIN,RHOMN,RHOMX,(USCRF(I),I=1,NSF)-NRSF
6,((TAG(I),I=1,NPARA),J=1,2),IPAR(I),I=1,NPAR),FISG(J,I),I=1,NSCAT)
0,NSG,EGY,KEXTNR
WRITE(11SC1)
1((NATOM,J,I),J=1,2),I=1,NSCAT),1EXT,EXTN,((TAG(J,I),J=1,2),((SOT(1),RFNE1380
2,((SCAT(J,I),J=1,2),OCCAT(I),OCCUP(I),SITE(I),((XYZ(J,I),J=1,3),
3(BETA(J,I),J=1,6),ICR(J,I),J=1,10),TOR(J,I),J=1,15),I=1,NATOM),
4MOEGN,(MOEGN(I),I=1,MOEGN)
4020 READ(ISC2)(11BUFI(I),I=1,18BUFI)
WRITE(11SC1)(11BUFI(I),I=1,18BUFI)
4030 REMIND ISCI
4040 REMIND ISCI
IF(1FIRST-EO-O-AND-MFSEL-EO-O(GO TO 4062
(K=MOEGN+1
(J=MOEGN+(MRANK*(MRANK+1))/2
WRITE(11SC1)MOEGN,(A(J),J=1,MOEGN)
WRITE(11SC1)(A(J),J=1,IJ)
WRITE(11SC1)(11BETA(J,I),J=1,6),SIGO(I),((SIG(XYZL(J,I),J=1,3),SIGR(J,I),I=1,6),I=1,NATOM)
1END FILE ISCI
4062 REMIND ISCI
C      END OF THIS ROUTINE IF NEW PARAMETERS ARE TO BE SAVED
C      RETURN
C      END OF RUN FOR NEW PARAMETERS NOT SAVED
4080 CALL EXIT
END

```

```

BLOCK DATA
INCLUDE IN023.LIST
DATA IN021,1,2,2,3,3,1,2,1,3,2,2,3/IN03/1,1,1,2,2,2,3,3,1,1,2,1,
12,2,1,1,3,1,3,2,2,3,2,2,3,3,1,2,3/
INCLUDE TAPE.LIST
DATA IN,10UT,ISCI,ISC2,ISC3,ISC4,ISC5,1PUN/5,6,10,29,11,12,26,1/
END
INCM 10
INCM 30
INCM 40
INCM 50
INCM 60
INCM 70

```



```

C          COMPILER (FLD=0)
C          SUBROUTINE NDEGN
C          THEN IN ORDER OF INDEPENDENT RELATIONSHIPS AND ARRANGE
C          DEFINE I1(K)=FLD(0,9,K)
C          DEFINE I2(K)=FLD(0,9,K)
C          DEFINE I3(K)=FLD(0,9,K)
C          DEFINE I4(K)=FLD(0,9,K)
C          DEFINE I5(K)=FLD(0,9,K)
C          INCLUDE OCEN,LIST
C          INCLUDE TAPE,LIST
C          DIMENSION IDPAR(2),INPAK(2,5),CNPAK(5)
C          NDEGN=0
C          KMAX=2640
C          KPI=1
C          DO 9000 I=1,N,9000 IDPAR((INPAK(I,J),I=1,2),CNPAK(J),J=1,5)
C          FORMAT(21,31,31,31,31,31)
C          IF IDPAR(1),EQ,0,AND, IDPAR(2),EQ,0 GOTO 100
C          DO 20 I=1,5
C          IF INPAK(1),EQ,0,AND, INPAK(2,1),EQ,0,AND, CNPAK(1),EQ,0, GOTO 100
C          IF INPAK(2,1),LT,0 GOTO 12
C          KDEGN(KP)=INPAK(INPAK(1,1),INPAK(2,1),IDPAR(1),IDPAR(2))
C          AAK(KP)=CNPAK(1)
C          KP=KP+2
C          NDEGN=NDEGN+1
C          IF KP,LT,KMAX GOTO 20
C          TOP MANY RELATIONS
C          11 WRITE(10UT,9011)
C          FORMAT(10T69 MANY DEPENDENCY RELATIONS, RUN ABORTED,1)
C          STOP
C          RUN+ INDICATED ON DEPENDENCY CARD.
C          12 IF (MOD(I,2),NE,0),KP=INPAK(1,1),NE,0 GOTO 16
C          JMAX=INPAK(2,1)
C          JMAX=JMAX+1
C          DO 15 J=JMIN,JMAX
C          KOFGN(KP)=INPAK(INPAK(1,1),J,IDPAR(1),IDPAR(2))
C          AAK(KP)=0.
C          KP=KP+2
C          NDEGN=NDEGN+1
C          IF KP=KNAX)15,11,11
C          CONTINUE
C          15 GO TO 20
C          16 WRITE(10UT,9016)
C          FORMAT(101MP=KPEP DEPENDENCY INFORMATION, RUN ABORTED,1)
C          STOP
C          20 CONTINUE
C          GO TO 10
C          RESHUFFLE CONSTRAINT INDICATORS TO GROUP THEM ACCORDING TO THE
C          INDEPENDENT PARAMETER.
C          100 KDEGN=1
C          DO 110 I=1,11
C          J=I+1
C          DO 110 J=J,J,NDEGN
C          IF (KDEGN(2+I-1)-KDEGN(2+J-1))110,110,
C          ITEMP=KDEGN(2+I-1)
C          TEMP=AAI(2+I)
C          KDEGN(2+I-1)=KDEGN(2+J-1)

```


72

[illegible]

76

```

IF(IIFSGN-EQ-0)GO TO 396
C EVALUATE STRUCTURE FACTOR FOR KINEMATOPHIC ORIENTATION
AMINUS=TEMP*(1-TEMP*BB1*OAT*TEMP*BB1*OAT*AMINUS)
BMINUS=TEMP*(1-TEMP*BB1*OAT*TEMP*BB1*OAT*AMINUS)
C EVALUATE INDIVIDUAL ATOM CONTRIBUTIONS
396 BINOL(L)=TEMP*(TEMP*AA1NOI-TEMP*BB1NOI)
BINOL(L)=TEMP*(TEMP*AA1NOI-TEMP*BB1NOI)
ACALC=ACALC+BINOL(L)
BCALC=BCALC+BINOL(L)
IF(MFSEL)4000+450+400
C MODIFY DERIVATIVES
400 TEMPS=TWU1*TEMP*
00 410 IAG=1,3
OAOXI(IAG,L)=TEMP*(TEMP*OAOXI(IAG)-TEMP*OXB(IAG))
OAOXI(IAG,L)=TEMP*(TEMP*OAOXI(IAG)-TEMP*OXB(IAG))
IF(IISOT(L))430+420+430
C DERIVATIVE WITH RESPECT TO ISOTROPIC TEMPERATURE FACTOR
420 OAOBI(L)=RH0*AINOL(L)
OAOBI(L,L)=RH0*BINOL(L)
GO TO 450
C DERIVATIVES WITH RESPECT TO ANISOTROPIC TEMPERATURE FACTOR
430 OAOB(IAH,L)=TEMP*(TEMP*OAB(IAH)-TEMP*OBB(IAH))
OAOB(IAH,L)=TEMP*(TEMP*OAB(IAH)-TEMP*OBB(IAH))
IF(IISOT(L))450+450+441
C DERIVATIVES WRT THE THIRD CUMULANT
441 00 442 IO=1,10
OAOI(10,L)=TEMP*(TEMP*OACI(10)-TEMP*OBCI(10))
OAOI(10,L)=TEMP*(TEMP*OACI(10)-TEMP*OBCI(10))
IF(IISOT(L))450+450+443
C DERIVATIVES WRT THE FOURTH CUMULANT
443 00 444 IO=1,15
OAOI(10,L)=TEMP*(TEMP*OAOI(10)-TEMP*OBOI(10))
OAOI(10,L)=TEMP*(TEMP*OAOI(10)-TEMP*OBOI(10))
444 0800(10,L)=TEMP*(TEMP*OAOI(10)-TEMP*OBOI(10))
450 CONTINUE
450 MFSEL=ISAVE
470 RETURN
ENTRY EXCALC
C CALCULATE EXTINCTION FACTOR
IF(IEXT)1010+1000+1010
C ISOTROPIC FORM
1000 EX=EXBETA*EXTIN(1)*FCALC
OROE(1)=1.0
RETURN
C CALCULATE ISOTROPIC EXTINCTION - CALCULATE TRIG FUNCTIONS OF ANGLES
1010 SCALC=SIN(XANG(1))
GCALC=COS(XANG(1))
SPHI=SIN(XANG(2))
CPHI=COS(XANG(2))
IF(IEXT-1)1030+1020+1030
C TYPE 1 CORRECTION
1020 VI(1)=SPHI*SCALC
VI(2)=CPHI*SCALC
VI(3)=GCALC*SPHI
GO TO 1040
C TYPE 2 ANISOTROPIC
1030 SNU=SIN(XANG(3))

```

```

CNU=COS(XANG(3))
VI(1)=CNU*SPHI*CNUSNU*CPHI
VI(2)=CNU*SPHI*CNUSNU*SPHI
VI(3)=SGHT*CNUSNU
C FOR PRODUCTS OF COEFFICIENTS
1040 00 1050 I=1,3
1050 VV(1)=VI(1)*e2
VV(4)=2.0*V(1)*V(2)
VV(5)=2.0*V(1)*V(3)
VV(6)=2.0*V(2)*V(3)
00 1060 I=1,6
1060 SUM=SUM+VV(I)*EXTIN(I)
IF(SUM-LE-0.0)SUM=1.0
TEMP=-1.0/SORT(SUM)
EX=EXBETA*FCALC*ABS(TEMP)
C CALCULATE DERIVATIVES OF THE FORM DF=STAR/OF-LJ
00 1070 I=1,6
1070 UROET(I)=0.5*VV(1)*TEMP/SUM
END

```

```

SFAC1740
SFAC1760
SFAC1780
SFAC1790
SFAC1800
SFAC1810
SFAC1820
SFAC1830
SFAC1840
SFAC1850
SFAC1860
SFAC1870
SFAC1880
SFAC1890
SFAC1900
SFAC1910
SFAC1920
SFAC1930
SFAC1940
SFAC1950
SFAC1960
SFAC1970
SFAC1980
SFAC1990
SFAC2000
SFAC2010
SFAC2020
SFAC2030
SFAC2040
SFAC2050
SFAC2060
SFAC2070
SFAC2080
SFAC2090
SFAC2100
SFAC2110
SFAC2120
SFAC2130
SFAC2140
SFAC2150
SFAC2160
SFAC2170
SFAC2180
SFAC2190
SFAC2200
SFAC2210
SFAC2220
SFAC2230
SFAC2240
SFAC2250
SFAC2260
SFAC2270
SFAC2280
SFAC2290
SFAC2300
SFAC2310

```



```

IJ=IPARA(IK)
IF(IJ)232,233,232
232 DERIV(IJ)*ACALC=OAOCL(J)*BCALC=OBDOCL(L,J)
2322 IF(I1)INDEX(I1)=IJ,2326,233
2324 II=I1+2
2326 CALL MODIFY(ORIV(IJ),I1,LOEGR(I1),I1(LDEGR(I1)),A(I1+1))
233 CONTINUE
G6 TO 2322
G6 TO 2324
C
IF(I8RT(IJ)-2)240,240,234
234 06 DERIVATIVES WRT TO THE FOURTH CUMULANT
L=I1,15
IF(I1)1
IJ=IPARA(IK)
IF(IJ)235,236,235
235 ORIV(IJ)*ACALC=DADU(L,J)*BCALC=OBDR(L,J)
2352 IF(I1=MOEGR(I1))236
2354 II=I1+2
2356 CALL MODIFY(ORIV(IJ),I1,LOEGR(I1),I1(LDEGR(I1)),A(I1+1))
2356 G6 TO 2354
236 CONTINUE
240 CONTINUE
C
FORM MATRICES
INDEX=MDEGN*1
06 260 M=1,MRANK
TEMP=ORIV(IJ)*WT
INDEX=INDEX+260
250 INDEX=INDEX*MRANK-M*1
G6 TO 260
260 A(INDEX)=A(INDEX)+TEMP*ORIV(N)
270 INDEX=INDEX+1
8(M)=8(M)-DELTA*TEMP
280 CONTINUE
RETURN
END

MATK1160
MATK1170
MATK1180
MATK1190
MATK1200
MATK1210
MATK1220
MATK1230
MATK1240
MATK1250
MATK1260
MATK1270
MATK1280
MATK1290
MATK1300
MATK1310
MATK1320
MATK1330
MATK1340
MATK1350
MATK1360
MATK1370
MATK1380
MATK1390
MATK1400
MATK1410
MATK1420
MATK1430
MATK1440
MATK1450
MATK1460
MATK1470
MATK1480
MATK1490
MATK1500
MATK1510
MATK1520
MATK1530
MATK1540

SUBROUTINE MODIFY(ORIV,NA,NP,TEMP)
INCLUDE OCMA.LIST
IF(NP,GE,2)G6 TO 100
ORIV=ORIV*TEMP*(ACALC=OAOH(NA)*BCALC=OBH(NA))
RETURN
100 IF(NP,GE,5)G6 TO 200
ORIV=ORIV*TEMP*(ACALC=OAOX(NP-1,NA)*BCALC=OBH(NP-1,NA))
RETURN
200 IF(NP,GE,11)G6 TO 300
ORIV=ORIV*TEMP*(ACALC=DAH(NP-4,NA)*BCALC=OBH(NP-4,NA))
RETURN
300 IF(NP,GE,21)G6 TO 400
ORIV=ORIV*TEMP*(ACALC=OADC(NP-10,NA)*BCALC=OBH(NP-10,NA))
RETURN
400 ORIV=ORIV*TEMP*(ACALC=OADD(NP-20,NA)*BCALC=OBH(NP-20,NA))
RETURN
END

C
DUMMY SUBROUTINES SPVAL AND SPOERI
SUBROUTINE SPVAL
RETURN
ENTRY SPOERI
RETURN
END

SPVL 10
SPVL 20
SPVL 30
SPVL 40
SPVL 50
SPVL 60

```



```

D3DL 10
D3DL 20
D3DL 30
D3DL 40
D3DL 50
D3DL 60
D3DL 70
D3DL 80
D3DL 90
D3DL 100
D3DL 110
D3DL 120
D3DL 130
D3DL 140
D3DL 150
D3DL 160
D3DL 170
D3DL 180
D3DL 190
D3DL 200
D3DL 210
D3DL 220

FUNCTION D3KDL R,EL,S,I,J,K,L,M)
  DIMENSION R(3),EL(3,3),S(3,3)
  DEFINE ABK J,K,L,M,N)*2,*AIJ(R,J,L)*BIJK(R,K,M,N)
  INTEGER P
  DEFINE PFI J,K,L,M,N)*PIJELM(R,I,J,K,L,M)
  SUM=SUM+AIJ(R,J,K)
  Dg 1000 N*1,3
  SUM=SUM+EL(M,N)*ABK(E,K,L,M,N)*ABK(J,K,M,L,N)*ABK(K,D3DL 90
  1 J,M,L,N))*S(N,J)*(ABK(I,K,L,M,N)*ABK(E,I,L,M,N)*ABK(I,K,M,L,N)*ABK(I,K,D3DL 100
  2 J)*ABK(E,I,M,L,N))*S(N,K)*(ABK(I,J,L,M,N)*ABK(J,I,L,M,N)*ABK(I,J,D3DL 110
  3 J,M,L,N)*ABK(J,I,M,L,N))
  Dg 1000 P*1,3
  SUM=SUM+SQ(J)*S(P,K)*PP(I,N,P,L,M)*S(N,I)*SQ(P,K)*PP(I,N,P,L,M)
  1 *S(N,I)*SQ(J)*PP(E,K,L,M,N)*S(N,I)*SQ(P,K)*PP(I,N,P,L,M)
  2 *S(N,I)*SQ(J)*PP(E,K,L,M,N)*S(N,I)*SQ(P,K)*PP(I,N,P,L,M)
  3 *ABK(I,K,N,P,L,M)*ABK(J,K,I,P,L,M)
  1000 CONTINUE
  D3KDL=SUM
  IP(L,EO,M)*D3KDL=SUM/2.
  RETURN
END

