

# U.S. DEPARTMENT OF COMMERCE / National Bureau of Standards



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# Physical Properties Data for Rock Salt

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A. Monograph

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Library of Congress Cataloging in Publication Data Main entry under title:

Physical properties data for rock salt.

(National Bureau of Standards monograph; 167) Supt. of Docs. no.: C 13.44:167
1. Rock-salt—Handbooks, manuals, etc.
2. Radioactive waste disposal in the ground—Handbooks, manuals, etc. I. Gevantman, L. H. II. Series: United States. National Bureau of Standards
Monograph: 167
QC100.U556 no. 167 [TN900] 602'.18s

80-607096

National Bureau of Standards Monograph 167 Nat. Bur. Stand. (U.S.), Mono. 167, 288 pages (Jan. 1981) CODEN: NBSMA6

## U.S. GOVERNMENT PRINTING OFFICE WASHINGTON: 1981

For sale by the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402 Price \$12. (Buckram) (Add 25 percent for other than U.S. mailing)

# Preface

The Office of Standard Reference Data of the National Bureau of Standards is responsible for a broad-based program to provide reliable physical and chemical reference data to the U.S. technical community. Under this program a number of data evaluation centers both at NBS and at universities and other private institutions are supported and coordinated; these activities are collectively known as the National Standard Reference Data System (NSRDS). Important areas of the physical sciences are covered systematically by NSRDS data centers, and data bases with broad utility are prepared and disseminated. These centers can also take on special compilations of data addressing specific applications such as those frequently required by other Federal Agencies in carrying out their mission responsibilities. The existence of an ongoing program permits the collection of data for these special compilations to be carried out in an efficient and timely manner.

This Monograph on Properties of Rock Salt was prepared by the Office of Standard Reference Data in response to needs of the Department of Energy for reliable data in connection with nuclear waste disposal. The resources and experience of several NSRDS data centers were enlisted to produce a compilation of the various relevant properties of rock salt. We hope that the Monograph will be a useful source of reference data and serve as a model for other compilations of data required by Government agencies and private institutions.

> David R. Lide, Jr., Chief Office of Standard Reference Data

# Acknowledgement

I wish to acknowledge the sponsorship and financial support of the Office of Nuclear Waste Isolation and to thank Dr. G. Raines for his sound advice and support. I also appreciate the individual efforts of Drs. W. C. McClain and J. E. Russell, formerly of that office, for their encouragement and support during the execution of this project. I also wish to thank the individual authors for their technical contributions and Drs. Y. S. Touloukian, G. J. Janz, and J. L. Haas, Jr., for their aid and cooperation in making available the facilities of their individual data centers to the authors. The efforts of Dr. D. Isherwood and her colleagues who served as technical reviewers are gratefully acknowledged. Finally, I deeply appreciate the assistance of Mrs. M. E. Schlager, of the Office of Standard Reference Data, who helped me with all of the many tasks leading to the publication of this Monograph.

L. H. Gevantman

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# **Physical Properties Data for Rock Salt**

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Office of Standard Reference Data, National Bureau of Standards, Washington, D.C. 20234

Rock salt and pure sodium chloride properties data are assembled into a single source. The properties covered include geological, mechanical, optical, thermal, radiation damage, electrical, magnetic, chemical, and physical. A concerted attempt has been made to present the best data consistent with their availability in the literature. Recommended values for data are given where possible. A brief discussion of measurement techniques is included for each property.

Key words: Chemical; electrical; geological; monograph; magnetic; mechanical; optical; physical; properties data; radiation damage; rock salt; sodium chloride.

## Introduction

This effort was begun at the direction of the Office of Waste Isolation (OWI), Oak Ridge National Laboratory, Department of Energy,\* to answer a pressing need for a single source of data on rock salt properties. This need arose from the possibility that rock salt deposits provide an acceptable medium for the permanent storage of high level radioactive wastes. While a considerable body of data exists in the literature [references 1, 2, 3, and 4] on the physical properties of rock salt, it is not readily available in a single, easily identified source. Nor are the data in a form that permits designers of waste burial facilities to extract the variety of numerical values for use with any degree of confidence in these values. As a consequence, the Office of Standard Reference Data (OSRD) was asked to undertake a data evaluation project which would produce a data book on rock salt properties. These data also were to be evaluated, wherever possible, for reliability consistent with the measurement state-ofthe-art.

While the principal reasons for assembling this Monograph are nuclear-waste-storage inspired, the data for most of the properties cited would also apply to the burial of other types of waste where long-term stable facilities are required. It is intended that the data will serve as a source of generalized information to the salt industry. No attempt is made to argue the advantages or disadvantages for burial of nuclear wastes in rock salt formations. Such discussions are available elsewhere [references 5, 6, and 7].

## History of the Project

In organizing and defining the scope of this project the Office of Standard Reference Data recognized the need for two types of input. One was the viewpoints and criteria for information as represented by the sponsor. The second was the need for expertise in data assembly and evaluation, particularly the specific properties of interest. It was therefore the Office's role to bring these functions together to implement the project. In the first instance, the OSRD was fortunate in having excellent representation and advice from the Office of Nuclear Waste Isolation, which furnished an outline of the properties desired. After some consultation the OSRD was able to identify and designate three data centersthe Center for Information and Numerical Data Analysis and Synthesis (CINDAS), the Molten Salts Data Center, and the National Center for Thermodynamic Data of Minerals-to evaluate the data. An ad hoc committee, consisting of representatives from the Office of Standard Reference Data, the Office of Nuclear Waste Isolation, and each of the data center designates, met and reviewed the outline of the physical properties data to be contained in the Monograph. After some minor changes, work assignments based on the final version of the outline were distributed, and the work got under way. The OSRD assumed full responsibility for coordinating the efforts and for assembling and publishing the final product.

### Monograph Organization

The Monograph is in six chapters covering the geological, mechnical, optical, thermal, radiation damage, electrical, magnetic, chemical, and physical properties of rock salt and pure NaCl. Each chapter has been written by a different author, or authors, consistent with

<sup>\*</sup>This project was funded in part by the Office of Waste Isolation, Oak Ridge National Laboratory, Department of Energy.

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his field of expertise. Some attempt at uniformity of presentation has been made not only in the order of presentation of the data but also in content. In some instances exchanges of data among data centers have taken place so that the data given in one chapter also represent the efforts of other center contributors.

In general, each chapter attempts to present the best data available on the subject property in both tabular and graphic form. Wherever possible, recommended values and error limits are given. If this is not possible because the data are in disarray or are insufficient for subject judgment, a full review of the useful data and a rationale for working with the data are presented. Experimental methods for data measurement are given in brief form with precision limits on the measurement capability where possible. Brief reviews of error analysis are also included where applicable. In sum, every aspect of the particular property has been compiled, evaluated, and recorded when the data are available from the literature. The lack of a recommended value means the data are either lacking or too imprecise to permit evaluation. Nevertheless it is felt that a useful attempt has been made to present the better data now available in a single source.

As in all publications of this type, errors and omissions of one kind or another are bound to occur. Corrections and additions to the data by readers are solicited.

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# Chapter 1

# Geology, Mineralogy, and Some Geophysical and Geochemical Properties of Salt Deposits

John Lorenz\*, John L. Haas, Jr.\*, Michael A. Clynne\*\*, Robert W. Potter, II\*\*, and Constance M. Schafer\*

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# **1.1. General Introduction**

Rock salt is a coarsely crystalline, sedimentary rock containing massive, fibrous, or granular aggregates. Rock salt occurs in extensive beds, or in domes and plugs. Rock salt is the result of evaporation of saline water and is a member of a suite of related rocks, the evaporite series. Rock salt is dominantly halite, but other minerals are present such as calcite, dolomite, anhydrite, gypsum, and potash minerals. (Potash is an industrial term for the complex potassium and magnesium evaporites. A more complete list of minerals commonly found in evaporite deposits is given in chapter 2.) These minerals may be deposited contemporaneously in adjacent parts of a basin. The mineralogy is dependent on variations in topography, water depth, salinity, and other factors. Because these factors can change during geologically short periods of time, beds of different evaporite minerals overlie and overlap each other in sequences reflecting the changes in equilibrium that occur locally during the subsidence and sedimentary filling of basins.

Given the right conditions, halite can be the dominant mineral that accumulates. Halite, the chloride of sodium (NaCl), can form rare, pure beds as much as 80 meters thick. Once deposited and buried by succeeding layers of sediments, halite and associated minerals are susceptible to a variety of changes brought about by the effects of the elevated temperatures and pressures that are found at depths. Beside actual changes in mineralogy of the accessory minerals, the most dramatic changes are due to the lowered viscosity of halite and the increased contrast between its density and that of the surrounding sediments. Deeply buried salt commonly forms diapirs (domes or anticlinal folds, the overlying rocks of which have been bent or ruptured by the squeezing out of the plastic core) 1-6 kilometers in diameter by flowing plastically from original bedding horizons up thousands of meters through the sediments and sometimes to the surface.

Some of the characteristics of rock salt deposits change when the rock salt flows into domes. Domes contain generally purer halite, and rock salts in domes lose most of their primary sedimentary structures. Fluid inclusions in domed rock salt are more apt to contain foreign substances, such as oil. Other characteristics of rock salt, specifically porosity and permeability, do not necessarily change on intrusion. Both porosity and permeability are minimal in bedded and diapiric rock salt deposits. Salt domes are discussed more fully in section 1.3 below.

Thick halite and associated evaporite deposits are found in four large sedimentary basins in the United States (figure 1.1). Several smaller deposits exist, and the major deposits themselves can be subdivided by age and stratigraphy. Primary sedimentary thickness of the deposits ranges from some 1300 to 1400 m in the Ochoan evaporite sequence of Permian age (see Appendix 1.1 for geologic time scale) [1] in the Delaware basin of Texas and New Mexico [2] to surficial veneers now being deposited in the playa lakes of the western States. Diapiric rock salt is found only in the Gulf Coast area, though secondary thickening at the crests of anticlines has been described in the Paradox basin in Utah.

# 1.2. Bedded Deposits

# 1.2.1. Introduction

Ionic ratios suggest that most salt deposits were originally derived from evaporated sea water. Average sea water contains 38,450 ppm (parts per million) dissolved solids, of which about three quarters will precipitate as halite on evaporation. The evaporation rate of water is a function of the temperature of both the air and the water and of such things as the turbulence of the water surface. The rate of evaporation decreases as salinity of the remaining brine increases. In addition, Kinsman [3] has indicated that, for the precipitation of halite, the relative humidity must be less than 76 percent and, for the potash minerals, less than 67 percent. Most ancient evaporite deposits are formed in warm and arid climates. Another common feature of rock salt deposits is that they contain very little silt, sand, or other coarse, granular sediment; apparently only small amounts of these sediments were supplied to the basin during the evaporation of the brine. Such impurities as are found





are usually clay sized and are rarely larger than silt. The rate of supply of the fine-grained debris relative to the rate of accumulation of the chemical precipitates is also low for the beds of rock salt.

## 1.2.2. Depositional Models

Probably the most widely accepted theory to explain formations of bedded rock salt has been the "bar theory" originally proposed by Ochsenius [4]. This model in its simplest form hypothesizes an arm of the sea in which circulation is restricted (by a bar, ridge, or reef across the mouth); water in the arm is concurrently evaporated and replenished, and its dissolved salt is precipitated into basin-wide beds (figure 1.2). A large number of observed primary sedimentary structures in evaporites may be explained by this model: clay-filled desiccation cracks, ripple marks, and crossbedding in halite [5]; the presence of preferentially oriented hopper crystals [6]; dissolution horizons, unconformities, and halite conglomerates [7]; and cyclic deposition.

A variation on this model that has gained many adherents is Scruton's hypothesis [8] of constant water volume in a basin and reflux of final-stage brines to the sea (figure 1.3). This theory, which may have a modern analog in the Gulf of Kara Bogaz off the Caspian Sea, involves a subsea-level restriction that allows partial circulation in and out of the basin. The sea adds water over the restriction as it is evaporated from the basin. This restricted addition of sea water creates a salinity gradient; the water in the basin becomes progressively concentrated away from the sea and precipitates its various components in a lateral continuum of minerals. The final-stage brines either precipitate their contents at the far end of the basin or are cycled back out of the basin along the sea floor. This theory accounts for the large-scale lateral facies variations seen in many evaporite deposits.

Other theories have been formulated in attempts to explain characteristics of one or more salt deposits [9,10]. A model of separate basins attempted to account for some observed monomineralic accumulations of limestone, gypsum, and halite. Various theories about nonmarine or semimarine desert basins attempted to explain the lack of fossils in some salt deposits; at the other extreme, theories of subaqueous deposition from dense, deep-sea brines [11,12] were suggested to explain the apparent correlations between unfossiliferous deposits and their topographically low setting. The uniform and laterally extensive character of some bedding in salt deposits might also be explained by variations of these models of subaqueous deposition. The most recently proposed theory is based on the discovery of salt deposits flooring the Mediterranean Sea. Labeled "the theory of desiccating deep basins" by Hsü [9], it involves episodic cutoff and desiccation of large bodies of water such as the Mediterranean Sea or the Gulf of Mexico and evaporite deposition in the remnant salt lakes. Kirkland and Evans [13] assembled a collection of papers dealing with the origin of marine evaporites.

## 1.2.3. The Precipitation Sequence Predicted from Sea Water

Usiglio [14] in 1849 studied the precipitation sequence from evaporating sea water experimentally. His and other experimentally determined proportions of minerals from a fixed volume of sea water do not correspond well with those found in typical rock salt deposits (figure 1.4 and table 1.1), but several theories account for the discrepancies. If Scruton's reflux model is accepted, then the sea water need not be evaporated completely and the components of certain minerals may be retained in solution even though the preceding mineral in the series is extensively precipitated. The more soluble a mineral is, the less likely it is to be precipitated and preserved. The abundance of an individual evaporite mineral in the entire sedimentary rock record is inversely proportional to its solubility.

Another reason for the difference between observed sequences and the ideal sequence described by Borchert and Muir [15] is that the ideal sequence was precipitated at a constant temperature.

A discrepancy present in actual deposits that have reached the potash phase of deposition is the deficiency of sulfate minerals with respect to the ideal sequence. This deficiency is most often said to result from the destruction of sulfate minerals by sulfate-reducing anaerobic bacteria that derive their oxygen from the  $SO_4^{2^-}$  ion [16].

The mineral bischofite, which composes a sizeable part of the ideal precipitation sequence, is rarely found in the geologic record. The end brines containing this mineral are hydroscopic; that is, they are stable, resist evaporation, and usually find their way back to the sea.

#### 1.2.4. Cyclic Sedimentation

Jones [17] described bedded-sediment cycles in the Salado Formation of New Mexico that approximate Usiglio's predicted sequence [14]. The cycles are represented by beds 0.7 to 10 m thick; basal "clastic stratum" (green, brown clays) grades up into a "sulfate" (usually anhydrite) then to a "halite," and finally to a mixed "halite-clastic stratum." Similar cycles described



FIGURE 1.2. Ochsenius' bar theory [4] of rock-salt deposition as illustrated by Hsü [142].



FIGURE 1.3. Scruton's reflux hypothesis [143]—restricted marine basin showing stratigraphic sequence precipitated during lateral increase of brine salinity. Final stage brines may precipitate their contents at the shore end of the basin or may flow back to the sea along the basin floor. Modified from [143].

for the Hutchinson Salt Member of the Wellington Formation in Kansas [18] contain very thin carbonate beds above the basal shales. The basal clays in such cycles are often interpreted as resulting from solution lags caused by new influxes of fresh water that redissolve some of the clay-rich rock salt and set the precipitation sequence back to the anhydrite/gypsum phase.

Cyclic layering is common in Gulf Coast salt domes, where 2.4 to 25 cm-thick layers of anhydritic halite alternate with layers of pure halite, but these layers are not necessarily of depositional origin. The Castile Formation of southeast New Mexico also contains cyclic banding of calcite rich in organic matter alternating with pure anhydrite layers on a very small scale. These layers can be correlated for many kilometers across the Delaware basin [19] and may represent seasonal variations in climate during the Permian age.

#### 1.2.5. Diagenesis and Metamorphism

## 1.2.5.1. Introduction

In this book, no distinction is made between "diagenesis" and "metamorphism." The Glossary of Geology [20, p. 192, 446] defines the terms as follows:

"diagenesis [sedimentary] All the chemical, physical, and biologic changes, modifications, or transformations undergone by a sediment after its initial deposition (i.e., after it has reached its final resting place in the current cycle of erosion, transportation, and deposition), and during and after its lithification, exclusive of surficial alteration (weathering) and metamorphism.\*\*\*"

"metamorphism The mineralogical and structural adjustment of solid rocks to physical and chemical conditions which have been imposed at depth below the



FIGURE 1.4. Proportions of minerals experimentally precipitated from sea water compared with those found in natural rock-salt deposits. Modified from [144].

Table 1.1 Minerals that Precipitate from Increasing Brine Concentrations at Constant Temperature. Modified from [123]

Dominant mineral precipitating at concentration	Brine concentration (multiples of sea-water concentration)
Limestone/dolomite	1-4
Gypsum	4 - 1 2
Halite	12-64
Mg and K salts (potash minerals)	64-120
Bischofite	120-240

is the dihydrate of calcium sulfate that usually forms as a primary precipitate, but anhydrite, its dewatered equivalent, is the mineral most common in the rock record. Minerals of the potash phase are rarely found in their primary states. Some potash minerals do not form except after burial. Evidences for changes in evaporite deposits are the presence of minerals that do not form at normal surface temperature, abrupt lateral mineralogy changes, and irregular trace-element profiles (especially the profile for bromine). Braitsch [21] listed three types of change—dynamic, thermal, and solution—and classified them as metamorphic processes.