FUNCTION D3KDS(R,EL,S,I,J,K,LP,MP)
  DIMENSION R(3),EL(3,3),S(3,3)
  INTEGER P
  DEFINE ABK(E,K,L,M)*2,*BIJK(R,K,L,M)
  DEFINE ABK(J,K,L,M)*2,*AIJ(R,J,L)*BIJK(R,K,M,N)
  SUM=0.
  Dg 1000 L*1,3
  Dg 1000 M*1,ND,I,EO,MP)SUM=SUM*(M,J)*BBK(E,L,M)*S(M,K)*BBK(J,L,M)
  IF(M,EO,LP,AND,J,EO,MP)SUM=SUM*(L,I)*BBK(E,L,M)
  IF(M,EO,LP,AND,K,EO,MP)SUM=SUM*(L,I)*BBK(J,L,M)*S(L,J)*BBK(I,L,M)
  IF(L,EO,LP,AND,J,EO,MP)SUM=SUM*(M,K)*BBK(I,L,M)
  Dg 1000 N*1,3
  IF(L,NE,LP)Gg Tg 500
  IF(L,EO,MP)SUM=SUM*(EL,M,N)*(ABK(J,E,M,L,N)*ABK(E,J,M,L,N))
  IF(J,EO,MP)SUM=SUM*(EL,M,N)*ABK(I,K,M,L,N)*ABK(E,I,M,L,N)
  IF(K,EO,MP)SUM=SUM*(EL,M,N)*ABK(I,J,M,L,N)*ABK(E,I,M,L,N)
  Dg 1000 LP)Gg Tg 750
  IF(J,EO,MP)SUM=SUM*(EL,N,P)*S(M,K)*PIJELM(R,I,L,M,N,P)
  IF(I,EO,MP)SUM=SUM*(EL,N,P)*S(M,K)*PIJELM(R,J,L,M,N,P)*S(M,J)*
  1 PIJELM(R,K,L,M,N,P))
  IF(M,NE,LP)Gg Tg 1000
  IF(K,EO,MP)SUM=SUM*(EL,N,P)*S(L,J)*PIJELM(R,I,L,M,N,P)*S(L,I)*
  1 PIJELM(R,J,L,M,N,P))
  IF(J,EO,MP)SUM=SUM*(EL,N,P)*S(L,I)*PIJELM(R,I,L,M,N,P)*S(L,I)*
  1000 CONTINUE
  D3KDS=SUM
  RETURN
END

```

```

D2DS 10
D2DS 20
D2DS 30
D2DS 40
D2DS 50
D2DS 60
D2DS 70
D2DS 80
D2DS 90
D2DS 100
D2DS 110
D2DS 120
D2DS 130
D2DS 140
D2DS 150
D2DS 160
D2DS 170

FUNCTION D2KDS(R,EL,I,J,K,EL,S)
  DIMENSION R(3),EL(3,3)
  DEFINE CCC(J,K,L,M)*3,*CIJ(R,J,K,I,L,M)
  SUM=0.
  IF(I,NE,LP)Gg Tg 1000
  SUM=SUM+AIJ(R,J,K)
  Dg 500 M*1,3
  SUM=SUM+EL(M,N)*CCC(J,K,M,N)
  500 IF(J,NE,LP)Gg Tg 2000
  1000 IF(J,M,L,N)*CCC(J,K,M,N)
  SUM=SUM+EL(I,K)
  Dg 1500 M*1,3
  Dg 1500 N*1,3
  SUM=SUM+EL(M,N)*CCC(I,K,M,N)
  1500 D2KDS=SUM
  2000 RETURN
  END

FUNCTION TKTL(R,I,J,K,EL,S)
  DIMENSION R(3),EL(3,3),S(3,3)
  INTEGER P
  DEFINE BK(E,L,M)*BIJK(R,K,L,M)
  DEFINE A(I,J)*AIJ(R,I,J)
  SUM=0.
  Dg 1000 I*1,3
  SUM=SUM+2,*S(L,I)*S(M,J)*BK(E,L,M)*S(L,I)*S(M,K)*BK(J,L,M)*S(L,J)*
  1 S(M,K)*BK(I,L,M))
  Dg 1000 N*1,3
  SUM=SUM+2,*EL(M,N)*S(L,I)*(A(J,M)*BK(E,L,N)*A(K,M)*BK(J,L,N))*S(L,ITKTL 120
  1 J*(A(I,M)*BK(E,L,N)*A(K,M)*BK(I,L,N))*S(L,K)*(A(I,M)*BK(J,L,N)*
  2 A(J,M)*BK(I,L,N)))
  Dg 1000 P*1,3
  Dg 1000 Q*1,3
  SUM=(S(L,J)*SQ(M)*PIJELM(R,I,L,M,N,P)*S(L,I)*S(M,K)*
  1 PIJELM(R,J,L,M,N,P)*S(L,I)*S(M,K)*PIJELM(R,K,L,M,N,P)*2,*EL(I,TKTL 170
  2 M)*A(I,I)*A(J,N)*BK(E,M,P)*A(I,L)*A(K,N)*BK(J,M,P)*A(J,L)*A(K,TKTL 190
  3 BK(I,M,P)))
  1000 CONTINUE
  TKTL=SUM
  RETURN
END

```



```

FUNCTION DIJXLM(R,I,J,K,L,M)
DIMENSION R(3)
IN=J+K+L+M
IF(MOD(IN,6).EQ.0.AND.IN.LE.18)GOTO 1000
IF(MOD(IN,6).EQ.9.OR.IN.EQ.15)GOTO 1060
IF(JI.NE.KI.OR.KI.NE.LI.OR.LI.NE.MI)GOTO 1040
DIJX 10
DIJX 20
DIJX 30
DIJX 40
DIJX 50
DIJX 60
DIJX 70
DIJX 80
DIJX 90
DIJX 100
DIJX 110
DIJX 120
DIJX 130
DIJX 140
DIJX 150
DIJX 160
DIJX 170
DIJX 180
DIJX 190
DIJX 200
DIJX 210
DIJX 220
DIJX 230
DIJX 240
DIJX 250
DIJX 260
DIJX 270
DIJX 280
DIJX 290
DIJX 300
DIJX 310
DIJX 320
DIJX 330
DIJX 340
DIJX 350
DIJX 360
DIJX 370
DIJX 380
DIJX 390
DIJX 400
DIJX 410
DIJX 420
DIJX 430
DIJX 440
DIJX 450
DIJX 460
DIJX 470
DIJX 480
DIJX 490
DIJX 500
DIJX 510
DIJX 520
DIJX 530
DIJX 540
DIJX 550
DIJX 560
DIJX 570
1040 DIV=4,
GOTO 1100
1060 DIV=6,
GOTO 1100
1080 DIV=12,
GOTO 1100
1100 IF(MOD(IN,3).NE.0)GOTO 1500
M=3
IN=IN/3
IF(MOD(IN,3).NE.0)GOTO 1250
L=3
IN=IN/3
IF(MOD(IN,3).NE.0)GOTO 1125
K=3
J=IN/3
GOTO 1900
1125 IF(MOD(IN,2).NE.0)GOTO 1150
J=IN/2
GOTO 1900
1150 K=1
J=J-1
GOTO 1900
1250 IF(MOD(IN,2).NE.0)GOTO 1375
L=2
IN=IN/2
K=2
IF(MOD(IN,2).NE.0)GOTO 1150
J=IN/2
GOTO 1900
1375 L=1
GOTO 1150
1500 IF(MOD(IN,2).NE.0)GOTO 1750
M=2
IN=IN/2
GOTO 1250
1750 M=1
GOTO 1375
1900 GOTO (100,200,300),I
100 GOTO (110,150,2000),J
110 GOTO (120,140,3000),K
120 GOTO (125,130,2000),L
125 GOTO (130,200,2000),M
130 IF(L=2)GOTO 145,4000
140 IF(L=2)GOTO 145,4000
145 IF(M=2)GOTO 4000,3000
150 IF(L=2)GOTO 150,1000
160 IF(L=2)GOTO 170,5000
170 IF(M=2)GOTO 2000,1000
200 GOTO (210,250,2000),J

```

```

210 GOTO (220,240,1000),K
220 GOTO (225,230,2000),L
230 IF(M=2)GOTO 2000,4000,M
240 IF(L=2)GOTO 245,3000
245 IF(M=2)GOTO 3000,1000
250 IF(K=2)GOTO 260,4000
260 IF(L=2)GOTO 270,2000
270 IF(M=2)GOTO 1000,4000
300 GOTO (310,350,1000),J
310 GOTO (325,340,4000),L
325 GOTO (325,330,2000),L
330 GOTO (2600,1000,4000),M
340 IF(L=2)GOTO 345,1000
345 IF(M=2)GOTO 1000,4000
350 IF(K=2)GOTO 360,3000
360 IF(L=2)GOTO 370,2000
370 IF(M=2)GOTO 2000,3000
1000 RETURN
2000 FAC=1,
2010 DIJXLM=FAC*R(I)/(24.*DIV)
RETURN
3000 MM=MOD(I,3)*1
3010 DIJXLM=(R(M))/(24.*DIV)
RETURN
4000 MM=MOD(I,3)*1
GOTO 3010
5000 GOTO 2010
END

```

```

FUNCTION FIJXLM(R,I,J,K,L,M)
DIMENSION R(3)
DEFINE DIJXLM(R,I,J,K,L,M)
FIJXLM=FIJXLM+DIJXLM(R,I,J,K,L,M)
RETURN
END

```

```

FIJX 10
FIJX 20
FIJX 30
FIJX 40
FIJX 50
FIJX 60
FIJX 70
FIJX 80
FIJX 90

```



```

      330 CONTINUE
      C
      S=0.0
      340 YP(K)=XYZ(K,11)-XYP(K)
      XZP=0.0
      350 XZP=XZP+YP(K)*G(K,N)
      360 IP(18-SE*(N-EN-S))=10.0,410.370
      370 S=BOXT(18)
      C
      CHECK IF LIST ARRAYS FULL
      IF(LIST-300)390,380,390
      380 WRITE(IGOUT,8)
      390 IF(LIST-410)
      GO TO 410
      C
      ADD ATOM TO LIST
      NUNK(LIST)=644JJ+J
      400 K=1,3
      410 XPR(K,LIST)=XYP(K)
      IF(NBODAN)410,402,402
      402 WRITE(IGOUT,6)TAG(K,JJ),K=1,2),XYP,S,LIST
      410 CONTINUE
      420 CONTINUE
      430 IP(NBODAN-1)=440,440,450
      440 RETURN
      C
      COMPUTE BAND ANGLES
      450 WRITE(IGOUT,10)TITLE
      460 J=LIST-1
      C
      LOOP THROUGH ATOMS
      DO 500 I=1,NATOM
      WRITE(IGOUT,12)TAG(K,1),K=1,2),(XYZ(I,J),J=1,3)
      C
      FIRST LOOP THROUGH LIST
      DO 500 J=1,IJ
      DO 460 K=1,3
      460 YP(K)=XPR(K,J)-XYZ(K,I)
      B=0.0
      XPR(M)=0.0
      470 XPR(N)=XPR(M)+G(K,N)*XPR(K)
      480 B=S*XPR(N)*XPR(N)
      490 S=1.0/BOXT(18)
      NAT=NOM(J)/64
      IE=J+1
      C
      SECOND LOOP THROUGH LIST
      DO 570 K=IE,LIST
      S2=0.0
      500 TP(M)=XPR(N,K)-XYZ(N,I)
      DO 520 N=1,3
      XZP=0.0
      510 XZP=XZP+TP(M)*G(M,N)
      520 S2=S2+XZP*TP(N)

```

```

      530 S2=S2/BOXT(S2)
      IF(NBODAN)170,570,570,570,530
      CTH=0.0
      540 CTH=CTH+XYP(M)*YP(M)
      DO 540 M=1,3
      CTH=CTH*S2
      TEMP=ABS(CTH)
      IF(TEMP-1.0)560,560,550
      550 CTH=CTH/TEMP
      560 CTH=10.0,09ACOS(CTH)/PI
      WRITE(IGOUT,14)TAG(M,NAT),M=1,2),J,(TAG(M,NAT),M=1,2),K,CTH
      570 CONTINUE
      580 RETURN
      END
      EODN1160
      EODN1170
      EODN1180
      EODN1190
      EODN1200
      EODN1210
      EODN1220
      EODN1230
      EODN1240
      EODN1250
      EODN1260
      EODN1270
      EODN1280
      EODN1290
      EODN1300
      EODN1310
      EODN1320
      EODN1330
      EODN1340
      EODN1350
      EODN1360
      EODN1370
      EODN1380
      EODN1390
      EODN1400
      EODN1410
      EODN1420
      EODN1430
      EODN1440
      EODN1450
      EODN1460
      EODN1470
      EODN1480
      EODN1490
      EODN1500
      EODN1510
      EODN1520
      EODN1530
      EODN1540
      EODN1550
      EODN1560
      EODN1570
      EODN1580
      EODN1590
      EODN1600
      EODN1610
      EODN1620
      EODN1630
      EODN1640
      EODN1650
      EODN1660
      EODN1670
      EODN1680
      EODN1690
      EODN1700
      EODN1710
      EODN1720
      EODN1730

```

[illegible]


```

9220 FORMAT(1X,5(I3,F10.4))
1*5
IF(1.LE.NDECN)GO TO 210
RETURN
END

PQGN 320
PQGN 330
PQGN 340
PQGN 350
PQGN 360

* ROUTINE TO ADJUST THE SIZE OF THE MEMORY FIELD OF AN ACTIVE PROGRAM
* CALLING SEQUENCE
* CALL CORSZ(ARRAY(N))
* ARRAY(N) MUST BE AT THE END OF THE 11' OR 10' BANK OF THE PROGRAM.
* N IS THE LARGEST INDEX REQUIRED BY THE PROGRAM.
*
$(( )
  AXS
  CORSZ* L AO-Q,X11 * GET FINAL ADDRESS
  TNE AO, LAST * SAME SIZE AS BEFORE?
  J 2,X11 * YES - RETURN,
  L AI, LAST
  S
  TG AO, AI * NEED MORE CORE?
  J 2,X11 * YES
  ER CORES * YES - REDUCE NEEDS.
  J 2,X11 * NO
  ER MCORES * GET MORE.
  J 2,X11
  LAST *0
  END

SUBROUTINE WEIGHT
C THIS ROUTINE REVISED AN-O/R RESEQUENCE ON HCT, 28, 1968
C
C DUMMY ROUTINE
ENTRY REJECT
DUMMY ROUTINE
RETURN
END

XPAR PRMC
  COM MON/XPAN/HPAR,ATGX(3,3),XTGAI(3,3),PARM(60),PARMAN(2,60),IPAR(60)
  1,IRPAR(60),GXZ(3),SKYZ(3),GXPI(3),T(3,3),EL(3,3),SA(3,3),TRNE(3,3)
  2 ,ITRNS(3,3),TRANS(3,3),ITRNS(3,3),RTEN(3,3),DTE-M(6),GTEN(10)
END
TAPE PRMC
END
LSWAT PRMC
  COM MON/LSWAT/M 200),TEXT,1TPAR(1000),MPANK,KCYCL,LAHEL(3),JSRE(10
  1),NESE,SIGMA,NOEN,M(200)
END
ACPN PRMC
  COM MON/A/RETA(6,60),GR(3,3),ISOT(60),NATOM,TAR(2,60),TITLE(18),XYZ(
  13,60),P,CR(10,60),OR(15,60)
END
DCON PRMC
  COM MON/O/ACALC,AIN(60),ANW(2,20),ICALC,RI NH(60),DADM(6,60),DADM(
  1 60),DAD(3,60),DRDH(6,60),DRDH(60),DRDH(3,60),IM(3),IM(3),ISCAT(2,
  2 60),ISCL,MSEL,DCAL(60),MCCUP(60),SCALE(10),SCAT(20),SITE(60)
  3,DAD(10,60),DRUC(10,60),DADM(15,60),DRDH(15,60),AMINUS,HA1NUS
  4,DRDE(6),NOEN
  DIMENSION SAVE(60),KDEGN(2640),AA(2640)
  EQUIVALENCE (SAVE,AIND),(KDEGN,AA,OADC(1,37))
END
INDE3 PRMC
  COM MON/INDE3/INDE(2,6),IND(3,10)
END

```

93

D6	300	J=I,I	STWV1160
EE	KK-I		STWV1170
L=	L'KE		STWV1180
C	L INDEXES A(I,J)		STWV1190
3D0	Q=Q+AL*PBK J,K		STWV1200
IF	(I-NEAKN)310,330,330		BYWV121D
31D	KJ=I+I		STWV1220
D6	320 J=KJ,NEAKN		STWV1230
L=	L'I		STWV1240
C	L INDEXES A(J,I)		STWV1250
320	Q=Q+AL*PBK J,K		STWV1260
330	STWV1270		STWV1270
D6	340 J=L,NEAKN		STWV1280
34D	KJ J,I=SCR J,J		STWV1290
350	CONTINUE		STWV1300
C	SBT NON-SINGULAR FLAG AND EXIT		STWV1310
360	JEANE-NEAKN		STWV1320
RETURN			STWV1330
END			STWV1340
1	READ(5,I NAME	BNDN 10	
I	FORMAT(12)	BNDN 2D	
IF	(NAMB-2)3,4,S	BNDN 30	
3	CALL BADTBA'	BNDN 40	
GO	TO 6	BNDN 50	
4	CALL SER	BNDN 6D	
5	WRITE(6,2 NAME	BNDN 7D	
6	FORMAT(12) 2 NAME	BNDN 8D	
2	FORMAT(12) 2 NAME	BNDN 90	
STEP		BNDN 100	
6	BND	BNDN 110	

[illegible]