#### 1.2.5.2. Dynamic Metamorphism

surface zones of weathering and cementation, and which differ from the conditions under which the rocks in question originated\*\*\*."

In an evaporite deposit, the distinction between diagenesis and metamorphism would be arbitrary at best because the contained minerals are responsive to small changes in temperature and pressure above the ambient conditions for deposition. Some changes that are considered metamorphic take place before others that are considered diagenetic.

The minerals most susceptible to change are those precipitated from the most concentrated brines. Gypsum

Dynamic metamorphism is the simplest type of metamorphism and the one that most readily affects the mineral halite. Braitsch [21] described it as the mechanical plastic deformation of salts under low stress and the associated isochemical and isophase recrystallization. Kupfer [22] indicated that the segregation of anhydrite from halite in salt domes probably took place during this type of deformation. Effects of dynamic metamorphism include (1) textures characterized by large, uniformly oriented crystals and (2) the folding of original bedding. It is caused by overburden pressures and tectonic stresses that produce movement of the rock salt.

#### 1.2.5.3. Thermal Metamorphism (Including Load Metamorphism)

As sediments subside with a basin, they are subjected to the elevated temperatures and pressures associated with the temperature gradient of the earth's crust and the increased pressure of the overlying sediments. These temperatures and pressures dewater the loosely hydrated minerals in the early stages of burial. Dehydration of most evaporite minerals is easily accomplished and usually takes place at temperatures below  $100^{\circ}$ C [23]. The most important of these reactions is CaSO<sub>4</sub> · 2H<sub>2</sub>O = CaSO<sub>4</sub> + 2H<sub>2</sub>O, which occurs at depths of 100-175 m [24]. Carnallite (KCl · MgCl<sub>2</sub> · 6H<sub>2</sub>O) is often dewatered to produce sylvite KCl and a MgCl<sub>2</sub> brine. The brine liberated from these reactions is important in solution metamorphism as described below.

Thermal metamorphism also causes extensive recrystallization in monomineralic beds, specifically halite beds, though the resulting textures are not oriented as in dynamic recrystallization. In beds containing more than one primary mineral, the ionic components of minerals are mobile and new minerals are often formed at the expense of primary ones. This complex process is described by Braitsch [21].

#### 1.2.5.4. Solution Metamorphism

The dehydration of a cubic meter of gypsum produces slightly less than ½ cubic meter of water. During dehydration, a 10 m-thick bed of gypsum will decrease in thickness to a 6.2 m-thick bed of anhydrite [25]. Because gypsum is one of the first minerals to precipitate in the evaporation of sea water, most evaporite deposits include a thick basal anhydrite sequence that provided brines for solution metamorphism during the formation of the anhydrite. In certain other deposits, brines may have originated as magmatic or artesian ground waters [26].

The brines created by these processes flow through "tectonically created permeability" [27], dissolving the more soluble minerals and depositing less soluble minerals from solution. (Some of the mobility of the fluid may be due to this differential solubility of the host rock rather than to its actual permeability.) Dissolution and redeposition of the components available in the rock result in a continuously changing composition in the brines; the changes are directed towards the same end composition as that of end brines in an evaporation sequence [28].

The complex changes in mineralogy due to solution metamorphism are most important in potash deposits, where the secondary minerals are often more abundant than the primary precipitates. Variations in metamorphic mineralogy are due to changes in temperature and composition of the intruding fluids and intruded rocks. Brines can cause temporary cavities, brecciation, and collapse structures, as well as mineral changes. However, the brines quickly become saturated with respect to halite and anhydrite, and "further migration . . . can usually produce no further effects within a pure rock salt deposit" [29].

### 1.2.6. Regional Rock Salt Geology

Summary discussions of the rock salt deposits in the United States are given by Pierce and Rich [2] and by Johnson and Gonzales [30]. The reader is referred there for both further information and bibliographies on the stratigraphy of individual deposits. The variability of salt deposits is exemplified by the differences in the data supplied by Pierce and Rich for many of the basins; presumably the data are derived from different authors or different parts of a basin. However, much of the variability may be real. Variability in salt depositis can be a response to the shape of the basin, the topography within the basin, the rate of subsidence of the various parts of the basin, the location of freshwater or unsaturated marine water input, and the different rates of evaporation within the basin. Because rock salt has been significantly changed by various chemical and physical stresses after burial, studies of modern surficial evaporite deposits are not as applicable to an understanding of rock salt as studies of subsurface deposits that only can be obtained in situ from well logs and mines. We often only have a limited and localized knowledge of subsurface deposits.

Rock salt deposits range greatly in size. The most widespread deposits in the United States, excluding the probable extension of the Louann Salt of Jurassic age under the Gulf of Mexico, are the Permian evaporite sequences of Texas, New Mexico, Colorado, Oklahoma, and Kansas. Table 1.2 shows the correlation between geologic ages and time before the present. These deposits (figure 1.1) cover an area about 1000 km long, north to south, and about 240 to 320 km wide. They are subdivided by age and stratigraphy into at least five local basins [31]. In New Mexico and Texas, the salt-bearing Castile and Salado Formations, approximately 600 and 70 meters thick, respectively, are Late Permian in age and are found in the Delaware basin. The Salado Formation extends into the Midland basin. The approximately 250 m-thick Wellington Formation, best known in the Wellington basin of Kansas, is of early Permian age. These salt deposits are part of the same general depositional and tectonic province, called the Permian basin, but are loosely related products of

#### Table 1.2

#### GEOLOGIC TIME SCALE

Modified Subdivision in Use by the U.S. Geological Survey [1, p. 150] System or Era or Age Estimates Commonly Used for Erathem Period Boundaries (millions of years) Quaternary Cenozoic 1.8 Tertiary 65 Cretaceous 136 Mesozoic Jurassic 190-195 Triassic 225 Permian 280 Pennsylvanian 320 Mississippian 345 Paleozoic Devonian 395 Silurian 430-440 Ordovician 500 Cambrian 570 Proterozoic - 2,500 Archean

different localities in it and thin or wedge out between subdivisions of the basin.

The Silurian salt-bearing Salina Formation of Michigan, northern Ohio, Ontario, New York, Pennsylvania, and West Virginia covers a maximum linear distance of 880 km. The formation is a thin (0-100 m) blanket across most of Ohio, Pennsylvania, and West Virginia but thickens to 300 m in parts of New York and to 600 m in Michigan where the subsidence of the Appalachian and Michigan basins allowed thicker accumulations.

The Williston basin in North Dakota, Montana, and Saskatchewan is unique in that it had four episodes of rock-salt accumulation in the same geographic location (during Devonian, Mississippian, Permian, and Triassic time). In an area about 500 km long and 500 km wide, the salt-bearing formations range from 30 to 50 m in thickness, though they are buried deeply and are poorly known.

The Louann Salt and the associated formations of the United States Gulf Coast are also poorly known. Most oilwell drilling is terminated when the salt beds are reached so that estimates of thickness are highly speculative, ranging from 170 to 1700 m. The Louann Salt extends well into the Gulf of Mexico to the Sigsbee knolls, which are considered to be salt domes. Thus, it has great areal extent, despite an area in central Louisiana that may be salt free.

#### 1.2.7. The Variability within Salt Beds

The percentage of a given formation that is bedded rock salt ranges from 0 to 100 percent, though most deposits shown in figure 1.1 are less than 50 percent other minerals. The distribution of other minerals within a formation is irregular, reflecting depositional changes, subsequent metamorphism, and ground-water leaching.

The thickest individual monomineralic halite beds that might exist in a formation cannot be identified from the literature. Deciding the thickness and number of clay or anhydrite partings that must be in a rock salt bed before it is no longer considered to be halite is a subjecttive process. Pierce and Rich [32] stated: The normal bedded rock salt deposit is composed of a number of separate beds that have slight to large variations in composition. A forty-foot vertical section, selected at random in a salt sequence, might consist of:

	Feet	Inches
Salt	9	0
Anhydrite		2
Salt	7	6
Shale		2
Salt		6
Shale	2	0
Salt	12	0
Shale and anhydrite		8
Salt	8	<u>0</u>
Total	40	0

Some authors would tend to call the above section a pure halite bed if the 2 foot (0.6 m) shale break were thinner. Impurities in bedded rock salt may also be present as finely disseminated intracrystalline particles and blebs, especially of clay or anhydrite.

Gleaned from Pierce and Rich [2], the following are estimates of the maximum thicknesses of "pure" individual halite beds in some formations.

Thickness,
in meters
80
20
70
30
210
20
70
10
70
50
50

Average bed thickness ranges are well below 50 percent of the above-given maximum thicknesses. The Louann Salt of southern Louisian is perhaps one of the purer rock salt deposits, but it is poorly known. Andrews [33] described it as very white to grey, clear, coarsely crystalline and containing anhydrite streaks, and very pure without clastic material. The Hermosa Formation of Utah, on the other hand, is described by Pierce and Rich [34] as containing "many shale and anhydrite beds," despite its flowage into great accumulated thicknesses at anticline crests. Gross-scale composite sections of some salt-bearing formations in the United States are given by Lefond [35] and can be found in the Northern Ohio Geological Society Salt Symposia volumes.

# 1.3. Salt Domes 1.3.1. Introduction

Only the rock salt deposits of the Gulf Coast embayment have produced salt domes in the United States, though incipient doming is present in the Paradox basin salt deposits. More than 300 salt domes have been recognized, onshore and offshore, in Texas, Louisiana, and Mississippi.

These domes have risen from great depths. Their source, the bedded Louann Salt, is approximately 5000 m deep north of the area in central Louisiana that may be salt free. South of the area, the depth estimates range from 11,700 m to as much as 20,000 m, though the generally accepted figures are from 13,000 to 15,000 m. The domes rise above the source bed from local thickenings of the bed all the way up to present-day land surfaces. In the United States, the salt beds are not exposed at the surface; however, the locations of many domes are marked by solution and collapse that produced lakes. Some of the lakes contain central islands that may be the result of continued doming.

Domes may be circular to broadly elliptical, and their diameter may either increase or decrease downwards. Some domes may even have detached from their source bed. Domes commonly have a mushroom shape near the top, on any or all sides, termed "overhang" (figure 5). The average diameter at the top of Gulf Coast domes is about 3.2 km, though they range from 1 to 6 km in diameter [36a and b]. The upper surfaces may be flat, convex upward, or irregular and are usually but not always covered by "caprock."

#### 1.3.2. Formation

Salt-dome formation is related to the incompressible and plastic characteristics of salt. As shown by figure 1.6, halite has a greater density than clastic sediments at surface conditions. Pore spaces in forming rock salt are quickly filled by halite on recrystallization. In clastic sedimentary rocks, pore space is filled by water; only gradually is the water forced out and the pore space reduced by the increasing pressure of thickening overburden. The result is that the density of clastic rocks, usually sandstone and shale, increases as depth of burial increases whereas that of halite remains constant. At a depth from 130 m [37] to 700 m [38], the density of



FIGURE 1.5. Idealized stratigraphic cross section of upper part of an intermediate depth Gulf Coast salt dome.

salt equals that of average sedimentary rocks; below that, an unstable density inversion is present because denser clastic sediments overlie lighter rock salt. (The incipiently domed rock salt of the Paradox basin is covered by about 700 m of overburden, but the deep salts of the Williston basin are undomed.)

Added to this density inversion is the plasticity of halite, which increases as temperature and pressure increase. "At depths of between 2500 and 3000 meters, the temperature is about 100°C and the pressure over  $600 \text{ kg/cm}^2$  [58.84 MPa]. Under these conditions, salt is very plastic; it is in fact about as soft as butter on a hot summer's day" [39]. While this is an overstatement, it must be recognized that rock salt, alone among the common rock types, flows readily in response to small gradients in pressure and temperature.

Salt flows toward sedimentary and tectonic irregularities in the overburden. Folded strata are especially conducive to rock salt flowage because of the differential stresses. Salt accumulates at the crests of folds. The greater the depth of burial, the larger the local accumulation of rock salt, and the greater the tendency towards penetration of the overlying sediments. The mobility of rock salt is such that its original site of deposition may be as far as 25 km from the dome where it is presently found [41].

Salt flows to and within domes in pulses, not continuously. This pulsing flow is indicated by the different episodes of folding (refolded folds) found within domes and the irregular effects the rising dome has had on the adjacent stratigraphy (described below). Estimates of the actual rates of flow are on the order of a few millimeters per year [42]. In contrast with the Persian domes that are pushed up to some 1300 m above the surrounding plain and are still rising [43], most of the Gulf Coast domes seem currently to be in a state of equilibrium. Sediment deposition on top of them would probably remobilize them. Borchert and Muir [44] stated 'salt will normally continue to flow into the dome until the supply from the surrounding area is exhausted. So the height of the dome is largely governed by the thickness of the original bed of salt."

#### 1.3.3. Associated Structures

#### 1.3.3.1. Internal Structures

The internal structure of salt domes is visible in the contortions of the ubiquitous banding of pure halite and



Depin below solidce, moosands of feet

FIGURE 1.6. Density-depth relationship for Gulf Coast sediments and rock salt. Modified from Nettleton [145]

anhydritic halite. This layering is usually 0.025 to 0.25 m thick and is tacitly assumed to be the original sedimentary layering. The anhydrite rarely makes up more than 5 percent of the impure layers but gives them a distinctively darker coloration.

Folding of the bands in domes of northern Louisiana is relatively simple because of the short distance that they have risen, but the folding in southern Louisiana is complex. The overall pattern of folding is one of radially distributed vertical folds. Because the major vector of flow in domes is vertical, vertical cross-sections within the domes rarely show more than parallel near-vertical lineations. A horizontal section, however, shows complex ellipses and concentric and ptygmatic (disharmonic) folding. Shearing and attenuation of folds, in many places to elimination, are also common. Rare but more competent anhydrite bands may show boudinage, a set of regular extensional partings. All these folds have axes that are near vertical and are continuous vertically for as far as the exposure (usually a mining face) is available. Kupfer [45] stated "folding in domes is due to minor lateral drift of adjacent elements during vertical motion." As such, it is secondary in importance as a record of movement to the vertical lineations. The multiple episodes of refolding were probably caused by varying components of this lateral drift. Generally, the bedding is parallel to the side of the dome near the edges and becomes more complex inward.

Differential vertical movement within the dome produces "spines" of salt that rise higher than adjacent parts of the dome. Spines are usually cited as the cause of shear zones noted within salt domes. The structure in shear zones has been homogenized and looks deceptively simple, though pieces of the rock surrounding the dome are sometimes incorporated into these zones. Rare highangle and more common bedding-slip faulting may also be produced by spine movement [46].

#### 1.3.3.2. External Structures

The rock salt of the Louisiana domes is rimmed by an external shear zone called the "shale sheath." In the Weeks Mine, Louisiana, this sheath is a chaotic shale/salt mixture, 130-330 m thick. Sedimentary layers pierced by salt domes may be abruptly truncated against a dome-margin shear zone, but more commonly they are upturned or even overturned against the shale sheath.

Other adjacent sedimentary layers were directly created by the doming action. As rock salt was withdrawn from the beds peripheral to the dome, the overlying sediments subsided into a "rim syncline," while the central rocks were pushed upward by the dome. Sediments eroded from the central high were redeposited in the rim syncline, creating both a local unconformity over the top of the dome and adjacent sedimentary strata that dip away from the dome and pinch out against it. In other circumstances, a bed that was being deposited regionally concurrent with doming would be thinner over the dome. The local stratigraphy records the relationship between episodic growth of the dome and the regional deposition.

Two sets of faults in the overlying sediments are usually associated with domes: 1) tear faults radial to the dome and 2) tension faults tangential to the dome (figure 1.7). The latter often create a "central graben" over the center of the dome.

#### 1.3.3.3. Caprock

Some salt domes are covered by "caprock," a sequence of a basal, granular anhydrite, an intermediate layer of gypsum, and a covering of calcite (which in many places contains minable quantities of native sulfur). Hawkins and Jirik [118] noted that 181 of the some 330 known salt



FIGURE 1.7. Example of the fault pattern in sediments overlying a salt dome near Galveston County, Texas. Modified from [146].

domes along the Gulf Coast are known to have caprock and that it is usually thicker on domes that are closer to the surface. Uncapped domes are also known. The thickness of caprock ranges from less than 3 m to greater than 500 m and averages 130 m [47].

The origin of caprock is probably a combination of a solution lag of anhydrite, as the anhydrite-bearing rock salt of the dome intruded into the freshwater horizon [48], and an in-place alteration of the upper zones of that anhydrite to gypsum and calcite. Given the low percentage of anhydrite in dome rock salt, a large volume of the rock salt must have been dissolved in order to leave some of the thicker layers of caprock.

Arguments for the in-place origin of caprock are largely based on the presence of authigenic minerals not found within the dome rock salt and isotopic ratios indicating organic activity. The  $S^{34}/S^{32}$  ratios of the sulfur pockets found in the calcite are reflections of the preference of certain anaerobic bacteria for one of those isotopes [49] in their conversion of CaSO<sub>4</sub> to H<sub>2</sub>S and ultimately to S in order to obtain oxygen. These bacteria feed on the hydrocarbons associated with domes. The remaining Ca combines with CO<sub>2</sub>, also bacterially produced, to produce the top layer of calcite (which is enriched in C<sup>12</sup>, also indicative of an organic origin).