```

210 FORMATT(12XAL,7X10P10.5)
211 FORMATT(20X10P10.5)

      FPH(3)=1./3.
      FPH(4)=2./3.
      FPH(7)=1./6.
      FPH(8)=5./6.
      PI=ACOS(-1.0)
      WAVELENGTH=1.0
      WAVELENGTH=1.0
      READ(IN,3)A,ANG
      C CALCULATE SINES AND COSINES OF DIRECT SPACE ANGLES
      D6 4 I=1,3
      IF(ABS(ANG(I)-90.0).GT.1.0E-3)G6 TO 1000
      SI(I)=1.0
      ANG(I)=90.0
      G6 TO 4
      ANG(I)=90./180.0
      SI(I)=SIN(ANG(I))
      COS(I)=COS(ANG(I))
      C MATRIX G IS THE REAL SPACE METRIC TENS9R
      4 G(1,1)=A(I)*2
      D6 144 I=1,2
      IJ=I+1
      D6 144 J=I+3
      IF(I=1-J)G(1,I)=A(I)*ANG(IK)
      144 G(I,J)=G(I,J)
      C COMPUTE REAL SPACE CELL VOLUME
      V6L=A(1)*A(2)*A(3)*SQRT(1.0-ANG(1)*2-ANG(2)*2-ANG(3)*2)
      C COMPUTE RECIPROCAL SPACE CELL PARAMETERS
      ASK(1)=A(2)*A(3)*SK(1)/V6L
      ASK(2)=A(1)*A(3)*SK(2)/V6L
      ASK(3)=A(1)*A(2)*SK(3)/V6L
      CSK(1)=(ANG(1)*ANG(2)*ANG(3))/(S(2)*S(3))
      CSK(2)=(ANG(1)*ANG(3)*ANG(2))/(S(1)*S(3))
      CSK(3)=(ANG(1)*ANG(2)*ANG(3))/(S(1)*S(2))
      WRITE(10UT,57)MCELL,A,ANG,ASK,CS,V6L
      C READ CONTROL CARD
      READ(IN,5)NA,ICNT,IMWD,LELV,IERF,LTYPE,DLIMIT
      IF(DLIMIT(3).LE.0.0)DLIMIT(3)=DLIMIT(2)
      I2=ICNT
      WRITE(10UT,58)TYPE,ACELL(1,1)
      C READ SYMMETRY CARDS
      D6 7 I=1,48
      READ(IN,6)M(IT(K)),(IP6S(L,K),L=1,2),K=1,3,IEF
      WRITE(10UT,9)M(IT(K)),(IP6S(L,K),L=1,2),K=1,3
      C CLEAR ROTATIONAL MATRICES
      D6 12 J=1,3
      D6 10 K=1,3
      10 RSK(K,J)=0
      C TRANSLATIONAL OPERATOR
      D6 11 K=1,8
      IF(IT(J)=1)R(K,1)=13,11
      11 CONTINUE
      C CARD CHARACTERS ARE NOT IN THE ACCEPTABLE LIST
      STOP 11

```

```

C SBT TRANSLATIONAL VALUE
13 TS(J,1)=PPB(K)
D6 14 K=1,3
D6 14 L=1,2
C COMPARE POSITIONAL INFORMATION WITH ACCEPTABLE VALUES
D6 15 N=1,10
IF(IP6S(N)-IP6S(L,K))15,16,15
C CONTINUE
15 CONTINUE
16 IF(PPB(K)-PPB(L))16,17,14
STOP 11
C STORE ROTATIONAL MATRIX ELEMENT
17 RS(K,J)=ISIGN(1,IP6S(N))
14 CONTINUE
12 CONTINUE
C CHECK IF THIS IS THE LAST SYMMETRY CARD
12 CONTINUE
16 IF(IEF)16,17,18
7 CONTINUE
C TOO MANY SYMMETRY CARDS
STOP 22
18 NSS=1
IF(ICNT)38,39,38
C EXPAND LIST FOR CENTRIC SPACE GROUP
39 D6 40 I=1,NSS
N=1+NSS
TS(J,1)=TS(J,1)
D6 40 K=1,3
40 RS(K,J,N)=2S(K,J,1)
NSS=2*NSS
C FORM MATRICES FOR LATTICE POINTS
38 NLP=1
D6 19 I=1,3
19 TP(I,1)=0
IF(LTYPE=PI)21,20,21
C IF LTYPE=PI IS NOT PRIMITIVE
21 D6 22 I=1,3
22 TP(2,I)=0.5
NLP=2
IF(LTYPE=1A1)23,24,23
C A CENTERED LATTICE
24 TP(2,1)=0
D6 TO 20
23 IF(LTYPE=1A1)25,26,25
25 IF(LTYPE=1A1)27,28
26 TP(2,2)=0
D6 TO 20
25 IF(LTYPE=1C1)28,27,28
27 TP(2,3)=0
C CENTERED LATTICE
D6 TO 20
28 IF(LTYPE=1I1)29,20,29
29 IF(LTYPE=1I1)30,31
30 NLP=4
D6 32 I=2,4
D6 33 J=1,3
33 TP(1,J)=0.5

```

```

BADI 580
BADI 590
BADI 600
BADI 610
BADI 620
BADI 630
BADI 640
BADI 650
BADI 660
BADI 670
BADI 680
BADI 690
BADI 700
BADI 710
BADI 720
BADI 730
BADI 740
BADI 750
BADI 760
BADI 770
BADI 780
BADI 790
BADI 800
BADI 810
BADI 820
BADI 830
BADI 840
BADI 850
BADI 860
BADI 870
BADI 880
BADI 890
BADI 900
BADI 910
BADI 920
BADI 930
BADI 940
BADI 950
BADI 960
BADI 970
BADI 980
BADI 990
BADI 1000
BADI 1010
BADI 1020
BADI 1030
BADI 1040
BADI 1050
BADI 1060
BADI 1070
BADI 1080
BADI 1090
BADI 1100
BADI 1110
BADI 1120
BADI 1130
BADI 1140
BADI 1150

```

```

32 TP(I,I-1)*0
   GO TO 20
C
31 TM(2,1)*TM(2,1)
   TP(3,2)*TM(2,1)
   TP(3,3)*TM(2,1)
   NLP=3
   TM(2,2)*2./3.
   TP(3,1)*TM(2,2)
20 IF IERR.EQ.0 GO TO 101
   READ(10,50)SIG(J),J=1,J1
C
100 READ(10,50)SIG(J),J=1,J1
   WRITE(10,207)SIG(J),J=1,J1
   WRITE(10,208)
   L=0.
   GO 223 I=1,NA
   DO 223 J=1,3
   IJ=3*(I-1)+J
   SIG(IJ)=SIG(IJ)+SIG(IJ)*E-1,IJ)
   IF(J.NE.1,02,I=GT,4)GO TO 215
   IF(J.NE.1,02,I=GT,4)GO TO 215
   GO TO 216
215 IF(J.NE.1)GO TO 21E
   WRITE(10,209)MATOM(K,I),K=1,2,(SIG(IJ)*E-1,I)
   GO TO 221
21E IF(I,02,4)GO TO 220
   GO TO 221
220 WRITE(10,210)JFGB(J),(SIG(IJ)*E-1,I)
   GO TO 216
221 WRITE(10,211)SIG(IJ),K=1,IJ)
C
216 DO 222 K=1,IJ
   SIG(IJ)=SIG(IJ)*SIG(IJ)*E-2
   DO 223 K=1,IJ
   SIG(IJ)=SIG(IJ)
223 COR(I,I)=SIG(IJ)
C
105 IF(IERR.EQ.0)GO TO 44
   COMPUTE RMS DISTANCE AND ANGLE
43 CALL E90AN(E90)
44 IF(1BLV)45,46,45
C
45 CALL ELVIE
   COMPUTE THERMAL ELLIPSOIDS
C
46 CALL ELIT
   END OF CALCULATION, TERMINATE PROGRAM
   END

```

```

EADT1740
EADT1750
EADT1760
EADT1770
EADT1780
EADT1790
EADT1800
EADT1810
EADT1820
EADT1830
EADT1840
EADT1850
EADT1860
EADT1870
EADT1880
EADT1890
EADT1900
EADT1910
EADT1920
EADT1930
EADT1940
EADT1950
EADT1960
EADT1970
EADT1980
EADT1990
EADT2000
EADT2010
EADT2020
EADT2030
EADT2040
EADT2050
EADT2060
EADT2070
EADT2080
EADT2090
EADT2100
EADT2110
EADT2120
EADT2130
EADT2140
EADT2150
EADT2160
EADT2170
EADT2180
EADT2190
EADT2200
EADT2210
EADT2220
EADT2230
EADT2240
EADT2250
EADT2260
EADT2270
EADT2280
EADT2290
EADT2300
EADT2310

```



```

D6 D6 N=1,3
76 OLDE(K*3)=DLDE(K*3)-XZP(N)*BSIN(K,L)
C FILL IN SELF VARIANCE-COVARIANCE MATRIX
I3=3*(IATP(J)/64)-2
J1=((I3+1)*I3)/2
D6 D7 I=1,3
D6 D8 I=1,3
SIG(K*3,4)=CORR(L)
I4=60,106 TO 77
D6 D7 N=2,K
L=1
76 SIG(K*3,N*3)=CORR(L)
77 J1=I1+K-1
C GET CROSS TERMS FOR VARIANCE-COVARIANCE MATRIX
C CALL COMPTC(1,3,4,1,4,NA)
C COMPUTE VARIANCE-COVARIANCE WITHIN LIMITS
C CALL VARIAN(DS,DLDA,DLDA,EIGX,EIGY,1)
DS=DS/5
I3=IATP(J)/64
I4=IATP(J)/64
WRITE(1007,9005)NATOM(K*3),K*1,2),(KZPM(K*3),K*3),S,DS,J
D6 TO 71
1001 I3=IATP(J)/64
WRITE(1007,1002)NATOM(K*3),K*1,2),(KZPM(K*3),K*3),E,J
71 CONTINUE
C
C LOOP THROUGH THE ASYMMETRIC UNIT TO GENERATE ATOMS
D6 I JJ=1,NA
C LOOP THROUGH THE SYMMETRY OPERATIONS
D6 J1=1,NSS
C GENERATE TRANFORMED POSITION
XPL)=TS(L,J)
D6 I3 M=1,3
13 KP(L)=KPL)+SK(L,M,J)*XZM(M,J)
D6 D2 M=1,NLP
C LOOP THROUGH LATTICE POINTS
D6 D4 L=1,3
14 KP(L)=KPL)+TP(L,M,L)
D6 D3 I=1,3
NXX(I+3)-3,0-DX(I)-KXP(I)
63 NXX(I+3)-3,0-DX(I)-KXP(I)
NEU=NEK(4)
NTU=NTX(5)
D6 D2 NXX(6)
D6 D2 IA=NXL,NEU
KPL)=KPL)+PLAT(1A-3)
KPL)=KPL)+PLAT(1B-3)
D6 D2 IC=NXL,NEU
KPL)=KPL)+PLAT(1C-3)
C CHECK FOR ATOM DUPLICATION
D6 I13 I=1,NATOM
I4=IATP(I)/64,BG,JJ TO 24
D6 TO 113
24 D6 D4 L=1,3

```

```

IPABS (KTP(L)-KZP(L,I))=0.00002)*N,11,4,11,3
114 CONTINUE
C THROUGH HERE IF THE ATOM HAS ALREADY BEEN GENERATED
D6 TO 12
113 CONTINUE
C COMPUTE DISTANCE
D6 D5 K=1,3
15 YP(K)=XZM(K,I1)-KTP(K)
D6 D7 N=1,3
XZP(N)=0
D6 D6 K=1,3
16 XZP(N)=XZP(N)+YP(K)*K(N)
17 5=XZP(N)*TP(N)
C CALCULATE DISTANCE WITHIN LIMITS
IP((I1+K-8)*I1)/2,12,16
D6 D5 K=1,3
18 DISTANCE=6E, CHECK IF D6M IN GENERATED LIST
19 IF(NATOM-1000)19,20,20
C ABRUPTLY OVERFLOWING, PRINT MESSAGE AND TERMINATE
20 WRITE(1007,9999)
RETURN
C ADD GENERATED ATOM TO LIST AND COMPUTE DERIVATIVES
19 NATOM=NATOM+1
KPL)=KPL)+K*64+J
DLDA(5,1)=D6M(1)*TP(2)+YP(3)
DLDA(5,1)=D6M(2)*TP(1)+YP(3)
DLDA(6,1)=D6M(3)*TP(1)+YP(2)
D6 D2 K=1,3
XZP(K,NATOM)=XTP(K)
DLDE(K*3)=XZP(K)
DLDE(K*3)=0
DLDA(5,1)=XTP(K)*XZP(K)/A(K)
D6 D4 K=1,3
21 DLDE(K*3)=DLDE(K*3)-XZP(N)*BSIN(K*3,J)
1J=3*J-2
IF(108E,EQ,0)D6 TO 1004
1003 J1=((I1+1)*I1)/2
D6 D2 K=1,3
L=J1
KICK(K*3,4)=CORR(L)
I4=60,106 TO 23
D6 D2 N=2,K
L=1
22 KICK(K*3,N*3)=CORR(L)
23 J1=J1+K-1
C GENERATE CROSS MATRIX ELEMENTS
CALL CORRI(GIG,6,I1,JJ,CORR,1,4,NA)
S=SQRT(E)
CALL ARIAN(D6,DLDE,DLDA,EIGX,EIGY,1)
WRITE(1007,9005)NATOM(N,JJ),N=1,2),XTP,8,DS,NATOM
D6 TO 12
1004 G=SQRT(E)
C PRINT DISTANCE FOR NO ERROR CALCULATED
WRITE(1007,1002)NATOM(N,JJ),N=1,2),XTP,8,NATOM
12 CONTINUE
1 CONTINUE
C END OF BOND DISTANCE CALCULATION, RETURN IF NO ANGLES

```


132

104

```

K*E*1
IF(L,LE,6) GO TO 27
1021 DO 30 K*1,3
    THETA(K)=QI(K)/(A(E)*OMAG)
    IF(ABS(THETA(K))-1.0)32,32,31
    31 THETA(K)=SIGN(1.0,THETA(K))
    IF(ABS(THETA(K))-1.0)33,33,32
    32 THETA(K)=180.0+ABS(THETA(K))/PI
    33 THETA(K)=180.0+ABS(THETA(K))/PI
1024 DO 33 K*1,3
    IF(1882.80,0.100 TO 1023
    DO 34 K*1,6
C      THETA IS THE ANGLE WITH THE I TO REAL AXIS
    DTHED(J,K)=DODR(J,K)/(A(E)*OMAG)-QI(K)*DRODR(J)/(A(E)*QMAO*0.2)
    34 DTHED(J,K)=DODA(J,K)/(A(E)*OMAG)-QI(K)*DRODR(J)/(A(E)*QMAO*0.2)
    DTHED(J,K)=DTHED(J,K)-QI(K)/(A(E)*0.2*QMAO)
    IF(ABS(ETH(K))-1.0E-3)150,150,151
    151 DTHED(J,K)=DTHED(J,K)/ETH(K)
    DTHED(J,K)=DTHED(J,K)/ETH(K)
    GO TO 33
    150 DTHED(J,K)=0.
    DTHED(J,K)=0.
    33 CONTINUE
    COL=ABS(AN(ETH(K),DTHED(1,K),DTHED(1,K),BIGA,BIGB,II))
    35 ETH(K)=ETH(K)*180.0/PI
    36 WRITE(10DT,9005 M IAXIS(K),THETA(K),ETH(K),K*1,3)
    GO TO 19
1023 WRITE(10DT,1025 M IAXIS(K),THETA(K),K*1,3)
    19 CONTINUE
    2 CONTINUE
    RETURN
    END

```