The general sequence of events in the formation of caprock is:

1. Solution lag of anhydrite (CaSO<sub>4</sub>).

2. Hydration of anhydrite to gypsum

 $(CaSO_4 + 2H_2O = CaSO_4 \cdot 2H_2O).$ 

3. Bacterial reduction of gypsum and methane (CH<sub>4</sub>) to produce  $H_2S$ ,  $CO_2$ , and  $Ca^{2+}$ .

4. Inorganic oxidation of  $H_2S$  to S, and combination of  $Ca^{2+}$  and  $CO_2$  to form calcite (CaCO<sub>3</sub>).

#### 1.3.4. Mineralogy

Gulf Coast salt dome deposits are generally more than 97 percent halite. The major impurity is anhydrite, which makes up from 1 to 10 percent of the darker beds [50, 51]. The bedding style is termed "graded" in that, above a sharp basal contact, the impure bed gradually grades to pure halite. More precise rock salt analyses and descriptions of crystal habit are given in section 1.4.

The mineralogy can change during diapirism (saltdome formation). Some evidence indicates that "differential purification may occur during diapirism" [52]. Halite-rich layers respond to stress and flow more readily than the less plastic impurities such as the anhydrite or clay layers. Though the Louann Salt is reported to be a relatively pure halite deposit, the domes formed from it probably contain even fewer impurities.

The rock salt in some domes in Louisiana is incompetent. Hand specimens tend to fall apart readily along crystal boundaries [53]. An inverse relationship between competency and the vertical distance of piercement may be present.

# 1.4. Mineralogy and Petrology 1.4.1. Introduction

Halite has a cubic crystal shape, but it may also be found in a massive, granular, or fibrous habit. It may break with perfect right-angle cleavage or, to a lesser extent, it may fracture conchoidally. Its hue, dependent on the amount and type of impurities, may be colorless, grey, white, or red. In certain instances, it is a deep blue. Summaries of the optical and physical properties of halite and other evaporite minerals have been published by Borchert and Muir [54] and by Braitsch [55]. They are also discussed in other chapters of this book.

#### 1.4.2. Impurities

Rock salt contains a variety of accessory or minor minerals. The accessory minerals in salt domes (the type of deposit that is most pure) are summarized in table 1.3. These minerals are also found in bedded deposits, where

.zziM , YjnuoJ ismel	××× ××		
ssxəT ,bnuoM zniizoH	×× ××× × ×		
Носкіеу, Техаз	*****		
.AJ ,bİəiìnniW	*****		×
.Al ,9ltzsD 9jiAW	****		trace X
.Al ,bnslel eY99W	*****		****
.AJ ,92in9V	×× ×		trace X X X
.AJ ,Tuhqin2	××× × × ×		××
.Ал ,гэйгг	××× ×		
.Al ,notgnidssW əásl	******		x x x
.АЛ ,93втітэН эйгд	××× ×		××
.AJ ,sgninnəl	×× ××		
.AJ ,.bI mozrəffəl	*****		****
.Ал , үяй . Ы пэртяд	** **		x
Еазт Наскьетгу, LA.	****		×
.Al , Worred	××× ×		trace X
.Ал., wstoodD	*****		× × × ×
.Al ,uslā uovaā	****		×
.AJ ,bnsIsI yıəvA	*****		****
.Al ,əttuä si əznA	****		trace X
Common Minerals (in order of abundance)	Anhydrite Dolomite Calcite Pyrite Quartz Limonite Hauerite Sulphur Hematite Celestite Barite Marcasite Kaolinite	Other inclusions	Potash salts Oil Gas Quartz sand

their volume and distribution range from 0 to 100 percent of a formation or sample and from thick intercalated beds to disseminated intercrystalline grains. Jones [18, p. A1] summarized the small-scale occurrence of impurities in rock salt beds of the Wellington Formation in Kansas as follows:

"Anhydrite and detrital argillaceous clay materials are the main accessory constituents of the rock and commonly form angular interstitial patches and irregular veinlike masses. Other minor constituents—such as polyhalite, dolomite, magnesite, hematite, celestite, marcasite, and pyrite—occur as single crystals or as groups of crystals that project into halite from the edges of argillaceous patches and from small lensic or veinlike masses of anhydrite. Small pseudomorphs after gypsum, outlined by crystals and fine-grained masses of anhydrite, are scattered irregularly through the rock."

Representative analyses of hand samples from United States salt domes are given in table 1.4.

To illustrate the typical composition of rock salt containing more impurities, Jones [18] gave the following breakdown for the entire Salado Formation of New Mexico: rock salt, 38.6 percent; clay-rich rock salt, 45.0 percent; sulfate rocks, 12.5 percent; and clastic rocks, 3.9 percent. These percentages vary across the basin, and the formation becomes principally anhydrite and dolomite on the southern edges. To the north, the percentage of clay, sand, and silt in the Salado Formation increases to dominance. Salt-percentage maps show that rock salt composes the greatest percentage of most saltbearing formations near the center of a basin.

Impurities in the Gulf Coast salt domes are very irregularly distributed, and the composition and grade of rock salt are often different in adjacent spines of a dome. The overall impurity percentage estimates vary between 1 and 2 percent for domes in southern Louisiana [56] and up to 15 percent for northern Louisiana and Texas [57].

The percentage of impurities also varies across the complete spectrum at the intermediate scale of the 30 cm- to 8-m-thick beds that make up bedded formations. As a rule, rock salt is purer in the upper parts of beds, especially the thicker ones. In the Salina Formation in New York, "halite makes up 85 to 95 percent of the laminated salt by weight" [58, p. 41]; in the same formation in northeastern Ohio, impurities (mostly dolomite and anhydrite) range from 0 to 30 percent, the percentage being greatest near contacts with beds of anhydrite [59]. In the Salado Formation of New Mexico, most salt beds contain from 1 to 10 percent impurities including anhydrite, polyhalite, and clay [60] as disseminated intercrystalline blebs. A composite sample of the Hutchinson Salt Member of the Wellington from Kansas yielded 5.7 percent insoluble material, mostly anhydrite [61].

## 1.4.3. Grain Size and Orientation

## 1.4.3.1. Bedded Deposits

The crystal size of halite in bedded deposits varies from a few millimeters to more than 0.1 m on a side. Most often the crystals of a bed are of roughly the same size, though gradations from a zone of one size to a zone of another size are common. Larger crystals tend to be found where fewer impurities are present to inhibit their growth during recrystallization.

Where rock salt has not been extensively recrystallized, hopper crystals may be preserved in bedded salt. These pyramidal, originally open-ended crystals, 0.005 to 0.01 m on a side, grow point down at the evaporation surface of a brine until their weight overcomes surface tension and they settle to the bottom [62]. In some instances, sheets of uniformly oriented hopper crystals are found in rock salt beds, indicating that they grew together at the surface and settled as a unit. These crystals often serve as nucleation sites for cubic crystals, which grow in crystallographic continuity during recrystallization or periods of supersaturation of brines at the bottom of the basin or both. Hopper crystals can be recognized by the abundant, minute fluid inclusions that outline successive growth planes of the crystal and show characteristic "chevron" patterns in thin section.

Another of the few remnant primary crystalline textures in salt deposits is that displayed by gypsum. Gypsum commonly grows as crystals attached to the basin floor, in a distinctive "swallow-tail" configuration, centimeters in length. This texture is commonly preserved even though the gypsum may be changed to anhydrite or replaced by other minerals (usually halite). The texture may be used to tell the "up" direction of a piece of core.

#### 1.4.3.2. Salt Domes

The size of halite crystals in salt domes usually ranges from 0.005 to 0.01 meters on a side, though some domes contain rare zones of finer grained crystals. More common "pods" of coarse grained crystals 0.025 to 0.05 meters on a side commonly cut across bedding and may be the result of resolution and deposition caused by ground-water intrusion [64]. These coarsely crystalline pods are often associated with water seepages, oil inclusions, and shear zones between spines.