```

ELVR2320
ELVR2330
ELVR2340
ELVR2350
ELVR2360
ELVR2370
ELVR2380
ELVR2390
ELVR2400
ELVR2410
ELVR2420
ELVR2430
ELVR2440
ELVR2450
ELVR2460
ELVR2470
ELVR2480
ELVR2490
ELVR2500
ELVR2510
ELVR2520
ELVR2530
ELVR2540
ELVR2550
ELVR2560
ELVR2570
ELVR2580
ELVR2590
ELVR2600
ELVR2610
ELVR2620
ELVR2630
ELVR2640
ELVR2650
ELVR2660
ELVR2670
ELVR2680
ELVR2690
ELVR2700
ELVR2710
ELVR2720
ELVR2730
ELVR2740
ELVR2750
ELVR2760
ELVR2770
ELVR2780
ELVR2790
ELVR2800
ELVR2810
ELVR2820
ELVR2830
ELVR2840
ELVR2850
ELVR2860
ELVR2870
ELVR2880
ELVR2890
ELVR2900
ELVR2910
ELVR2920
ELVR2930
ELVR2940
ELVR2950
ELVR2960
ELVR2970
ELVR2980
ELVR2990
ELVR3000
ELVR3010
ELVR3020
ELVR3030
ELVR3040
ELVR3050
ELVR3060
ELVR3070
ELVR3080
ELVR3090
ELVR3100
ELVR3110
ELVR3120
ELVR3130
ELVR3140
ELVR3150
ELVR3160
ELVR3170
ELVR3180
ELVR3190
ELVR3200
ELVR3210
ELVR3220
ELVR3230
ELVR3240
ELVR3250
ELVR3260
ELVR3270
ELVR3280
ELVR3290
ELVR3300
ELVR3310
ELVR3320
ELVR3330
ELVR3340
ELVR3350
ELVR3360
ELVR3370
ELVR3380
ELVR3390
ELVR3400
ELVR3410
ELVR3420
ELVR3430
ELVR3440
ELVR3450
ELVR3460
ELVR3470
ELVR3480
ELVR3490
ELVR3500
ELVR3510
ELVR3520
ELVR3530
ELVR3540
ELVR3550
ELVR3560
ELVR3570
ELVR3580
ELVR3590
ELVR3600
ELVR3610
ELVR3620
ELVR3630
ELVR3640
ELVR3650
ELVR3660
ELVR3670
ELVR3680
ELVR3690
ELVR3700
ELVR3710
ELVR3720
ELVR3730
ELVR3740
ELVR3750
ELVR3760
ELVR3770
ELVR3780
ELVR3790
ELVR3800
ELVR3810
ELVR3820
ELVR3830
ELVR3840
ELVR3850
ELVR3860
ELVR3870
ELVR3880
ELVR3890
ELVR3900
ELVR3910
ELVR3920
ELVR3930
ELVR3940
ELVR3950
ELVR3960
ELVR3970
ELVR3980
ELVR3990
ELVR4000
ELVR4010
ELVR4020
ELVR4030
ELVR4040
ELVR4050
ELVR4060
ELVR4070
ELVR4080
ELVR4090
ELVR4100
ELVR4110
ELVR4120
ELVR4130
ELVR4140
ELVR4150
ELVR4160
ELVR4170
ELVR4180
ELVR4190
ELVR4200
ELVR4210
ELVR4220
ELVR4230
ELVR4240
ELVR4250
ELVR4260
ELVR4270
ELVR4280
ELVR4290
ELVR4300
ELVR4310
ELVR4320
ELVR4330
ELVR4340
ELVR4350
ELVR4360
ELVR4370
ELVR4380
ELVR4390
ELVR4400
ELVR4410
ELVR4420
ELVR4430
ELVR4440
ELVR4450
ELVR4460
ELVR4470
ELVR4480
ELVR4490
ELVR4500
ELVR4510
ELVR4520
ELVR4530
ELVR4540
ELVR4550
ELVR4560
ELVR4570
ELVR4580
ELVR4590
ELVR4600
ELVR4610
ELVR4620
ELVR4630
ELVR4640
ELVR4650
ELVR4660
ELVR4670
ELVR4680
ELVR4690
ELVR4700
ELVR4710
ELVR4720
ELVR4730
ELVR4740
ELVR4750
ELVR4760
ELVR4770
ELVR4780
ELVR4790
ELVR4800
ELVR4810
ELVR4820
ELVR4830
ELVR4840
ELVR4850
ELVR4860
ELVR4870
ELVR4880
ELVR4890
ELVR4900
ELVR4910
ELVR4920
ELVR4930
ELVR4940
ELVR4950
ELVR4960
ELVR4970
ELVR4980
ELVR4990
ELVR5000
ELVR5010
ELVR5020
ELVR5030
ELVR5040
ELVR5050
ELVR5060
ELVR5070
ELVR5080
ELVR5090
ELVR5100
ELVR5110
ELVR5120
ELVR5130
ELVR5140
ELVR5150
ELVR5160
ELVR5170
ELVR5180
ELVR5190
ELVR5200
ELVR5210
ELVR5220
ELVR5230
ELVR5240
ELVR5250
ELVR5260
ELVR5270
ELVR5280
ELVR5290
ELVR5300
ELVR5310
ELVR5320
ELVR5330
ELVR5340
ELVR5350
ELVR5360
ELVR5370
ELVR5380
ELVR5390
ELVR5400
ELVR5410
ELVR5420
ELVR5430
ELVR5440
ELVR5450
ELVR5460
ELVR5470
ELVR5480
ELVR5490
ELVR5500
ELVR5510
ELVR5520
ELVR5530
ELVR5540
ELVR5550
ELVR5560
ELVR5570
ELVR5580
ELVR5590
ELVR5600
ELVR5610
ELVR5620
ELVR5630
ELVR5640
ELVR5650
ELVR5660
ELVR5670
ELVR5680
ELVR5690
ELVR5700
ELVR5710
ELVR5720
ELVR5730
ELVR5740
ELVR5750
ELVR5760
ELVR5770
ELVR5780
ELVR5790
ELVR5800
ELVR5810
ELVR5820
ELVR5830
ELVR5840
ELVR5850
ELVR5860
ELVR5870
ELVR5880
ELVR5890
ELVR5900
ELVR5910
ELVR5920
ELVR5930
ELVR5940
ELVR5950
ELVR5960
ELVR5970
ELVR5980
ELVR5990
ELVR6000
ELVR6010
ELVR6020
ELVR6030
ELVR6040
ELVR6050
ELVR6060
ELVR6070
ELVR6080
ELVR6090
ELVR6100
ELVR6110
ELVR6120
ELVR6130
ELVR6140
ELVR6150
ELVR6160
ELVR6170
ELVR6180
ELVR6190
ELVR6200
ELVR6210
ELVR6220
ELVR6230
ELVR6240
ELVR6250
ELVR6260
ELVR6270
ELVR6280
ELVR6290
ELVR6300
ELVR6310
ELVR6320
ELVR6330
ELVR6340
ELVR6350
ELVR6360
ELVR6370
ELVR6380
ELVR6390
ELVR6400
ELVR6410
ELVR6420
ELVR6430
ELVR6440
ELVR6450
ELVR6460
ELVR6470
ELVR6480
ELVR6490
ELVR6500
ELVR6510
ELVR6520
ELVR6530
ELVR6540
ELVR6550
ELVR6560
ELVR6570
ELVR6580
ELVR6590
ELVR6600
ELVR6610
ELVR6620
ELVR6630
ELVR6640
ELVR6650
ELVR6660
ELVR6670
ELVR6680
ELVR6690
ELVR6700
ELVR6710
ELVR6720
ELVR6730
ELVR6740
ELVR6750
ELVR6760
ELVR6770
ELVR6780
ELVR6790
ELVR6800
ELVR6810
ELVR6820
ELVR6830
ELVR6840
ELVR6850
ELVR6860
ELVR6870
ELVR6880
ELVR6890
ELVR6900
ELVR6910
ELVR6920
ELVR6930
ELVR6940
ELVR6950
ELVR6960
ELVR6970
ELVR6980
ELVR6990
ELVR7000
ELVR7010
ELVR7020
ELVR7030
ELVR7040
ELVR7050
ELVR7060
ELVR7070
ELVR7080
ELVR7090
ELVR7100
ELVR7110
ELVR7120
ELVR7130
ELVR7140
ELVR7150
ELVR7160
ELVR7170
ELVR7180
ELVR7190
ELVR7200
ELVR7210
ELVR7220
ELVR7230
ELVR7240
ELVR7250
ELVR7260
ELVR7270
ELVR7280
ELVR7290
ELVR7300
ELVR7310
ELVR7320
ELVR7330
ELVR7340
ELVR7350
ELVR7360
ELVR7370
ELVR7380
ELVR7390
ELVR7400
ELVR7410
ELVR7420
ELVR7430
ELVR7440
ELVR7450
ELVR7460
ELVR7470
ELVR7480
ELVR7490
ELVR7500
ELVR7510
ELVR7520
ELVR7530
ELVR7540
ELVR7550
ELVR7560
ELVR7570
ELVR7580
ELVR7590
ELVR7600
ELVR7610
ELVR7620
ELVR7630
ELVR7640
ELVR7650
ELVR7660
ELVR7670
ELVR7680
ELVR7690
ELVR7700
ELVR7710
ELVR7720
ELVR7730
ELVR7740
ELVR7750
ELVR7760
ELVR7770
ELVR7780
ELVR7790
ELVR7800
ELVR7810
ELVR7820
ELVR7830
ELVR7840
ELVR7850
ELVR7860
ELVR7870
ELVR7880
ELVR7890
ELVR7900
ELVR7910
ELVR7920
ELVR7930
ELVR7940
ELVR7950
ELVR7960
ELVR7970
ELVR7980
ELVR7990
ELVR8000
ELVR8010
ELVR8020
ELVR8030
ELVR8040
ELVR8050
ELVR8060
ELVR8070
ELVR8080
ELVR8090
ELVR8100
ELVR8110
ELVR8120
ELVR8130
ELVR8140
ELVR8150
ELVR8160
ELVR8170
ELVR8180
ELVR8190
ELVR8200
ELVR8210
ELVR8220
ELVR8230
ELVR8240
ELVR8250
ELVR8260
ELVR8270
ELVR8280
ELVR8290
ELVR8300
ELVR8310
ELVR8320
ELVR8330
ELVR8340
ELVR8350
ELVR8360
ELVR8370
ELVR8380
ELVR8390
ELVR8400
ELVR8410
ELVR8420
ELVR8430
ELVR8440
ELVR8450
ELVR8460
ELVR8470
ELVR8480
ELVR8490
ELVR8500
ELVR8510
ELVR8520
ELVR8530
ELVR8540
ELVR8550
ELVR8560
ELVR8570
ELVR8580
ELVR8590
ELVR8600
ELVR8610
ELVR8620
ELVR8630
ELVR8640
ELVR8650
ELVR8660
ELVR8670
ELVR8680
ELVR8690
ELVR8700
ELVR8710
ELVR8720
ELVR8730
ELVR8740
ELVR8750
ELVR8760
ELVR8770
ELVR8780
ELVR8790
ELVR8800
ELVR8810
ELVR8820
ELVR8830
ELVR8840
ELVR8850
ELVR8860
ELVR8870
ELVR8880
ELVR8890
ELVR8900
ELVR8910
ELVR8920
ELVR8930
ELVR8940
ELVR8950
ELVR8960
ELVR8970
ELVR8980
ELVR8990
ELVR9000
ELVR9010
ELVR9020
ELVR9030
ELVR9040
ELVR9050
ELVR9060
ELVR9070
ELVR9080
ELVR9090
ELVR9100
ELVR9110
ELVR9120
ELVR9130
ELVR9140
ELVR9150
ELVR9160
ELVR9170
ELVR9180
ELVR9190
ELVR9200
ELVR9210
ELVR9220
ELVR9230
ELVR9240
ELVR9250
ELVR9260
ELVR9270
ELVR9280
ELVR9290
ELVR9300
ELVR9310
ELVR9320
ELVR9330
ELVR9340
ELVR9350
ELVR9360
ELVR9370
ELVR9380
ELVR9390
ELVR9400
ELVR9410
ELVR9420
ELVR9430
ELVR9440
ELVR9450
ELVR9460
ELVR9470
ELVR9480
ELVR9490
ELVR9500
ELVR9510
ELVR9520
ELVR9530
ELVR9540
ELVR9550
ELVR9560
ELVR9570
ELVR9580
ELVR9590
ELVR9600
ELVR9610
ELVR9620
ELVR9630
ELVR9640
ELVR9650
ELVR9660
ELVR9670
ELVR9680
ELVR9690
ELVR9700
ELVR9710
ELVR9720
ELVR9730
ELVR9740
ELVR9750
ELVR9760
ELVR9770
ELVR9780
ELVR9790
ELVR9800
ELVR9810
ELVR9820
ELVR9830
ELVR9840
ELVR9850
ELVR9860
ELVR9870
ELVR9880
ELVR9890
ELVR9900
ELVR9910
ELVR9920
ELVR9930
ELVR9940
ELVR9950
ELVR9960
ELVR9970
ELVR9980
ELVR9990

```



```

1000 LCHR 590
      IF (IDRM.EQ.6)J1=2
      IF (IDRM.EQ.4)J1=2
      EL(J,J).E=PAR(J)
      EL(K,J).E=PAR(J)
129  IL=IL+1
      L=IL+J
130 CONTINUE
      DO 140 J=1,N
      C CONTAINS A LIST OF TDB PARAMETERS WHICH ARE MEMBERS OF THE L
      C TENSOR IN THIS SET.
      DO 1000 I=1,NA
      DO 140 J=1,IL
      JJ=L(J)
      DO 140 K=1,MDBON,2
      IF (I*(NSTRK(E)).NE.0.OR.I2*(NSTRK(E)).GT.(L(I)))/GO TO 1000
      IF (I*(NSTRK(E)).EQ.JJ.AND.I2*(NSTRK(E)).EQ.I)/GO TO 150
140 CONTINUE
      NG MATCH FOUND FOR THIS ATOM
      GO TO 1000
      C ATOM I DEPENDS ON THE CURRENT SET, APPLY LIBRATION CORRECTION.
      DO 160 J=1,3
      160 STZ(J)=XYZ(J,1)-GXZ(J)
      CALL UTMUL(XTGA,R,3,RC)
      CALL UTMUL(XTGA,R,3,XYZ)
      DO 170 J=1,3
      170 XYZ(J,1)=XYZ(J)-GXZ(J)
1000 CONTINUE
      IET=L(IL)+1
      IF (IST.GT.NFAR)RETURN
      GO TO 50
      END

```

[illegible]

110


```

00 L20 J=1, IZA
K=NUM*(J-1)+IVA+1
DO 100 I=1, IZA
KK=K+I-1
DO 110 M=K, KK
110 LINE=(M-K+1)=BUFF(M)+SIGNL*.5+BUFF(M)
II=J+IZI-1
120 M=(TEI(OUT, I, 4)FMAT(1SPC), I, (LINE(M), M=1, I)
IF (I=EO.O) GO TO 15
K=NUM+1
L=1000
MK(TEI(SCI), IVA, IZA, IZO, L, IX, IXI, IXF, IV, IZI, IZF
*TEI(SCI), BUFF(M), M=K, NUMZ)
GO TO 15
900 STOP
END

```



```

IF (INITIAL1165-120,120
146 CALL PLOTIO(0,0,0,999)
STOP
C
157 FORMAT(20A4,F5.0,15,F5.0-615,F5.0-215)
158 FORMAT(40A4,F10.4,F10.4,10H EGES OF -2F7.2, 20H 1NS. WITH ANGLE OF +F
17.2, 9H DEGREES -/X121, 21H POINTS PER EDGE AND ,12, 32H INTERPONT1800
ZLATION POINTS PER SPLINE)
160 FORMAT (11H0, 22H NO CONTOURS SPECIFIED)
162 FORMAT (315,0)
164 FORMAT (11H015,14H CONTOUR TYPES,/(1X,3F8.2,141)
165 FORMAT (11H015, 9H VERTICES,/(1X51-3F8.2,211)
166 FORMAT (11H015, 24H CROSSES WITH ARM LENGTH,F6.2, 5H INS.,/(1X51-4X
12F8.2,211)
167 FORMAT (11H0, 42H NO SECTION SELECTIONS. -- JOB ABAOONOED.)
168 FORMAT (11H015, 44H SECTION SELECTIONS GIVEN IN INTERVALS OF 1/,14
11X, 5FH0RM (1,14, 13H IN STEPS OF 14, 44H TO ,141)
169 FORMAT (11H0, 33H C OF READ WHILE SEARCHING FOR ,215)
170 FORMAT (11H0, 33H C OF READ WHILE SEARCHING FOR ,215)
171 FORMAT (11H015, 17H PLOT OF SECTION 1,15, 15,9H SELECTED)
172 FORMAT (11X, 41H SELECTED AND READ SECTION NUMBERS 01FFR, /1X21,
17H READ, +21, 9H SELECTED)
173 FORMAT (11H0, 58H SELECTED AND READ SECTION SIZES 01FFR, -- JOB
1BANOOED, /1X21, 12H SIZE READ, +21, 14H SIZE SELECTED)
174 FORMAT (11H0, 17H PLOT OF SECTION 1,14,14,14, 6H BEGUN)
176 FORMAT (11H0, 25H NO MAP DENSITY IN RANGE ,2F10.2, 20H AVAILABLE
1NGE IS ,2F10.2)
177 FORMAT (11H0, 50H NO CONTOURS FOR THIS SECTION. -- NOTHING PLOTTE
178 FORMAT(15F5.0-0.46)
FNO
C
CNTP1760
CNTP1750
CNTP1740
CNTP1730
CNTP1720
CNTP1710
CNTP1700
CNTP1690
CNTP1680
CNTP1670
CNTP1660
CNTP1650
CNTP1640
CNTP1630
CNTP1620
CNTP1610
CNTP1600
CNTP1590
CNTP1580
CNTP1570
CNTP1560
CNTP1550
CNTP1540
CNTP1530
CNTP1520
CNTP1510
CNTP1500
CNTP1490
CNTP1480
CNTP1470
CNTP1460
CNTP1450
CNTP1440
CNTP1430
CNTP1420
CNTP1410
CNTP1400
CNTP1390
CNTP1380
CNTP1370
CNTP1360
CNTP1350
CNTP1340
CNTP1330
CNTP1320
CNTP1310
CNTP1300
CNTP1290
CNTP1280
CNTP1270
CNTP1260
CNTP1250
CNTP1240
CNTP1230
CNTP1220
CNTP1210
CNTP1200
CNTP1190
CNTP1180
CNTP1170
CNTP1160
CNTP1150
CNTP1140
CNTP1130
CNTP1120
CNTP1110
CNTP1100
CNTP1090
CNTP1080
CNTP1070
CNTP1060
CNTP1050
CNTP1040
CNTP1030
CNTP1020
CNTP1010
CNTP1000
CNTP990
CNTP980
CNTP970
CNTP960
CNTP950
CNTP940
CNTP930
CNTP920
CNTP910
CNTP900
CNTP890
CNTP880
CNTP870
CNTP860
CNTP850
CNTP840
CNTP830
CNTP820
CNTP810
CNTP800
CNTP790
CNTP780
CNTP770
CNTP760
CNTP750
CNTP740
CNTP730
CNTP720
CNTP710
CNTP700
CNTP690
CNTP680
CNTP670
CNTP660
CNTP650
CNTP640
CNTP630
CNTP620
CNTP610
CNTP600
CNTP590
CNTP580
CNTP570
CNTP560
CNTP550
CNTP540
CNTP530
CNTP520
CNTP510
CNTP500
CNTP490
CNTP480
CNTP470
CNTP460
CNTP450
CNTP440
CNTP430
CNTP420
CNTP410
CNTP400
CNTP390
CNTP380
CNTP370
CNTP360
CNTP350
CNTP340
CNTP330
CNTP320
CNTP310
CNTP300
CNTP290
CNTP280
CNTP270
CNTP260
CNTP250
CNTP240
CNTP230
CNTP220
CNTP210
CNTP200
CNTP190
CNTP180
CNTP170
CNTP160
CNTP150
CNTP140
CNTP130
CNTP120
CNTP110
CNTP100
CNTP90
CNTP80
CNTP70
CNTP60
CNTP50
CNTP40
CNTP30
CNTP20
CNTP10
CNTP00

```

[illegible]

```

CPLT 580
CPLT 590
CPLT 600
CPLT 610
CPLT 620
CPLT 630
CPLT 640
CPLT 650
CPLT 660
CPLT 670
CPLT 680
CPLT 690
CPLT 700
CPLT 710
CPLT 720
CPLT 730
CPLT 740
CPLT 750
CPLT 760
CPLT 770
CPLT 780
CPLT 790
CPLT 800
CPLT 810
CPLT 820
CPLT 830
CPLT 840
CPLT 850
CPLT 860
CPLT 870
CPLT 880
CPLT 890
CPLT 900
CPLT 910
CPLT 920
CPLT 930
CPLT 940
CPLT 950
CPLT 960
CPLT 970
CPLT 980
CPLT 990
CPLT1000
CPLT1010
CPLT1020
CPLT1030
CPLT1040
CPLT1050
CPLT1060
CPLT1070
CPLT1080
CPLT1090
CPLT1100
CPLT1110
CPLT1120
CPLT1130
CPLT1140
CPLT1150

VA=XA(11)
VB=YA(11)
J=1
115 I=2,ICOUNT
  IF (ABS(XA(11))-XA(1)-GT-J) GO TO 114
  IF (ABS(YA(11))-YA(1)-GT-J) GO TO 114
  J=J+1
114
  VA=XA(1)
  VB=YA(1)
  XA(J)=VA
  YA(J)=VB
115 CONTINUE
  XA(J)=XA(ICOUNT)
  YA(J)=YA(ICOUNT)
  VX(J)=VX(ICOUNT)
  VY(J)=VY(ICOUNT)
  IN=J
  IF (IN-GT-2) CALL PREPLT
  XA(1)=XA(ICOUNT)
  YA(1)=YA(ICOUNT)
  I=1
  IRET=1
116
  GO TO (102,104,1050,123),IRET
  VX(1)=VX(2)-YA(1)*JUNINT
  VY(1)=VY(2)-XA(1)*JUNINT
  VX(ICOUNT)=(XA(ICOUNT)-XA(ICOUNT-1))*JUNINT
  VY(ICOUNT)=(YA(ICOUNT)-YA(ICOUNT-1))*JUNINT
  GO TO 113
117 IF (ISAVE.NE.ICOUNT) GO TO 118
  GO TO (102,104,1050,123),IRET
118 LOG4=0
  X=ABS(XA(1))-XA(ISAVE+1)
  Y=ABS(YA(1))-YA(ISAVE+1)
  IF (X+Y-GT-1.E-4) GO TO 122
  I=ISAVE/2
  K=ISAVE
  GO TO 119 J=1,1
  X=XA(J)
  XA(J)=XA(K)
  XA(K)=X
  Y=YA(J)
  YA(J)=YA(K)
  YA(K)=Y
119 K=K-1
  ICOUNT=ICOUNT-1
  K=ISAVE+1
  GO TO 121 J=ISAVE,ICOUNT
  XA(J)=XA(K)
  YA(J)=YA(K)
121 K=K-1
  ISAVE=0
  GO TO 120
122 K=K-1
  KSAVE=ISAVE
  IRET=4
  GO TO 116

```

```

SUBROUTINE CPLOT (IPLOT,RON,COL,ELEV)
COMMON /81/ A,B,ALF,NA,NB,AA,BB,AX,AY,AF,BF,X1,X2,Y1,Y2,CALF,SALF
1 A(1)=LE(20)
COMMON /PLOT/ ITOT,IN,NP,IT,NT,UNIT,LOG1,LOG2,LOG3,LOG4,ICOUNT,NCOCPLT,
UNIT,NOLG,IT2,C14000,XA(4001),YA(4001),VX(4001),VY(4001)
XX=COL*RB+RON*AA+CALF*X1
YY=ROW*AA+SALF*Y1
IF (IPLOT-1) 101,103,106
101 IF (ICOUNT-LE-1) GO TO 102
  IRET=1
  GO TO 107
102 IF (LOG4-EO-1) GO TO 103
  ICOUNT=0
103 ICOUNT=ICOUNT-LT,NCOUNT) GO TO 104
  IRET=2
  GO TO 107
104 ICOUNT=ICOUNT+1
  XA(ICOUNT)=XXX
  YA(ICOUNT)=YYY
  GO TO 107
C
C
C
NOTE INTERCHANGE OF X AND Y
RETURN
1050 IF (NOT(GE.O)CALL NUMBER(XXX,YYY,.1,ELEV,90.0,NOIG))
  RETURN
106 IRET=3
  IF (LOG4-EO-1) GO TO 118
  IF (LOG4-EO-1) GO TO 117
  X=ABS(XA(1))-XA(ICOUNT)
  Y=ABS(YA(1))-YA(ICOUNT)
  IF (X+Y-GT-1.E-6) GO TO 112
  LOG3=0
  X=XA(1)
  Y=YA(1)
  BY=Y-Y1
108 IF (AMIN(LABS(8Y1),ABS(Y-V21))-LE,1.E-4) GO TO 110
  BY=BYCALF/SALF
  IF (AMIN(LABS(X-X1)-BY),ABS(X-X2-BY))-LT,1.E-4) GO TO 110
  IF (LOG3-GT-0) GO TO 116
  LOG3=1
  X=XA(ICOUNT)
  Y=YA(ICOUNT)
  GO TO 108
110 IF (LOG3-EO-2) GO TO 116
  IF (LOG3-EO-1) GO TO 111
  LOG3=2
  GO TO 109
111 LOG4=1
  ISAVE=ICOUNT
  GO TO (102,104,1050,123),IRET
112 VX(1)=VX(2)-YA(ICOUNT-1))*0.5JUNINT
  VY(1)=VY(1)-XA(ICOUNT-1))*0.5JUNINT
  VY(1)=VY(ICOUNT)
  UA=AA*JUNINT*0.7
  UB=BB*JUNINT*0.7

```

```

123 IRET=KRET
      COUNT=COUNT-KSAVE
      KSAVE=KSAVE+1
      ISAVE=1
      GO TO 120
END

```

```

CPLT1160
CPLT1170
CPLT1180
CPLT1190
CPLT1200
CPLT1210
CPLT1220

SUBROUTINE ICOUNT (DATA, NRUM, NCOL, NRUSO, NCUSO, CBEG, CLIM, ACSTP)
  ICNT 10
  CONTOURING SUBPROGRAM BY S. H. ZISK, MIT LINCOLN LAB, MARCH 1968-
  ICNT 20
  REMITTEN IN USASI BASIC FORTRAN BY NM BRENNER MIT LL, MARCH 1968-
  ICNT 30
  DO 4000 XLEV=CBEG,CLIM,CSTP (EFFECTIVELY, NOT LITERALLY)
  ICNT 40
  CSTP IS ACSTP WITH THE SIGN CHOSEN TO INCREASE IN THE CORRECT
  ICNT 50
  DIRECTION FROM CBEG TO CLIM.
  ICNT 60
  FOR EACH XLEV, PLOTS A CONTOUR OF DATA(I,J), OUTPUT BEING RETURNED
  ICNT 70
  TO SUBROUTINE.
  ICNT 80
  UP OR DOWN TRACES. CLOT12, CLOT13, FOR LABELING AT THIS POSITION.
  ICNT 90
  IF DESIRED, FULL CALL IS CALL GPLOT(I1PLOT, ROW, COL, XLEV1, WHERE
  ICNT 100
  ROW IS FROM 1- TO FLOAT(IMAX1), COL IS FROM 1- TO FLOAT(IMAX1).
  ICNT 110
  CONTR EXTRUDES ONE POINT AT A TIME TO CLOT. IF DESIRED FOR
  ICNT 120
  EFFICIENCY, CLOT MAY SAVE UP POINTS IN A SCRATCH ARRAY.
  ICNT 130
  WHEN IPLOT IS 0, CLOT SHOULD DRAW A LINE SEGMENT FROM THE REMEM-
  ICNT 140
  BERED POINT TO THE NEW POINT, AND THEN MAKE THE NEW POINT THE REME-
  ICNT 150
  BERED POINT.
  ICNT 160
  A CONTOUR LABEL IS CALLED FROM CLOT (I1PLOT=2), ONLY ONCE PER
  ICNT 170
  COMPLETE CONTOUR SEGMENT, SO THAT IF SEVERAL DIFFERENT LOOPS ARE
  ICNT 180
  AT HEIGHT XLEV, THEY WILL EACH GET A LABEL.
  ICNT 190
  ICNT 200
  ICNT 210
  ICNT 220
  THIS PROGRAM IS WRITTEN IN USASI BASIC FORTRAN IN AN ATTEMPT TO BE
  ICNT 230
  COMPATIBLE WITH AS MANY EXISTING FORTRAN COMPILERS AS POSSIBLE.
  ICNT 240
  AS WRITTEN, THIS PROGRAM ASSUMES DATA IS A FLOATING POINT ARRAY.
  ICNT 250
  ICNT 260
  DIMENSION DATA(I)
  ICNT 270
  REAL MARK
  ICNT 280
  ICNT 290
  DIMENSION DATA(NRUM,NCOL), OF WHICH ONLY (IMAX1,MAX1) ARE USED.
  ICNT 300
  NOTE--THE LOW ORDER BIT OF EACH ENTRY DATA(I,J) IS LIABLE TO CHANG-
  ICNT 310
  THIS WILL NEGLIGIBLY AFFECT A FLOATING POINT ARRAY.
  ICNT 320
  ICNT 330
  CORRECTED AND MODIFIED FEB. 1970. G F BID. SC.
  ICNT 340
  ICNT 350
  1RT AND 1UP INDICATE THE DIRECTION OF THE LAST CONTOUR STEP.
  ICNT 360
  1RT=0, 1 INDICATES THAT THE LAST STEP HAD X DECREASING, INCREASING
  ICNT 370
  1UP=0, 1 INDICATES THAT THE LAST STEP HAD Y DECREASING, INCREASING.
  ICNT 380
  DIRECTION OF THE NEXT CONTOUR STEP IS DETERMINED BY THE VALUES AT
  ICNT 390
  A+B, C, AND 0 WITH THE LAST STEP ENJOING ON OA OR AT 0 (SPECIAL CASE)
  ICNT 400
  AND A+B, C, 0 THE VERTICES OF A SQUARE LABELLED IN ORDER.
  ICNT 410
  A TEST BASED ON THE VALUE DIE (AN ESTIMATE OF THE VALUE AT THE CEN-
  ICNT 420
  OF THE SQUARE) WAS ADDED TO MAKE THE CONTOURING MORE CONSISTENT.
  ICNT 430
  ICNT 440
  ICNT 450
  MAXX=NRUSO
  ICNT 460
  ICNT 470
  ICNT 480
  ICNT 490
  ICNT 500
  ICNT 510
  ICNT 520
  ICNT 530
  ICNT 540
  ICNT 550
  ICNT 560
  ICNT 570
  MAXX=NRUSO
  ICNT 580
  ICNT 590
  CSTP=SIGN(CSTP,CLIM-CBEG)
  ICNT 600
  CTR=CBEG
  ICNT 610
  CLEAR LEAST SIGNIFICANT BIT
  ICNT 620
  101 XLEV=UNMARK(CTR)
  ICNT 630
  JLOOP=1
  ICNT 640
  JUP=JLOOP
  ICNT 650
  1X=1
  ICNT 660
  1Y=1
  ICNT 670
  NTOF=NRUM*MAXY
  ICNT 680
  DO 102 I=1,NTOF
  ICNT 690
  102 DATA(I)=UNMARK(DATA(I))
  ICNT 700

```

ICNT1160
ICNT1170
ICNT1180
ICNT1190
ICNT1200
ICNT1210
ICNT1220
ICNT1230
ICNT1240
ICNT1250
ICNT1260
ICNT1270
ICNT1280
ICNT1290
ICNT1300
ICNT1310
ICNT1320
ICNT1330
ICNT1340
ICNT1350
ICNT1360
ICNT1370
ICNT1380
ICNT1390
ICNT1400
ICNT1410
ICNT1420
ICNT1430
ICNT1440
ICNT1450
ICNT1460
ICNT1470
ICNT1480
ICNT1490
ICNT1500
ICNT1510
ICNT1520
ICNT1530
ICNT1540
ICNT1550
ICNT1560
ICNT1570
ICNT1580
ICNT1590
ICNT1600
ICNT1610
ICNT1620
ICNT1630
ICNT1640
ICNT1650
ICNT1660
ICNT1670
ICNT1680
ICNT1690
ICNT1700
ICNT1710
ICNT1720
ICNT1730

IF I1X-1) 216,120,137
120 LOOP=0
GO TO 137
121 IF I1X-MAX+1) 130,122,122
122 IF I1Y-1) 217,130,123
C
-C FINOING THE LOWER OR UPPER CORNER OF A PLATEAU THAT HITS THE
C RIGHT EDGE.
123 IF (OJAZ-OJAZ2) 131,124,131
124 L=L+1-NROW
L=L+1-NROW
LX=L-NROW
OJAZ=UNMARK(DATAILPX1)
OJAZ=UNMARK(DATAILMX1)
IF (OJAZ-XLEV) 125,126,125
125 IUP=0
GO TO 127
126 IF (OJAZ-XLEV) 127,131,127
C
C IF BOTH UPPER AND LOWER POINTS ARE ALSO ON, THEN DUMP THIS ONE.
C
127 IRT=0
ILOOP=0
XPT=MAXX
X1=XPT
GO TO 137
C
C SKIPS ANY BLOCK OF ALL XLEV
C FOR 1ST POINT GREATER THAN XLEV
C
128 IF (XLEV-OJAZ2) 130,130,136
C
C FOR 1ST POINT LESS THAN XLEV
C
129 IF (XLEV-OJAZ2) 136,130,130
C
C OMTS ANY RIGHT HANO EDGE COLUMN OF ALL XLEV
C
130 IF (I1X-MAX+1) 135,131,131
C
C IF I1X = MAXX-1 WE JUST SCANNED THE LAST COLUMN-GAP...MUST SWITCH
C ROWS.
C
131 IF I1Y-MAXY) 133,132,218
C
C IF IY = MAXY, WE ARE AT THE TOP ROW ALSO AND CONTOURING IS DONE.
C
132 ILOUP=1
GO TO 207
133 IY=1
IY=IY+1
L=IX+NROW*(IY-1)
IF I1Y-MAXY) 105,134,219
134 JLOUP=0
ILOOP=JLOUP
JUP=ILOOP

ICNT 580
ICNT 590
ICNT 600
ICNT 610
ICNT 620
ICNT 630
ICNT 640
ICNT 650
ICNT 660
ICNT 670
ICNT 680
ICNT 690
ICNT 700
ICNT 710
ICNT 720
ICNT 730
ICNT 740
ICNT 750
ICNT 760
ICNT 770
ICNT 780
ICNT 790
ICNT 800
ICNT 810
ICNT 820
ICNT 830
ICNT 840
ICNT 850
ICNT 860
ICNT 870
ICNT 880
ICNT 890
ICNT 900
ICNT 910
ICNT 920
ICNT 930
ICNT 940
ICNT 950
ICNT 960
ICNT 970
ICNT 980
ICNT 990
ICNT1000
ICNT1010
ICNT1020
ICNT1030
ICNT1040
ICNT1050
ICNT1060
ICNT1070
ICNT1080
ICNT1090
ICNT1100
ICNT1110
ICNT1120
ICNT1130
ICNT1140
ICNT1150

THE LEAST SIGNIFICANT BIT OF DATAIL1) IS USED TO MARK THE LEFTHAND
EDGE OF THE CONTOUR WHEN IT CROSSES THAT ROW.
C SEARCH SCANS THE ROWS FROM LEFT TO RIGHT, AND BOTTOM TO TOP.
C LOOKING FOR THE FIRST POINT ON THE XLEV CONTOUR.
103 IUP=JUP
ILOOP=JLOUP
IRT=1
IF I1X-MAXX) 104,131,212
104 L=1+NROW*(IY-1)
C
C IY-1Y SAVE THE LAST POINT THAT WAS SEARCHED, TO RESTART THE
C SEARCH AFTER FINISHING THE CURRENT CONTOUR LINE.
105 OJAZ=UNMARK(DATAIL)
OJAZ=UNMARK(DATAIL)
IF (OJAZ-XLEV) 106,116,106
106 IF (I1X-1) 213,107,116
107 IF (I1Y-1) 214,112,108
108 L=L+1-NROW
OJAZ=UNMARK(DATAIL)
OJAZ=UNMARK(DATAIL)
IF (OJAZ-XLEV) 111,109,111
109 IF (OJAZ-OJAZ2) 111,110,111
110 YPT=IY-1
GO TO 115
111 IF (I1Y-MAXY) 112,116,215
C
C LOOKING FOR AN INTERSECTION IN THE LEFT-HAND COLUMN BEFORE
C SCANNING FOR INTERSECTIONS IN THE CURRENT ROW.
112 LPX=L-NROW
OJAZ=UNMARK(DATAILPX1)
IF (OJAZ-XLEV) 113,116,113
113 IF (OJAZ-OJAZ2)*(OJAZ-XLEV) 114,114,116
C
C ARE BOTH DIO AND OJAZ ON THE SAME SIDE OF THE CONTOUR
C
114 CEL=OJAZ-OJAZ1
IF (CEL=0) I1X=1-CEL
XPT=OJAZ-OJAZ1
XPT=OJAZ-OJAZ1
X1=XPT
Y1=YPT
ILOOP=0
IF (OJAZ-OJAZ2) 113,130,130
C
C IF TWO ROWS ARE EACH FILLED WITH HIGH AND LOW NUMBERS RESPECTIVELY
C WE HAVE JUST FOUND THE INTER-ROW CONTOUR.
116 OJAZ=UNMARK(DATAIL)
OJAZ=UNMARK(DATAIL)
IF (OJAZ-OJAZ2) 130,117,130
117 IF (OJAZ-XLEV) 129,118,128
118 IF (OJAZ-XLEV) 119,121,119
119 XPT=IX