Halite crystals elongated preferentially in the vertical direction, that is, parallel to the direction of flow, have been reported [41, 42, 51, 65]. The length ratios of vertical to horizontal axes are commonly about 1.5 and, in some crystals, are as much as 6.0. The elongation is thought to be caused by a combination of mechanical

0, compound found to be absent; tr, trace; 98.03, compound percentage; ---, compound listed but presumably absent; blank, compound not listed in original analysis, presumably not tested for

Compound		A	very Isla	nd Dome, L	Α		Jeffersc	n Island D	ome, LA	01d Hackberry Salt Dome, LA	Choctaw Dome, LA
NaCl	99.026	99.252	99.07	99.035	90.008	99.137	98.950	98.730	98.820	95.720	97.710
Moisture	0.019			0.009	0.012	0.012					0
Acid Insoluble			0			1	0.004	0.014			
Water Insoluble	0.711	0		0.686	0.718	0.642			0.032		
$CaSO_4$	0.225	0.694	0.18	0.227	0.223	0.166	1.032	1.192	1.129	3.950	2.140
CaC1 <sub>2</sub>	0.010	0.042	0	0.024	0.020	0.026			0.040	0.140	0
CaCO <sub>3</sub>		0	0	0	0	0	1 1 1	0.053		0	
MgC1 <sub>2</sub>	0.009	0.012	0.01	0.019	0.019	0.017	0.006	0.006	0.006	0.008	0
$MgSO_4$	0			0	0	0				1	0.036
Mg CO <sub>3</sub>		0	0								
Na $_2$ SO $_4$	0	0		0	0	0				1 1 1	0.046
$Na_2CO_3$		0									
KC1	0				1	1 I I				0	0.004
$Fe_2O_3$		0	0	0	0	0			tr	0.012	0.005
$R_{2}O_{3}$											
A1 203			0	1	k 1 1	1 5 1				i r 1	
SiO2							0.004	0.014	0.001	0.030	0.064
Total	100.000	100.000	99.26	100.000	100.000	100.000	966.66	100.009	100.028	99.860	100.005
Source of Data	[125]	[2]	[35]	[61]	[61]	[01]	[61]	[61]	[61]	[61]	[61]

	), compo presuma	und found bly abse	d to be al nt; blank,	sent; tr, compound	trace; 98.( not listed	)3, compou in origin	nd perce al analy	ntage; sis, pres	-, compound umably not t	listed but cested for	
Compound	B	elle Isla	and Dome,	LA	Winnfield Dome, LA	Weeks I	sland Dc	me, LA	Grand Dome,	Saline Texas	Bedded salt Natrium, VA
NaCl	92.75	96.41	92.750	96.405	97.23	97.920	99.10	98.923	98.883(1)	98,926(1)	96.440
Moisture						0.040	0.03	0.004			0.350
Acid Insoluble											
Water Insoluble	3.33	0.06	3.325	0.059	1.01	0.032			tr		1.070
caso <sub>4</sub>	0	3.05	0	3.053	1.65	1.930	0.81	0.941	1.099	1.041	1.600
CaC1 <sub>2</sub>	0	0.23	0	0.226	0.08						0.230
caco <sub>3</sub>	1.80	0	1.804	0	0				0.010	0.010	
MgC1 <sub>2</sub>	0	0.07	0	0.074	0				tr	4 1 1	)   
$MgSO_4$						0.020		0.003			1 1 1
Mg Co <sub>3</sub>	0.20	0	0.201	0	0				1		
Na <sub>2</sub> SO <sub>4</sub>			0.837	0					0.008	0.023	, , ,
Na <sub>2</sub> CO <sub>3</sub>			0.067	0					1 1 1	1	
KC1											0.310
Fe <sub>2</sub> 0 <sub>3</sub>						0.050	0.01	0.083			
R203	0.50	0.03	0.500	0.025	0.03				:	:	
A1 203											
SiO <sub>2</sub>											
Total	98.58	99.85	99.484	99.842	100.00	99.992	99.95	99.954	100.000	100.000	100.000
Source of Data	[35]	[32]	[2]	[2]	[35]	[61]	[61]	[61]	[65]	[65]	[125]

Compound	Bedde	ed Louann	Salt, Ala	bama	Bedded Haynesvil tion, A	salt of le Forma- Nlabama	Bedded Retsof	salt , NY	Bedded salt Watkins Glenn, NY	Bedde Detroit	ed salt Michigan
Na C1	92.08	95.93	86.20	99.55	76.10	08.66	98.262	98.249	99.835	98.050	98.181
Moisture							0.015	0.023	0.035	0.163	0.114
Acid Insoluble											
Water Insoluble		1	9.17	0.10	22.80	0.30	0.962	1.227	0	1.041	0.756
CaSO <sub>4</sub>	0.71	3.56	0.02	0.05	0.01	0.03	0.743	0.473	0.102	0.634	0.872
CaCl <sub>2</sub>	2.04	0.20	1.60	0.08	0.50	0.20	0.006	0.022	0.020	0.053	0.053
caco <sub>3</sub>	0.15	0.14	3.90	0.22	1.10	0.39					
MgCl <sub>2</sub>	0.08	0.04	:	t I I		1	0.002	0.006	0.008	0.052	0.024
MgSO <sub>4</sub>							1				-
Mg CO <sub>3</sub>											
Na <sub>2</sub> SO <sub>4</sub>											1
Na 2CO 3											
KC1							1				, , ,
Fe <sub>2</sub> 0 <sub>3</sub>											
R203	3.52	0.10									
A1 203											
SiO2	1.42	0.03	1	1	1	1					
Tota1	100.00	100.00	100.89	100.00	100.51	100.72	066.060	100.000	100.000	99.993	100.000
Source of Data	[35]	[32]	[35]	[32]	[32]	[32]	[125]	[35]	[35]	[35]	[125]

Compound		Bed	ded salt, Kansas			Bedded salt Hutchinson, Kansas
NaCl	96.776(1)	96,001 <sup>(1)</sup>	96.150 <sup>(2)</sup>	95.465 <sup>(2)</sup>	96.900	96.970
Moisture						0.670
Acid Insoluble	0.165	0.316		0.208		
Water Insoluble			0.223		0.24	1.407
$CaSO_4$	2.744	3.203	3.252	3.978	2.55	0.857
CaC1 <sub>2</sub>	0.010	0.033	0.018	0.015		0.031
CaCO <sub>3</sub>						
MgC1 <sub>2</sub>	0.293	0.426	0.342	0.322	0.24	0.066
MgS04					0.07	1
MgCO <sub>3</sub>						
Na <sub>2</sub> SO <sub>4</sub>						1
Na <sub>2</sub> CO <sub>3</sub>						
KC1						:
Fe203	0.012	0.021	0.015	0.012		
$R_2 O_3$						
A1 203						
SiO2						
Tota1	100.000	100.000	100.000	100.000	100.000	100.001
Source of Data	[35]	[35]	[35]	[35]	[35]	[125]

coluble soluble	Bedded sa 98.097 0.530 1.173 0.011 0.027 0.639	11, Ohio 97.60 0.40 2.00	91.57	Bedded sal 86.70	t, Oklahoma 94.08	93.15
al	100.477	100.00	(3)	(3)	(3)	(3)
of Data	[35]	[35]	[35]	[35]	[35]	[35]

Foo

- Fercent Nach determined from the difference between the sum of the other constituents and lov percent this method was probably also used for other analyses that total exactly 100 percent. []
- "Analyses are of salt as mined from beds of high-purity sodium chloride and do not represent the composition of the entire evaporite deposit" [126]. This may apply to other high-sodium-chloride values in this table. (2)
- No percent other than NaCl given in report of analysis. (3)

rotation of the entire crystal and translation gliding within it during flow. The rotation and translation are counteracted by the effects of recrystallization during periods of quiescence or contemporaneously with flow. In the deeper parts of domes, higher temperatures increase diffusion rates, and recrystallization processes keep pace with those causing crystal elongation.

Anhydrite stringers are commonly vertically aligned in domes, where linear concentrations of small aligned crystals form "pencil anhydrite." This alignment is well shown in the Grand Saline Dome in Texas [65].

#### 1.4.3.3. Pseudomorphism

Minerals may be entirely replaced several times by other minerals more stable at varying temperature and pressure conditions because the salts deposited from the brines are only stable at low temperatures or because the phases precipitated are metastable and increased temperature permits the recombination of the chemical components. Schaller and Henderson [63] cited many examples of such pseudomorphism, which is the replacement of the mineral but the retention of its crystal form. Among the more common, besides the above-mentioned halite-for-gypsum replacement, are polyhalite replacing anhydrite, kainite replacing langbeinite, and sylvite replacing carnallite. In some crystals, where the physical properties of the replacement mineral are similar to those of the original, x-ray diffraction tests are necessary to determine which mineral is present, though the crystal form is distinctive of only the original mineral.

## 1.4.4. Density of Rock Salt Deposits

At  $15^{\circ}$ C, the average density of pure NaCl is 2.165 g/cm<sup>3</sup> [66]. The density of the rock salt in most natural deposits is close to this. But, as the percentage of dense anhydrite impurity increases, so does the density of the sample. A rock that is 20 percent anhydrite and 80 percent halite rock would have a density of 2.32 g/cm<sup>3</sup> and a specific volume of 0.431 cm<sup>3</sup>/g. Odé [67, p. 685] stated "the density of rock salt aggregates varies roughly between 2.16 and 2.25. The variations are usually caused by anhydrite." Compaction is a negligible variable in changing the density of salt, even to depths of 18,300 meters [68]. Tables 1.5b and 1.5a list published densities and specific volumes of rock salt and other evaporites from some United States deposits and of individual constituent minerals in their pure form.