```

175 IF (IXPT+IRT-MAXI) 172,172,176
176 IDENT=IDENT+2
GO TO 171
C
C Y-LIMIT CHECK
C
177 IF (IYPT+IUP-2) 173,172,178
178 IF (IYPT+IUP-MAXY) 172,172,173
179 YPT=IYA
YPT=IYC
GO TO 194
180 XPT=IX8
YPT=IY8
GO TO 194
181 XPT=IXC
YPT=IYC
IF (IDENT) 182,196,194
C
C DON'T CHANGE DIRECTION IF IT'S AN **ON-TO-ON**
C
182 IF (IIND-1) 183,192,183
183 IRT=1-IRT
GO TO 194
184 DEL=018-DIA
IF (ABS(DEL),LT,1.0E-4)DEL=SIGN(1.0E-4,DEL)
DEL=DEL/DIG/DEL
IF (IIND-2) 185,186,185
185 XPT=FLOAT(IXA)+DEL*FLOAT(IRT+IRT-1)
YPT=IYA
GO TO 194
186 YPT=FLOAT(IYA)+DEL*FLOAT(IUP+IUP-1)
XPT=IXA
GO TO 194
187 DEL=018-DIC
IF (ABS(DEL),LT,1.0E-4)DEL=SIGN(1.0E-4,DEL)
DEL=DEL/DIG/DEL
IF (IIND-2) 188,189,188
188 XPT=FLOAT(IXC)+DEL*FLOAT(IUP+IUP-1)
YPT=IX8
GO TO 194
189 XPT=FLOAT(IXC)+DEL*FLOAT(IRT+IRT-1)
YPT=IY8
GO TO 194
190 DEL=018-DIC
IF (ABS(DEL),LT,1.0E-4)DEL=SIGN(1.0E-4,DEL)
DEL=DEL/DIG/DEL
IF (IIND-2) 191,193,191
191 XPT=FLOAT(IXC)+DEL*FLOAT(IRT+IRT-1)
YPT=IYC
GO TO 194
192 IUP=1-IUP
GO TO 194
193 YPT=FLOAT(IYC)+DEL*FLOAT(IUP+IUP-1)
XPT=IX8
GO TO 183
194 CALL CPLUT (1,XPT,YPT,XLEV)
C
C PLOTS A LINE TO THIS LOCATION--
C

```

```

ICNT2900
ICNT2910
ICNT2920
ICNT2930
ICNT2940
ICNT2950
ICNT2960
ICNT2970
ICNT2980
ICNT2990
ICNT3000
ICNT3010
ICNT3020
ICNT3030
ICNT3040
ICNT3050
ICNT3060
ICNT3070
ICNT3080
ICNT3090
ICNT3100
ICNT3110
ICNT3120
ICNT3130
ICNT3140
ICNT3150
ICNT3160
ICNT3170
ICNT3180
ICNT3190
ICNT3200
ICNT3210
ICNT3220
ICNT3230
ICNT3240
ICNT3250
ICNT3260
ICNT3270
ICNT3280
ICNT3290
ICNT3300
ICNT3310
ICNT3320
ICNT3330
ICNT3340
ICNT3350
ICNT3360
ICNT3370
ICNT3380
ICNT3390
ICNT3400
ICNT3410
ICNT3420
ICNT3430
ICNT3440
ICNT3450
ICNT3460
ICNT3470

```

```

IF (LOUMP-3) 195,206,206
195 IYI=YPT
IYI=IF(XPT)*NROW*(IYPT-1)
IF(ABS(IYI-FLOAT(IYPT))-0.01)196,196,198
C
C IF YPT IS AN INTEGER, MARK THE POINT IMMEDIATELY TO THE LEFT. IF IT IS ALREADY MARKED, THIS HAS BEEN PLOTTED BEFORE.
C
196 IF(DATA(I)-UNMARK(DATA(I)))202,197,202
C
C IF THIS POINT HAS BEEN TRAVELED BEFORE...
C
197 DATA(I)=MARK(DATA(I))
C
C IF NOT, KEYS THIS POINT FOR FUTURE REFERENCE.
C
198 IF(XPT-1,0)221,2040,199
199 IF (XPT-FLOAT(MAXI)) 200,204,222
200 IF (IYPT-1,1) 223,204,201
201 IF (IYPT-FLOAT(MAXY)) 141,204,224
202 IF (XPT-XI) 204,203,204
203 IF (IYPT-IYI) 204,206,204
C
C IF CONTOUR HAS COME FULL CIRCLE, THAT'S ALL...
C
2040 DATA(I)=MARK(DATA(I))
204 IF (LOUMP-1) 206,205,206
C
C IF THE CONTOUR HITS EITHER ANY EDGE OR (ITSELF IN THE MIDDLE), IT RETURNS ONCE TO THE STARTING POINT AND BEGINS CONTOURING IN THE OTHER DIRECTION. IF THE STARTING POINT IS ON AN EDGE, IT'S THE END OF THE CONTOUR LINE.
C
205 IRT=0
IUP=0
ILOUP=2
XPT=XI
YPT=YI
CALL CPLUT (0,XPT,YPT,XLEV)
C
C MOVES THE PEN BACK TO STARTING POINT WITHOUT PLOTTING.
C
GO TO 141
206 CALL CPLUT (2,XPT,YPT,XLEV)
C
C TO NUMBER EACH SECTION OF A CONTOUR
C
GO TO 103
C
LOUMP=0, MORE TO CONTOUR...1, END OF MAP, NO MORE...
C
3, ONE-POINT CONTOUR.
C
207 IF (ICSTP) 208,210,208
208 IF (ICCTR+ICSTP-CLIM)*SIGN(1,ICSTP)-1-E*ABS(ICSTP) 209,209,210
209 CTR=CTR+ICSTP
GO TO 101
210 CALL CPLUT (0,0,0,0,0)

```

```

ICNT3480
ICNT3490
ICNT3500
ICNT3510
ICNT3520
ICNT3530
ICNT3540
ICNT3550
ICNT3560
ICNT3570
ICNT3580
ICNT3590
ICNT3600
ICNT3610
ICNT3620
ICNT3630
ICNT3640
ICNT3650
ICNT3660
ICNT3670
ICNT3680
ICNT3690
ICNT3700
ICNT3710
ICNT3720
ICNT3730
ICNT3740
ICNT3750
ICNT3760
ICNT3770
ICNT3780
ICNT3790
ICNT3800
ICNT3810
ICNT3820
ICNT3830
ICNT3840
ICNT3850
ICNT3860
ICNT3870
ICNT3880
ICNT3890
ICNT3900
ICNT3910
ICNT3920
ICNT3930
ICNT3940
ICNT3950
ICNT3960
ICNT3970
ICNT3980
ICNT3990
ICNT4000
ICNT4010
ICNT4020
ICNT4030
ICNT4040
ICNT4050

```


C	MAKE SURE ALL POINTS HAVE BEEN PLOTTED	C	SUBROUTINE INTPLT	I0
C	RETURN	C	USING RATIONAL POLYN. SPLINE INT. OF 0 V AHUJA I B M SVST J	INTP 20
C	TRAPS TO OUTPUT A MARKING IF ANY BOUNDARY IS CROSSED.	C	P 208-217	INTP 30
C		C		INTP 40
C				INTP 50
C				INTP 60
C				INTP 70
C				INTP 80
C				INTP 90
C				INTP 100
C				INTP 110
C				INTP 120
C				INTP 130
C				INTP 140
C				INTP 150
C				INTP 160
C				INTP 170
C				INTP 180
C				INTP 190
C				INTP 200
C				INTP 210
C				INTP 220
C				INTP 230
C				INTP 240
C				INTP 250
C				INTP 260
C				INTP 270
C				INTP 280
C				INTP 290
C				INTP 300
C				INTP 310
C				INTP 320
C				INTP 330
C				INTP 340
C				INTP 350
C				INTP 360
C				INTP 370
C				INTP 380
C				INTP 390
C				INTP 400
C				INTP 410
C				INTP 420
C				INTP 430
C				INTP 440
C				INTP 450
C				INTP 460
C				INTP 470
C				INTP 480
C				INTP 490
C				INTP 500
C				INTP 510
C				INTP 520
C				INTP 530
C				INTP 540
C				INTP 550
C				INTP 560
C				INTP 570

```

A5=3,*@X1C-XCJ1-A9-A9-A9
A6=3,*@Y1C-YCJ1-A10-A10-A10
      (C1
      U=0
      GO=JOINT
      W=(1A10+A5)*U+A9*W+YC
      W=(1A20+A6)*U+A10*W+YC
      CALL PLOT(WX,WY,2)
      I=1+
      IF (1-LF.NP) GO TO 104
      IF=IC+1
      IF (IC-LI.IN) GO TO 103
      RETURN
      END

```

2

```

C COMMENT CARDS FOR FINPGC
C
C NBS SEPTEMBER , 1971
C
C THIS PROGRAM IS AN ADAPTATION OF THE XRAY 67 PROGRAM LIST FC, IT HAS
C BEEN ALTERED TO STAND ALONE AND READ THE FOURIER OUTPUT TAPS WRITTEN
C ON TAPE. THE LAST SQUARES PROGRAM WRITTEN BY L. W. FINGER AT TBB
C PHYSICAL LAB, CARNEGIE INSTITUTE OF WASHINGTON. THE PHASE IN
C CRYSTALLOGRAPHY HAS BEEN REPLACED BY SIGMA(P), SCALED UP BY A FACTOR OF
C MILLICYCLES/Å HAS BEEN REPLACED BY SIGMA(P), SCALED UP BY A FACTOR OF
C 10 TO MAKE IT CONSISTENT WITH PG,
C
C CARD ONE
C
C COL 1-6 COMPOUND IDENTIFICATION, 7-78 ANY TITLE
C
C CARD TWO
C
C COL 14 (1/2)/(3) FOR P INDEX VARIES (MOST)/(NEXT MOST)/(LEAST) RAPIDLY
C LIST 120
C LIST 130
C LIST 140
C LIST 150
C LIST 160
C LIST 170
C LIST 180
C LIST 190
C LIST 200
C LIST 210
C LIST 220
C LIST 230
C LIST 240
C LIST 250
C LIST 260
C LIST 270
C LIST 280
C LIST 290
C LIST 300
C LIST 310
C LIST 320
C LIST 330
C LIST 340
C LIST 350
C LIST 360
C LIST 370
C LIST 380
C LIST 390
C LIST 400
C LIST 410
C LIST 420
C LIST 430
C LIST 440
C LIST 450
C LIST 460
C LIST 470
C LIST 480
C LIST 490
C LIST 500
C LIST 510
C LIST 520
C LIST 530
C LIST 540
C LIST 550
C LIST 560
C LIST 570
C LIST 580
C LIST 590
C LIST 600
C LIST 610
C LIST 620
C LIST 630
C LIST 640
C LIST 650
C LIST 660
C LIST 670
C LIST 680
C LIST 690
C LIST 700
C LIST 710
C LIST 720
C LIST 730
C LIST 740
C LIST 750
C LIST 760
C LIST 770
C LIST 780
C LIST 790
C LIST 800
C LIST 810
C LIST 820
C LIST 830
C LIST 840
C LIST 850
C LIST 860
C LIST 870
C LIST 880
C LIST 890
C LIST 900
C LIST 910
C LIST 920
C LIST 930
C LIST 940
C LIST 950
C LIST 960
C LIST 970
C LIST 980
C LIST 990
C LIST 1000
C LIST 1010
C LIST 1020
C LIST 1030
C LIST 1040
C LIST 1050
C LIST 1060
C LIST 1070
C LIST 1080
C LIST 1090
C LIST 1100
C LIST 1110
C LIST 1120
C LIST 1130
C LIST 1140
C LIST 1150
C LIST 1160
C LIST 1170
C LIST 1180
C LIST 1190
C LIST 1200
C LIST 1210
C LIST 1220
C LIST 1230
C LIST 1240
C LIST 1250
C LIST 1260
C LIST 1270
C LIST 1280
C LIST 1290
C LIST 1300
C LIST 1310
C LIST 1320
C LIST 1330
C LIST 1340
C LIST 1350
C LIST 1360
C LIST 1370
C LIST 1380
C LIST 1390
C LIST 1400
C LIST 1410
C LIST 1420
C LIST 1430
C LIST 1440
C LIST 1450
C LIST 1460
C LIST 1470
C LIST 1480
C LIST 1490
C LIST 1500
C LIST 1510
C LIST 1520
C LIST 1530
C LIST 1540
C LIST 1550
C LIST 1560
C LIST 1570
C LIST 1580
C LIST 1590
C LIST 1600
C LIST 1610
C LIST 1620
C LIST 1630
C LIST 1640
C LIST 1650
C LIST 1660
C LIST 1670
C LIST 1680
C LIST 1690
C LIST 1700
C LIST 1710
C LIST 1720
C LIST 1730
C LIST 1740
C LIST 1750
C LIST 1760
C LIST 1770
C LIST 1780
C LIST 1790
C LIST 1800
C LIST 1810
C LIST 1820
C LIST 1830
C LIST 1840
C LIST 1850
C LIST 1860
C LIST 1870
C LIST 1880
C LIST 1890
C LIST 1900
C LIST 1910
C LIST 1920
C LIST 1930
C LIST 1940
C LIST 1950
C LIST 1960
C LIST 1970
C LIST 1980
C LIST 1990
C LIST 2000
C LIST 2010
C LIST 2020
C LIST 2030
C LIST 2040
C LIST 2050
C LIST 2060
C LIST 2070
C LIST 2080
C LIST 2090
C LIST 2100
C LIST 2110
C LIST 2120
C LIST 2130
C LIST 2140
C LIST 2150
C LIST 2160
C LIST 2170
C LIST 2180
C LIST 2190
C LIST 2200
C LIST 2210
C LIST 2220
C LIST 2230
C LIST 2240
C LIST 2250
C LIST 2260
C LIST 2270
C LIST 2280
C LIST 2290
C LIST 2300
C LIST 2310
C LIST 2320
C LIST 2330
C LIST 2340
C LIST 2350
C LIST 2360
C LIST 2370
C LIST 2380
C LIST 2390
C LIST 2400
C LIST 2410
C LIST 2420
C LIST 2430
C LIST 2440
C LIST 2450
C LIST 2460
C LIST 2470
C LIST 2480
C LIST 2490
C LIST 2500
C LIST 2510
C LIST 2520
C LIST 2530
C LIST 2540
C LIST 2550
C LIST 2560
C LIST 2570
C LIST 2580
C LIST 2590
C LIST 2600
C LIST 2610
C LIST 2620
C LIST 2630
C LIST 2640
C LIST 2650
C LIST 2660
C LIST 2670
C LIST 2680
C LIST 2690
C LIST 2700
C LIST 2710
C LIST 2720
C LIST 2730
C LIST 2740
C LIST 2750
C LIST 2760
C LIST 2770
C LIST 2780
C LIST 2790
C LIST 2800
C LIST 2810
C LIST 2820
C LIST 2830
C LIST 2840
C LIST 2850
C LIST 2860
C LIST 2870
C LIST 2880
C LIST 2890
C LIST 2900
C LIST 2910
C LIST 2920
C LIST 2930
C LIST 2940
C LIST 2950
C LIST 2960
C LIST 2970
C LIST 2980
C LIST 2990
C LIST 3000
C LIST 3010
C LIST 3020
C LIST 3030
C LIST 3040
C LIST 3050
C LIST 3060
C LIST 3070
C LIST 3080
C LIST 3090
C LIST 3100
C LIST 3110
C LIST 3120
C LIST 3130
C LIST 3140
C LIST 3150
C LIST 3160
C LIST 3170
C LIST 3180
C LIST 3190
C LIST 3200
C LIST 3210
C LIST 3220
C LIST 3230
C LIST 3240
C LIST 3250
C LIST 3260
C LIST 3270
C LIST 3280
C LIST 3290
C LIST 3300
C LIST 3310
C LIST 3320
C LIST 3330
C LIST 3340
C LIST 3350
C LIST 3360
C LIST 3370
C LIST 3380
C LIST 3390
C LIST 3400
C LIST 3410
C LIST 3420
C LIST 3430
C LIST 3440
C LIST 3450
C LIST 3460
C LIST 3470
C LIST 3480
C LIST 3490
C LIST 3500
C LIST 3510
C LIST 3520
C LIST 3530
C LIST 3540
C LIST 3550
C LIST 3560
C LIST 3570
C LIST 3580
C LIST 3590
C LIST 3600
C LIST 3610
C LIST 3620
C LIST 3630
C LIST 3640
C LIST 3650
C LIST 3660
C LIST 3670
C LIST 3680
C LIST 3690
C LIST 3700
C LIST 3710
C LIST 3720
C LIST 3730
C LIST 3740
C LIST 3750
C LIST 3760
C LIST 3770
C LIST 3780
C LIST 3790
C LIST 3800
C LIST 3810
C LIST 3820
C LIST 3830
C LIST 3840
C LIST 3850
C LIST 3860
C LIST 3870
C LIST 3880
C LIST 3890
C LIST 3900
C LIST 3910
C LIST 3920
C LIST 3930
C LIST 3940
C LIST 3950
C LIST 3960
C LIST 3970
C LIST 3980
C LIST 3990
C LIST 4000
C LIST 4010
C LIST 4020
C LIST 4030
C LIST 4040
C LIST 4050
C LIST 4060
C LIST 4070
C LIST 4080
C LIST 4090
C LIST 4100
C LIST 4110
C LIST 4120
C LIST 4130
C LIST 4140
C LIST 4150
C LIST 4160
C LIST 4170
C LIST 4180
C LIST 4190
C LIST 4200
C LIST 4210
C LIST 4220
C LIST 4230
C LIST 4240
C LIST 4250
C LIST 4260
C LIST 4270
C LIST 4280
C LIST 4290
C LIST 4300
C LIST 4310
C LIST 4320
C LIST 4330
C LIST 4340
C LIST 4350
C LIST 4360
C LIST 4370
C LIST 4380
C LIST 4390
C LIST 4400
C LIST 4410
C LIST 4420
C LIST 4430
C LIST 4440
C LIST 4450
C LIST 4460
C LIST 4470
C LIST 4480
C LIST 4490
C LIST 4500
C LIST 4510
C LIST 4520
C LIST 4530
C LIST 4540
C LIST 4550
C LIST 4560
C LIST 4570
C LIST 4580
C LIST 4590
C LIST 4600
C LIST 4610
C LIST 4620
C LIST 4630
C LIST 4640
C LIST 4650
C LIST 4660
C LIST 4670
C LIST 4680
C LIST 4690
C LIST 4700
C LIST 4710
C LIST 4720
C LIST 4730
C LIST 4740
C LIST 4750
C LIST 4760
C LIST 4770
C LIST 4780
C LIST 4790
C LIST 4800
C LIST 4810
C LIST 4820
C LIST 4830
C LIST 4840
C LIST 4850
C LIST 4860
C LIST 4870
C LIST 4880
C LIST 4890
C LIST 4900
C LIST 4910
C LIST 4920
C LIST 4930
C LIST 4940
C LIST 4950
C LIST 4960
C LIST 4970
C LIST 4980
C LIST 4990
C LIST 5000
C LIST 5010
C LIST 5020
C LIST 503
```


124

126


```

8411 CONTINUE
      IX( ISET2 ) = IX( IPIX )
      ITEMF = ( IPERC - IBLNK - ITEMP2 - IPIX ) / 2
      IFIX = IPERC - ITEMF - ITEMP2 - IPIX
      IF( ITEMP ) 8421, 8431, 8441
8421 WRITE( IOUT, 6422 ) INSH, NL, NP
8422 FORMAT( I0, 6, 22 ) INSH, NL, NP
      8441 THERE IS A HEADING THAT COMES OUT TOO WIDE.
C-----NO SPARE COLUMNS FOR CENTERING THE HEADING
8431 CONTINUE
      IX( 6 ) = IBLANK
      IX( 7 ) = IBLANK
      IX( 8 ) = IBLANK
      GO TO 8445
C-----READING NEEDS CENTERING GET OUT BCD CONTROL FOR FORMAT
8441 CONTINUE
      ITEMP2 = ITEMP - IBLNK - IPIX
      ISET2 = ISET1 - ITEMP2 - IPIX
      8442 CONTINUE = I0) 8442, 6443, 8443
8442 CONTINUE = I0) 8442, 6443, 8443
      IX( 8 ) = IXX( ITEMP )
      IX( 9 ) = IBLANK
      IX( 10 ) = IBLANK
      GO TO 8445
C-----ITS TWO DECIMAL PLACES LONG
8443 CONTINUE
      IFIX = ITEMP / I0
      IFIX = ITEMP / I0
      IX( 8 ) = INUM( IFIX * I0
      IX( 9 ) = INUM( IFIX * I0
      IX( 10 ) = IXXX
8445 CONTINUE
      IX( 2 ) = IBLANK
      IX( 3 ) = IBLANK
      IF( IFIX ) 8446, 8446, 8447
8446 CONTINUE
      IX( 1 ) = IBLANK
      GO TO 8450
8447 CONTINUE
      IF( IFIX - I0 ) 8448, 8449, 8449
8448 CONTINUE
      IX( 1 ) = IXX( IFIX )
      GO TO 8450
8449 CONTINUE
      IFIX = IFIX / I0
      IFIX = IFIX / I0
      IX( 1 ) = INUM( IFIX * I0
      IX( 2 ) = INUM( IFIX * I0
      IX( 3 ) = IXXX
8450 CONTINUE
C-----STOP THE FORMAT FOR A COLUMN HEADING
      GO 9451 J = I, I0
      IFUT = IFUT - I
      IF( IFUT ) = IX( J )
8451 GO TO 8461
C-----THIS IS A GONAPLOE REFLECTION OATON ABOVE IT... IN THE BUFFER
8501 CONTINUE
      IF( ISIGCS ) 8504, 8504, 8502
      LSTF5000
      LSTF5001
      LSTF5002
      LSTF5003
      LSTF5004
      LSTF5005
      LSTF5006
      LSTF5007
      LSTF5008
      LSTF5009
      LSTF5010
      LSTF5011
      LSTF5012
      LSTF5013
      LSTF5014
      LSTF5015
      LSTF5016
      LSTF5017
      LSTF5018
      LSTF5019
      LSTF5020
      LSTF5021
      LSTF5022
      LSTF5023
      LSTF5024
      LSTF5025
      LSTF5026
      LSTF5027
      LSTF5028
      LSTF5029
      LSTF5030
      LSTF5031
      LSTF5032
      LSTF5033
      LSTF5034
      LSTF5035
      LSTF5036
      LSTF5037

```