In the few cases where the type of density (table 1.5b) was indicated by the primary source, the bulk density was measured. This includes the volume of the pore space in the rock. The bulk density is relevant to

geophysical measurements of the rock in place, whereas the grain densities as listed in table 1.5a are useful for laboratory work on individual crystals. In most salt deposits, the pore space is minimal, and only a slight difference exists between bulk and grain densities of rock salt. Guido and Warner [69] gave the following comparison of density values for one sample from the Winnfield Dome of Louisiana:

> Bulk  $2.163 \pm 0.018 \text{ g/cm}^3$  (7 tests) Grain  $2.191 \pm 0.010 \text{ g/cm}^3$  (4 tests)

The procedures used in the measurement of the densities were as follows:

## Grain Density

a. Specimens powdered, dried, and weighed.

b. Specimen volumes determined by kerosene displacement.

c. Specimen densities averaged.

## Bulk Density

a. Specimen stripped clean and weighed to 0.1 gram.

b. Specimen volume determined to 0.1 cm<sup>3</sup> by Hg displacement.

The more variable the mineralogy of a salt deposit, the more variable will be the bulk densities. Where potash beds are present and where diagenetic or metamorphic changes have occurred, abrupt changes in mineralogy and, therefore, density are common. In the potash deposits of New Mexico, horizontal sylvite and langbeinite beds commonly are abruptly truncated by zones of massive halite that were deposited from secondary migrating fluids. The replacement of sylvite (density  $1.98 \text{ g/cm}^3$ ) by halite ( $2.16 \text{ g/cm}^3$ ) would produce an anomalously dense zone, whereas the replacement of langbeinite ( $2.83 \text{ g/cm}^3$ ) by halite would cause a minor decrease in relative density.

# **1.5. Fluid Inclusions**

# 1.5.1. Formation

Fluid inclusions in rock salt deposits range in volume from fractions of microliters to centiliters. They are formed when fluid is trapped in irregularities of growing crystals or in rehealed fractures. As such, they are records of the composition, temperature, and pressure of the fluid medium that was present during crystal growth or fracturing.

Ionic ratios in primary inclusions in bedded halite have been used to document the unchanged composition of sea water since Paleozoic time. Because neither

# Table 1.5a Reported Densities of Selected Pure Evaporite Minerals

Samp1e	Formula	Grain Density g/cm <sup>3</sup>	Specific Volume cm <sup>3</sup> /g	Source of Data
Anhydrite	CaSO <sub>4</sub>	2.89-2.98	0.346-0.336	[127]
		2.90	0.345	[57]
		2.963	0.337	[128]
		2.9-3.0	0.345-0.333	[129]
Calcite	CaCO <sub>3</sub>	2.72	0.368	[127]
		2.712	0.369	[128]
Carnallite	KMgC1 <sub>3</sub> •H <sub>2</sub> O	1.6	0.625	[127]
		1.60	0.625	[57]
		1.598	0.626	[128]
		1.6	0.625	[129]
Dolomite	CaMg(CO <sub>3</sub> ) <sub>2</sub>	2.85	0.351	[127]
		2.866	0.389	[128]
Gypsum	$CaSO_4 \cdot H_2O$	2.32	0.431	[127]
		2.31	0.433	[57]
		2.317	0.432	[128]
		2.3-2.4	0.435-0.417	[129]
Halite	NaC1	2.16	0.463	[127]
		2.16	0.463	[57]
		2.163	0.462	[128]
		2.1-2.2	0.467-0.455	[129]
Langbeinite	K <sub>2</sub> SO <sub>4</sub> •MgSO <sub>4</sub>	2.77	0.361	[128]
		2.82-2.83	0.357-0.353	[129]
Polyhalite	$K_2Ca_2Mg(SO_4)_4 \cdot 2H_2O$	2.78	0.360	[127]
		2.78	0.360	[128]
		2.78	0.360	[129]
Sy1vite	KC1	1.99	0.503	[127]
		1.98	0.505	[57]
		1.987	0.503	[128]
		1.98	0.503	[129]

# Table 1.5b Measured Densities of Natural Salt Deposits

Sample Composition	Sample Location	Bulk Density g/cm <sup>3</sup>	Specific Volume cm <sup>3</sup> /g	Source of data
Anhydrite				
Caprock	Grand Saline Dome, Texas	2.37-2.64	0.422-0.379	[130]
Anhydrite	Hockley Salt	2.35-2.89	0.426-0.346	[131]
with salt	Dome, Texas	2.89-2.91	0.346-0.344	[131]
TOCK		2.84-2.97	0.352-0.337	[131]
		2.60-2.90	0.385-0.345	[131]
Anhydrite	average from several localities.	2.9	0.345	[1 3 2]
Gypsum				
Weathered gypsum	Grand Saline Dome, Texas	2.26-2.36	0.442-0.424	[130]
Gypsum	Hockley Salt Dome, Texas	2.07	0.483	[131]
Gypsum	average from several localities.	2.2-2.6	0.455-0.385	[1 3 2]
Rock salt - Is	solated Measuremen	ts		
"Clear salt"	Grand Saline Dome, Texas	2.13-2.16	0.469-0.463	[130]
"Dark salt"	Grand Saline Dome, Texas	2.22-2.25	0.450-0.444	[130]
Salt	Winnfield Salt Dome, LA.	2.17	0.461	[130]
Salt	Hockley Salt Dome, Texas	2.20-2.21	0.455-0.452	[130]
Salt	Hockley Salt Dome, Texas	2.19-2.20	0.457-0.455	[1 30]
Salt	Hockley Salt Dome, Texas	2.15-2.18	0.456-0.459	[130]
Bedded salt	Eddy County, New Mexico	2.16	0.463	[130]
Rock salt - Va	ariation within Do	mes		
"Rock salt"	Hockley Dome, Texas	2.38	0.420	[131]
"Rock salt"	Hockley Dome, Texas	1.92	0.521	[131]
"Rock salt"	Hockley Dome, Texas	2.20	0.455	[131]

	Lable	e 1.56Continued		
"Rock salt"	Hockley Dome, Texas	2.39	0.418	[131]
"Rock salt"	Hockley Dome, Texas	2.23	0.448	[131]
"Rock salt"	Hockley Dome, Texas	2.18	0.457	[131]
"Rock salt"	Hockley Dome, Texas	2.18	0.457	[131]
"Rock salt"	Hockley Dome, Texas	2.19	0.457	[131]
"Rock salt"	Hockley Dome, Texas	2.21	0.453	[131]
"Rock salt"	Hockley Dome, Texas	2.26	0.442	[131]
"Rock salt"	Hockley Dome, Texas	2.28	0.439	[131]
96.3% NaCl	Winnfield Dome, LA	2.14	0.467	[133]
97.7% NaCl	Winnfield Dome, LA	2.15	0.465	[133]
87.5% NaCl	Winnfield Dome, LA	2.16	0.463	[133]
93.4% NaCl	Winnfield Dome, LA	2.23	0.448	[133]
99.3% NaCl	Winnfield Dome, LA	2.15	0.465	[133]
95.0% NaCl	Winnfield Dome, LA	2.12	0.472	[133]
78.4% NaCl	Winnfield Dome, LA	2.19	0.457	[133]
99.1% NaCl	Winnfield Dome, LA	2.14	0.467	[133]
97.1% NaCl	Winnfield Dome, LA	2.16	0.463	[133]
Dome salt	Avery Island Salt Dome, LA	2.14	0.467	[134]
Dome salt	Avery Island Salt Dome, LA	2.11	0.474	[134]
Dome salt	Avery Island Salt Dome, LA	2.12	0.472	[134]
Dome salt	Avery Island Salt Dome, LA	2.14	0.467	[134]
Dome salt	Avery Island Salt Dome, LA	2.10	0.476	[134]

bromine nor magnesium is a significant constituent of any of the minerals formed prior to the halite phase in the precipitation sequence, the Br/Mg ratios of primary fluid inclusions are similar to those of the original brines. Holser [70] stated that:

"Most of the Br/Mg ratios in the brine inclusions from Hutchinson are close to that of sea water and to modern bitterns. This indicates both that the inclusions are virtually unchanged samples of the bitterns left behind in Permian time and that the Br/Mg ratio of the sea has remained constant since the Permian... Brine inclusions from the Silurian of Michigan have a similar composition ..."

Ionic ratios in fluid inclusions also record the stage of evaporation or concentration of the brine at the time of halite crystallization. Kramer [71] indicated that the brines that precipitated the salt of the Salina Formation in Ohio and Michigan had concentrations 12 to 14 times that of normal sea water. Holser [70] believed that the brines that deposited the salt of the Hutchinson Salt Member of the Wellington Formation in Kansas were concentrated almost to the potash phase (a concentration factor of almost 64 times).