```

C-----SEE IF THIS IS A LESS THAN
8502 IF(SQ(I) - IFLT) 8504,8503,8504
C-----IF(S) AND DEPARTS IT MINUS
8504 IF(I) - IFLT(I)
8504 CONTINUE - IFLT(I)
C-----NOW WE MOVE THE DEGRIS TO THE BUFFER
C-----MOVE THE INDEX IF NEEDED BE
IF(IIN) 8512,8512,8511
8511 IOUT = IOUT + 1
8512 CONTINUE
C-----IF IFCG, 8532,8532,8521
8521 IOUT = IOUT + 1
8522 CONTINUE
C-----MOVE LESS-THAN EXTING SIGNAL IF NEEDED
IF(SIGN(I) 8532,8532,8531
8531 IOUT = IOUT + 1
8532 CONTINUE
C-----IF IFCG, 8542,8542,8541
8541 IOUT = IOUT + 1
8542 CONTINUE
C-----MOVE PHASE
IF(IPHC) 8552,8552,8551
8551 IOUT = IOUT + 1
8552 IOUT(IOUT) = IPHS(I)
C-----THE IFC ARRAY IS THE ACTUAL REFLECTION IN FORMATION FORMAT. IT IS
C-----SET DURING INITIALIZATIONS AT FIRST OF PROGRAM.
05 8561 J=1,6
IOUT=IOUT + 1
IOUT(IOUT) = IFC(J)
8561 CONTINUE
8601 CONTINUE LAST CLOSE PARENTHESIS IN THE FORMAT ARRAY
IOUT(IOUT) = IFC(I)
C-----CHECK OUT THE LINE NOW FORMED
IF(IOUT) 8651,8651,8653
8651 CONTINUE
WRITE (NTOUT,IPMT)
IF(IWOT) 8655,8655,8652
8652 WRITE(NTAPE,IPMT)
06 TO 8655
8653 WRITE(NTOUT,IEXT) (IOUT(J), J=1,IOUT)
IF(IWOT) 8655,8655,8654
8654 CONTINUE
WRITE(NTAPE,IPMT) (IOUT(J),J=1,IOUT)
8655 CONTINUE
C-----SEE IF ALL LINES ON THIS SHEET OF THIS PAGE ARE 000S
IF(NL-LINE) 8701,8701,8701
8701 IF(NSHEET-I) 8705,8705,8702
8702 WRITE (NTOUT,8102)
LSTF6360
LSTF6390
LSTF6400
LSTF6410
LSTF6420
LSTF6430
LSTF6440
LSTF6450
LSTF6460
LSTF6470
LSTF6480
LSTF6490
LSTF6500
LSTF6510
LSTF6520
LSTF6530
LSTF6540
LSTF6550
LSTF6560
LSTF6570
LSTF6580
LSTF6590
LSTF6600
LSTF6610
LSTF6620
LSTF6630
LSTF6640
LSTF6650
LSTF6660
LSTF6670
LSTF6680
LSTF6690
LSTF6700
LSTF6710
LSTF6720
LSTF6730
LSTF6740
LSTF6750
LSTF6760
LSTF6770
LSTF6780
LSTF6790
LSTF6800
LSTF6810
LSTF6820
LSTF6830
LSTF6840
LSTF6850
LSTF6860
LSTF6870
LSTF6880
LSTF6890
LSTF6900
LSTF6910
LSTF6920
LSTF6930
LSTF6940
LSTF6950
LSTF6960
LSTF6970
LSTF6980
LSTF6990
LSTF7000
LSTF7010
LSTF7020
LSTF7030
LSTF7040
LSTF7050
LSTF7060
LSTF7070
LSTF7080
LSTF7090
LSTF7100
LSTF7110
LSTF7120
LSTF7130
LSTF7140
LSTF7150
LSTF7160
LSTF7170
LSTF7180
LSTF7190
LSTF7200
LSTF7210
LSTF7220
LSTF7230
LSTF7240
LSTF7250
LSTF7260
LSTF7270
LSTF7280
LSTF7290
LSTF7300
LSTF7310
LSTF7320
LSTF7330
LSTF7340
LSTF7350
LSTF7360
LSTF7370
LSTF7380
LSTF7390
LSTF7400
LSTF7410
LSTF7420
LSTF7430
LSTF7440
LSTF7450
LSTF7460
LSTF7470
LSTF7480
LSTF7490
LSTF7500
LSTF7510
LSTF7520
LSTF7530
LSTF7540
LSTF7550
LSTF7560
LSTF7570
LSTF7580
LSTF7590
LSTF7600
LSTF7610
LSTF7620
LSTF7630
LSTF7640
LSTF7650
LSTF7660
LSTF7670
LSTF7680
LSTF7690
LSTF7700
LSTF7710
LSTF7720
LSTF7730
LSTF7740
LSTF7750
LSTF7760
LSTF7770
LSTF7780
LSTF7790
LSTF7800
LSTF7810
LSTF7820
LSTF7830
LSTF7840
LSTF7850
LSTF7860
LSTF7870
LSTF7880
LSTF7890
LSTF7900
LSTF7910
LSTF7920
LSTF7930
LSTF7940
LSTF7950
LSTF7960
LSTF7970
LSTF7980
LSTF7990
LSTF8000
LSTF8010
LSTF8020
LSTF8030
LSTF8040
LSTF8050
LSTF8060
LSTF8070
LSTF8080
LSTF8090
LSTF8100
LSTF8110
LSTF8120
LSTF8130
LSTF8140
LSTF8150
LSTF8160
LSTF8170
LSTF8180
LSTF8190
LSTF8200
LSTF8210
LSTF8220
LSTF8230
LSTF8240
LSTF8250
LSTF8260
LSTF8270
LSTF8280
LSTF8290
LSTF8300
LSTF8310
LSTF8320
LSTF8330
LSTF8340
LSTF8350
LSTF8360
LSTF8370
LSTF8380
LSTF8390
LSTF8400
LSTF8410
LSTF8420
LSTF8430
LSTF8440
LSTF8450
LSTF8460
LSTF8470
LSTF8480
LSTF8490
LSTF8500
LSTF8510
LSTF8520
LSTF8530
LSTF8540
LSTF8550
LSTF8560
LSTF8570
LSTF8580
LSTF8590
LSTF8600
LSTF8610
LSTF8620
LSTF8630
LSTF8640
LSTF8650
LSTF8660
LSTF8670
LSTF8680
LSTF8690
LSTF8700
LSTF8710
LSTF8720
LSTF8730
LSTF8740
LSTF8750
LSTF8760
LSTF8770
LSTF8780
LSTF8790
LSTF8800
LSTF8810
LSTF8820
LSTF8830
LSTF8840
LSTF8850
LSTF8860
LSTF8870
LSTF8880
LSTF8890
LSTF8900
LSTF8910
LSTF8920
LSTF8930
LSTF8940
LSTF8950
LSTF8960
LSTF8970
LSTF8980
LSTF8990
LSTF9000
LSTF9010
LSTF9020
LSTF9030
LSTF9040
LSTF9050
LSTF9060
LSTF9070
LSTF9080
LSTF9090
LSTF9100
LSTF9110
LSTF9120
LSTF9130
LSTF9140
LSTF9150
LSTF9160
LSTF9170
LSTF9180
LSTF9190
LSTF9200
LSTF9210
LSTF9220
LSTF9230
LSTF9240
LSTF9250
LSTF9260
LSTF9270
LSTF9280
LSTF9290
LSTF9300
LSTF9310
LSTF9320
LSTF9330
LSTF9340
LSTF9350
LSTF9360
LSTF9370
LSTF9380
LSTF9390
LSTF9400
LSTF9410
LSTF9420
LSTF9430
LSTF9440
LSTF9450
LSTF9460
LSTF9470
LSTF9480
LSTF9490
LSTF9500
LSTF9510
LSTF9520
LSTF9530
LSTF9540
LSTF9550
LSTF9560
LSTF9570
LSTF9580
LSTF9590
LSTF9600
LSTF9610
LSTF9620
LSTF9630
LSTF9640
LSTF9650
LSTF9660
LSTF9670
LSTF9680
LSTF9690
LSTF9700
LSTF9710
LSTF9720
LSTF9730
LSTF9740
LSTF9750
LSTF9760
LSTF9770
LSTF9780
LSTF9790
LSTF9800
LSTF9810
LSTF9820
LSTF9830
LSTF9840
LSTF9850
LSTF9860
LSTF9870
LSTF9880
LSTF9890
LSTF9900
LSTF9910
LSTF9920
LSTF9930
LSTF9940
LSTF9950
LSTF9960
LSTF9970
LSTF9980
LSTF9990
LSTF1000
LSTF1001
LSTF1002
LSTF1003
LSTF1004
LSTF1005
LSTF1006
LSTF1007
LSTF1008
LSTF1009
LSTF1010
LSTF1011
LSTF1012
LSTF1013
LSTF1014
LSTF1015
LSTF1016
LSTF1017
LSTF1018
LSTF1019
LSTF1020
LSTF1021
LSTF1022
LSTF1023
LSTF1024
LSTF1025
LSTF1026
LSTF1027
LSTF1028
LSTF1029
LSTF1030
LSTF1031
LSTF1032
LSTF1033
LSTF1034
LSTF1035
LSTF1036
LSTF1037
LSTF1038
LSTF1039
LSTF1040
LSTF1041
LSTF1042
LSTF1043
LSTF1044
LSTF1045
LSTF1046
LSTF1047
LSTF1048
LSTF1049
LSTF1050
LSTF1051
LSTF1052
LSTF1053
LSTF1054
LSTF1055
LSTF1056
LSTF1057
LSTF1058
LSTF1059
LSTF1060
LSTF1061
LSTF1062
LSTF1063
LSTF1064
LSTF1065
LSTF1066
LSTF1067
LSTF1068
LSTF1069
LSTF1070
LSTF1071
LSTF1072
LSTF1073
LSTF1074
LSTF1075
LSTF1076
LSTF1077
LSTF1078
LSTF1079
LSTF1080
LSTF1081
LSTF1082
LSTF1083
LSTF1084
LSTF1085
LSTF1086
LSTF1087
LSTF1088
LSTF1089
LSTF1090
LSTF1091
LSTF1092
LSTF1093
LSTF1094
LSTF1095
LSTF1096
LSTF1097
LSTF1098
LSTF1099
LSTF1100
LSTF1101
LSTF1102
LSTF1103
LSTF1104
LSTF1105
LSTF1106
LSTF1107
LSTF1108
LSTF1109
LSTF1110
LSTF1111
LSTF1112
LSTF1113
LSTF1114
LSTF1115
LSTF1116
LSTF1117
LSTF1118
LSTF1119
LSTF1120
LSTF1121
LSTF1122
LSTF1123
LSTF1124
LSTF1125
LSTF1126
LSTF1127
LSTF1128
LSTF1129
LSTF1130
LSTF1131
LSTF1132
LSTF1133
LSTF1134
LSTF1135
LSTF1136
LSTF1137
LSTF1138
LSTF1139
LSTF1140
LSTF1141
LSTF1142
LSTF1143
LSTF1144
LSTF1145
LSTF1146
LSTF1147
LSTF1148
LSTF1149
LSTF1150
LSTF1151
LSTF1152
LSTF1153
LSTF1154
LSTF1155
LSTF1156
LSTF1157
LSTF1158
LSTF1159
LSTF1160
LSTF1161
LSTF1162
LSTF1163
LSTF1164
LSTF1165
LSTF1166
LSTF1167
LSTF1168
LSTF1169
LSTF1170
LSTF1171
LSTF1172
LSTF1173
LSTF1174
LSTF1175
LSTF1176
LSTF1177
LSTF1178
LSTF1179
LSTF1180
LSTF1181
LSTF1182
LSTF1183
LSTF1184
LSTF1185
LSTF1186
LSTF1187
LSTF1188
LSTF1189
LSTF1190
LSTF1191
LSTF1192
LSTF1193
LSTF1194
LSTF1195
LSTF1196
LSTF1197
LSTF1198
LSTF1199
LSTF1200
LSTF1201
LSTF1202
LSTF1203
LSTF1204
LSTF1205
LSTF1206
LSTF1207
LSTF1208
LSTF1209
LSTF1210
LSTF1211
LSTF1212
LSTF1213
LSTF1214
LSTF1215
LSTF1216
LSTF1217
LSTF1218
LSTF1219
LSTF1220
LSTF1221
LSTF1222
LSTF1223
LSTF1224
LSTF1225
LSTF1226
LSTF1227
LSTF1228
LSTF1229
LSTF1230
LSTF1231
LSTF1232
LSTF1233
LSTF1234
LSTF1235
LSTF1236
LSTF1237
LSTF1238
LSTF1239
LSTF1240
LSTF1241
LSTF1242
LSTF1243
LSTF1244
LSTF1245
LSTF1246
LSTF1247
LSTF1248
LSTF1249
LSTF1250
LSTF1251
LSTF1252
LSTF1253
LSTF1254
LSTF1255
LSTF1256
LSTF1257
LSTF1258
LSTF1259
LSTF1260
LSTF1261
LSTF1262
LSTF1263
LSTF1264
LSTF1265
LSTF1266
LSTF1267
LSTF1268
LSTF1269
LSTF1270
LSTF1271
LSTF1272
LSTF1273
LSTF1274
LSTF1275
LSTF1276
LSTF1277
LSTF1278
LSTF1279
LSTF1280
LSTF1281
LSTF1282
LSTF1283
LSTF1284
LSTF1285
LSTF1286
LSTF1287
LSTF1288
LSTF1289
LSTF1290
LSTF1291
LSTF1292
LSTF1293
LSTF1294
LSTF1295
LSTF1296
LSTF1297
LSTF1298
LSTF1299
LSTF1300
LSTF1301
LSTF1302
LSTF1303
LSTF1304
LSTF1305
LSTF1306
LSTF1307
LSTF1308
LSTF1309
LSTF1310
LSTF1311
LSTF1312
LSTF1313
LSTF1314
LSTF1315
LSTF1316
LSTF1317
LSTF1318
LSTF1319
LSTF1320
LSTF1321
LSTF1322
LSTF1323
LSTF1324
LSTF1325
LSTF1326
LSTF1327
LSTF1328
LSTF1329
LSTF1330
LSTF1331
LSTF1332
LSTF1333
LSTF1334
LSTF1335
LSTF1336
LSTF1337
LSTF1338
LSTF1339
LSTF1340
LSTF1341
LSTF1342
LSTF1343
LSTF1344
LSTF1345
LSTF1346
LSTF1347
LSTF1348
LSTF1349
LSTF1350
LSTF1351
LSTF1352
LSTF1353
LSTF1354
LSTF1355
LSTF1356
LSTF1357
LSTF1358
LSTF1359
LSTF1360
LSTF1361
LSTF1362
LSTF1363
LSTF1364
LSTF1365
LSTF1366
LSTF1367
LSTF1368
LSTF1369
LSTF1370
LSTF1371
LSTF1372
LSTF1373
LSTF1374
LSTF1375
LSTF1376
LSTF1377
LSTF1378
LSTF1379
LSTF1380
LSTF1381
LSTF1382
LSTF1383
LSTF1384
LSTF1385
LSTF1386
LSTF1387
LSTF1388
LSTF1389
LSTF1390
LSTF1391
LSTF1392
LSTF1393
LSTF1394
LSTF1395
LSTF1396
LSTF1397
LSTF1398
LSTF1399
LSTF1400
LSTF1401
LSTF1402
LSTF1403
LSTF1404
LSTF1405
LSTF1406
LSTF1407
LSTF1408
LSTF1409
LSTF1410
LSTF1411
LSTF1412
LSTF1413
LSTF1414
LSTF1415
LSTF1416
LSTF1417
LSTF1418
LSTF1419
LSTF1420
LSTF1421
LSTF1422
LSTF1423
LSTF1424
LSTF1425
LSTF1426
LSTF1427
LSTF1428
LSTF1429
LSTF1430
LSTF1431
LSTF1432
LSTF1433
LSTF1434
LSTF1435
LSTF1436
LSTF1437
LSTF1438
LSTF1439
LSTF1440
LSTF1441
LSTF1442
LSTF1443
LSTF1444
LSTF1445
LSTF1446
LSTF1447
LSTF1448
LSTF1449
LSTF1450
LSTF1451
LSTF1452
LSTF1453
LSTF1454
LSTF1455
LSTF1456
LSTF1457
LSTF1458
LSTF1459
LSTF1460
LSTF1461
LSTF1462
LSTF1463
LSTF1464
LSTF1465
LSTF1466
LSTF1467
LSTF1468
LSTF1469
LSTF1470
LSTF1471
LSTF1472
LSTF1473
LSTF1474
LSTF1475
LSTF1476
LSTF1477
LSTF1478
LSTF1479
LSTF1480
LSTF1481
LSTF1482
LSTF1483
LSTF1484
LSTF1485
LSTF1486
LSTF1487
LSTF1488
LSTF1489
LSTF1490
LSTF1491
LSTF1492
LSTF1493
LSTF1494
LSTF1495
LSTF1496
LSTF1497
LSTF1498
LSTF1499
LSTF1500
LSTF1501
LSTF1502
LSTF1503
LSTF1504
LSTF1505
LSTF1506
LSTF1507
LSTF1508
LSTF1509
LSTF1510
LSTF1511
LSTF1512
LSTF1513
LSTF1514
LSTF1515
LSTF1516
LSTF1517
LSTF1518
LSTF1519
LSTF1520
LSTF1521
LSTF1522
LSTF1523
LSTF1524
LSTF1525
LSTF1526
LSTF1527
LSTF1528
LSTF1529
LSTF1530
LSTF1531
LSTF1532
LSTF1533
LSTF1534
LSTF1535
LSTF1536
LSTF1537
LSTF1538
LSTF1539
LSTF1540
LSTF1541
LSTF1542
LSTF1543
LSTF1544
LSTF1545
LSTF1546
LSTF1547
LSTF1548
LSTF1549
LSTF1550
LSTF1551
LSTF1552
LSTF1553
LSTF1554
LSTF1555
LSTF1556
LSTF1557
LSTF1558
LSTF1559
LSTF1560
LSTF1561
LSTF1562
LSTF1563
LSTF1564
LSTF1565
LSTF1566
LSTF1567
LSTF1568
LSTF1569
LSTF1570
LSTF1571
LSTF1572
LSTF1573
LSTF1574
LSTF1575
LSTF1576
LSTF1577
LSTF1578
LSTF1579
LSTF1580
LSTF1581
LSTF1582
LSTF1583
LSTF1584
LSTF1585
LSTF1586
LSTF1587
LSTF1588
LSTF1589
LSTF1590
LSTF1591
LSTF1592
LSTF1593
LSTF1594
LSTF1595
LSTF1596
LSTF1597
LSTF1598
LSTF1599
LSTF1600

```

U.S. DEPT. OF COMM. BIBLIOGRAPHIC DATA SHEET	1. PUBLICATION OR REPORT NO. NBS TN-854	2. Gov't Accession No.	3. Recipient's Accession No.
4. TITLE AND SUBTITLE A System of Fortran IV Computer Programs for Crystal Structure Computations		5. Publication Date February 1975	
		6. Performing Organization Code	
7. AUTHOR(S) Larry W. Finger and E. Prince		8. Performing Organ. Report No.	
9. PERFORMING ORGANIZATION NAME AND ADDRESS NATIONAL BUREAU OF STANDARDS DEPARTMENT OF COMMERCE WASHINGTON, D.C. 20234		10. Project/Task/Work Unit No.	
		11. Contract/Grant No.	
12. Sponsoring Organization Name and Complete Address (Street, City, State, ZIP) Same		13. Type of Report & Period Covered	
		14. Sponsoring Agency Code	
15. SUPPLEMENTARY NOTES			
16. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here.) This report gives detailed descriptions and instructions for use of a system of programs for crystallographic calculations, including least-squares refinement with generalized systems of constraints, calculation of bond distances and angles with errors, Fourier synthesis, plotting of contours in Fourier maps, and preparation of structure factor tables for publication.			
17. KEY WORDS (six to twelve entries; alphabetical order; capitalize only the first letter of the first key word unless a proper name; separated by semicolons) Computer programs; contour plotting; constrained refinement; crystallographic calculations; Fourier section; Fourier synthesis; least squares.			
18. AVAILABILITY ☒ Unlimited ☐ For Official Distribution. Do Not Release to NTIS ☒ Order From Sup. of Doc., U.S. Government Printing Office Washington, D.C. 20402, <u>SD Cat. No. C13. 46:854</u> ☐ Order From National Technical Information Service (NTIS) Springfield, Virginia 22151		19. SECURITY CLASS (THIS REPORT) UNCLASSIFIED	21. NO. OF PAGES 133
		20. SECURITY CLASS (THIS PAGE) UNCLASSIFIED	22. Price \$2.00

NBS TECHNICAL PUBLICATIONS

PERIODICALS

JOURNAL OF RESEARCH reports National Bureau of Standards research and development in physics, mathematics, and chemistry. It is published in two sections, available separately:

• Physics and Chemistry (Section A)

Papers of interest primarily to scientists working in these fields. This section covers a broad range of physical and chemical research, with major emphasis on standards of physical measurement, fundamental constants, and properties of matter. Issued six times a year. Annual subscription: Domestic, \$17.00; Foreign, \$21.25.

• Mathematical Sciences (Section B)

Studies and compilations designed mainly for the mathematician and theoretical physicist. Topics in mathematical statistics, theory of experiment design, numerical analysis, theoretical physics and chemistry, logical design and programming of computers and computer systems. Short numerical tables. Issued quarterly. Annual subscription: Domestic, \$9.00; Foreign, \$11.25.

DIMENSIONS/NBS (formerly Technical News Bulletin)—This monthly magazine is published to inform scientists, engineers, businessmen, industry, teachers, students, and consumers of the latest advances in science and technology, with primary emphasis on the work at NBS. The magazine highlights and reviews such issues as energy research, fire protection, building technology, metric conversion, pollution abatement, health and safety, and consumer product performance. In addition, it reports the results of Bureau programs in measurement standards and techniques, properties of matter and materials, engineering standards and services, instrumentation, and automatic data processing.

Annual subscription: Domestic, \$9.45; Foreign, \$11.85.

NONPERIODICALS

Monographs—Major contributions to the technical literature on various subjects related to the Bureau's scientific and technical activities.

Handbooks—Recommended codes of engineering and industrial practice (including safety codes) developed in cooperation with interested industries, professional organizations, and regulatory bodies.

Special Publications—Include proceedings of conferences sponsored by NBS, NBS annual reports, and other special publications appropriate to this grouping such as wall charts, pocket cards, and bibliographies.

Applied Mathematics Series—Mathematical tables, manuals, and studies of special interest to physicists, engineers, chemists, biologists, mathematicians, computer programmers, and others engaged in scientific and technical work.

National Standard Reference Data Series—Provides quantitative data on the physical and chemical properties of materials, compiled from the world's literature and critically evaluated. Developed under a world-wide

program coordinated by NBS. Program under authority of National Standard Data Act (Public Law 90-396).

NOTE: At present the principal publication outlet for these data is the Journal of Physical and Chemical Reference Data (JPCRD) published quarterly for NBS by the American Chemical Society (ACS) and the American Institute of Physics (AIP). Subscriptions, reprints, and supplements available from ACS, 1155 Sixteenth St. N. W., Wash. D.C. 20056.

Building Science Series—Disseminates technical information developed at the Bureau on building materials, components, systems, and whole structures. The series presents research results, test methods, and performance criteria related to the structural and environmental functions and the durability and safety characteristics of building elements and systems.

Technical Notes—Studies or reports which are complete in themselves but restrictive in their treatment of a subject. Analogous to monographs but not so comprehensive in scope or definitive in treatment of the subject area. Often serve as a vehicle for final reports of work performed at NBS under the sponsorship of other government agencies.

Voluntary Product Standards—Developed under procedures published by the Department of Commerce in Part 10, Title 15, of the Code of Federal Regulations. The purpose of the standards is to establish nationally recognized requirements for products, and to provide all concerned interests with a basis for common understanding of the characteristics of the products. NBS administers this program as a supplement to the activities of the private sector standardizing organizations.

Federal Information Processing Standards Publications (FIPS PUBS)—Publications in this series collectively constitute the Federal Information Processing Standards Register. Register serves as the official source of information in the Federal Government regarding standards issued by NBS pursuant to the Federal Property and Administrative Services Act of 1949 as amended, Public Law 89-306 (79 Stat. 1127), and as implemented by Executive Order 11717 (38 FR 12315, dated May 11, 1973) and Part 6 of Title 15 CFR (Code of Federal Regulations).

Consumer Information Series—Practical information, based on NBS research and experience, covering areas of interest to the consumer. Easily understandable language and illustrations provide useful background knowledge for shopping in today's technological marketplace.

NBS Interagency Reports (NBSIR)—A special series of interim or final reports on work performed by NBS for outside sponsors (both government and non-government). In general, initial distribution is handled by the sponsor; public distribution is by the National Technical Information Service (Springfield, Va. 22161) in paper copy or microfiche form.

Order NBS publications (except NBSIR's and Bibliographic Subscription Services) from: Superintendent of Documents, Government Printing Office, Washington, D.C. 20402.

BIBLIOGRAPHIC SUBSCRIPTION SERVICES

The following current-awareness and literature-survey bibliographies are issued periodically by the Bureau: Cryogenic Data Center Current Awareness Service

A literature survey issued weekly. Annual subscription: Domestic, \$20.00; foreign, \$25.00.

Liquefied Natural Gas. A literature survey issued quarterly. Annual subscription: \$20.00.

Superconducting Devices and Materials. A literature

survey issued quarterly. Annual subscription: \$20.00. Send subscription orders and remittances for the preceding bibliographic services to National Technical Information Service, Springfield, Va. 22161.

Electromagnetic Metrology Current Awareness Service Issued monthly. Annual subscription: \$100.00 (Special rates for multi-subscriptions). Send subscription order and remittance to Electromagnetics Division, National Bureau of Standards, Boulder, Colo. 80302.

U.S. DEPARTMENT OF COMMERCE
National Bureau of Standards
Washington, D.C. 20234

OFFICIAL BUSINESS

Penalty for Private Use, \$300

POSTAGE AND FEES PAID
U.S. DEPARTMENT OF COMMERCE
COM-215

THIRD CLASS MAIL