Because halite contains essentially zero magnesium and very little bromine, secondary inclusions formed during resolution, and precipitation of halite can be distinguished from primary inclusions by low Br/Cl and very low Mg/Cl ratios.

The temperature of formation of inclusions is also considered to be recorded in the vapor bubble that is present in some fluid inclusions. Assuming that the crystal formed at the earth's surface (at ambient pressure) in a purely aqueous medium, the vapor bubble must have formed in response to the vacuum created as the fluid enclosed within the crystal subsequently cooled and contracted. Unless some fluid has leaked from the inclusion, temperatures of formation can be experimentally determined by heating the inclusion to the point where the fluid expands to eliminate the bubble [72].

Dreyer and others [73] determined these temperatures for halite to be between 70° and 100°C and concluded that these high temperatures were records of the exothermic heat of crystallization localized at the crystal surface and not the overall temperatures of the precipitating brines. Peach [74], however, believed that these temperatures recorded overall formation temperatures and pressures during secondary recrystallization at depth.

#### 1.5.2. Composition

Data on the composition of fluid inclusions is minimal; many publications give only comparative ionion ratios rather than absolute parts per million. Tables 1.6a and 1.6b list some of the published data, many of them coming from Roedder [75]. In general, fluid inclusions are at saturation with respect to NaCl because their host mineral is halite. Metamorphism and recrystallization can cause the other ionic constituents of inclusions to vary greatly, even in adjacent inclusions. The major cations are Na<sup>+</sup>, Ca<sup>2+</sup>, and Mg<sup>2+</sup>; the dominant anion is Cl<sup>-</sup>, and some SO<sub>4</sub><sup>2-</sup> is present.

Kramer [76] stated "obviously secondary inclusions from Ontario (the Salina Formation) were almost pure NaCl brine." Roedder [77] noted that other inclusions from the same formation contain concentrated calcium brines. He also stated that most of the fluid inclusions at one locality of the Hutchinson Salt Member in Kansas are nearly pure NaCl brine.

Inclusions in domed rock salt have been subjected to recrystallization and, at least, mechanical deformation. At best, these inclusions can be considered to be only residues of the precipitating liquors or samples of secondary metamorphic brines. The methane gas and liquid oil inclusions in many of the Louisiana salt domes are certainly of secondary origin, having been incorporated into the salt contemporaneously with the dome formation.

Kramer [78] detailed a procedure for preparing and analyzing fluid inclusions, a summary of which follows:

1. 30 mg samples of inclusion-rich salt were first examined for inclusion morphology.

2. A 30 mg sample of inclusion-free salt from the same specimen was selected as a blank.

Table 1.6aPublished Compositions of Fluid Inclusions in United States Rock Salt. Modified from [135]

Sample Number	Na <sup>+</sup>	к+	Ca <sup>2+</sup>	Mg <sup>2+</sup>	C1	so <sub>4</sub> 2-	F	Concentration	Location of Sample
1	69,100	3,500	13,700	1,600	110,000	44,800	58	242,600	Salina salt beds (Silurian) Goderich, Ontario
2	88,200	4,700	16,400	2.050	145,000	38,100	63	294,500	Salina salt beds (Silurian) Cleveland, Ohio

Parts per Million of Total Inclusion Fluid

ginal Sourc of Data	[71]	[11]	[136]	[136]	[136]	[136]	[136]	[136]	[136]	[136]
Ori Location of Sample	Salina salt beds (Silurian) Goderich, Ontario	Salina salt beds (Silurian) Cleveland, Ohio	Wellington Formation (Permian) Hutchinson, Kansas	Salina salt beds (Silurian) Goderich, Ontario	Salado salt (Permian) Carlsbad, New Mexico	Salado salt (Permian) Carlsbad, New Mexico	Holocene salt, Baja, California			
s04/C1	0.41	0.26		0.034						
Br/C1			0.00122	0.0138	0.016	0.017	0.013	0.0034	0.0035	0.0133
Ca/C1	0.124	0.113	0.000	0.000	0.000	0.000	0.13	0.000	0.000	0.001
Mg/C1	0.015	0.014	0.219	0.237	0.247	0.22	0.21	0.068	0.171	0.258
Na/C1	0.63	0.61								
K/C1	0.030	0.030								
F/C1	0.00053	0.00043								
Sample Number	$1^{1/2}$	21/	N	4	IJ	9	7	ω	6	10

e

Table 1.6b Published Ratio-by-Weight Analyses of Fluid Inclusions in Halite Modified from [136,137]

Footnotes:

ы Roedder [75] calculated these weight ratios from the molar ratios originally presented. Analyses were made by microchemical leaching procedure and would give average fluid compositions for the sample. 1

3. Samples were weighed to  $\pm 2$  micrograms.

4. Samples were dried to a constant weight at 125°C.

5. Samples were ground with mortar and pestle and again dried to constant weight at 125°C.

6. Loss of weight between steps 4 and 5 was taken as the loss of inclusion water.

7. Ground samples were dissolved in water, and the solution was analyzed chemically. Ionic values greater than those of the blank sample were considered to have been derived from the inclusion fluids.

8. "The methods employed were flame emission for Na and K, chloranilate calorimetry and thorin titration for sulfate, potentiometric titration with AgNO<sub>3</sub> for Cl, alizarin calorimetry for F, fluorescence titration with calcein and EDTA for Ca, and EBT titration with EDTA for Ca and Mg" [78].

Fluid inclusions in halite are irregularly distributed and in many places are abundant adjacent to other zones where they are absent. They may be spherical, minimizing surface area, or cubic "negative" crystals, minimizing surface potential. Shuman and Fiedelman [79] found that, in artificially grown crystals, round inclusions formed in highly agitated water whereas cubic inclusions formed in quiet water. The number of inclusions in a sample is a "function of crystal size, concentration of solid particles in suspension in the brine, and particle size of the inclusions" [79]. Their irregular distribution is probably due to secondary metamorphism or recrystallization.

Inclusion volumes in some laboratory-grown halite crystals range from 0.23 to 0.45 percent of the total volume [79]. Roedder [80] stated that commercial reagent-grade halite contains abundant fluid inclusions that constitute about 0.5 percent of the total weight and that the inclusions in the bedded rock salt investigated constituted 0.44 weight percent of the rock.

The reported water content of rock salt is often well below this 0.5-percent figure. Aufricht and Howard [81] gave the following percentages of total volume occupied by water in rock-salt samples: rock salt in central Kansas, 0.05-0.08 percent; salt mines in Detroit, 0.1-0.15 percent; Louisiana salt domes, 0.003-0.008 percent. Odé [82] listed typical weight percentages of moisture from Hutchinson and Lyons Mines, Kansas, as 0.127-0.293 percent and 0.090-0.100 percent, respectively. Although Odé's analyzed samples were heated in excess of 250°C, most moisture analysts do not heat their sampes above 125°C. All moisture analyses in which the sample was heated above 125°C must be suspect. At 125°C, rock salt will still contain a residual calcium-magnesium-chloride brine from which the water will not be removed.

As indicated by figure 1.8, 100 percent of the moisture is not released by salt during normal laboratory heating times until the sample is heated in excess of 625°C. Shuman and Fiedelman [83] stated that, in order to remove 100 percent of the moisture in brine inclusions in salt within 1 hour, the sample must be heated to 801°C (1474°F), close to its melting point. Aufricht and Howard [84] also observed this. Roedder [85] found his 0.44 percent weight loss (attributed to vaporized fluid inclusions) on decrepitation of salt heated to incipient fusion [86].



FIGURE 1.8. Rate of moisture release from brine inclusions in halite heated to various temperatures. Modified from [147].

#### 1.5.3. Pressure Gas Inclusions

Although the vapor bubbles associated with fluid in primary inclusions are theoretically under a vacuum, other inclusions of gas are under considerable pressures. Baar [87] attributed some of these pressures to plastic deformation of rock salt by thick overburden and the resulting compression of the gas-filled cavities.

In East Germany, CO<sub>2</sub> gas associated with Tertiary volcanic activity was trapped under pressure when it was magmatically injected into buried salt deposits, partially melting them. Solidification and recrystallization enclosed the gas as inclusions and as microscopic flaws at crystal boundaries [88]. A diabase dike [89] is known to cut through the New Mexico rock salt deposits, though no association has been made between it and pressured gas inclusions.

Gas inclusions are often associated with potash beds [90], and suggestions have been made that they are accumulations of argon, derived from the radioactive potassium isotope found in such minerals as sylvite (KCl) and langbeinite  $(K_2Mg_2(SO_4)_2)$ . Hoy and others [91] have noted that carbon dioxide pockets and blowouts in Texas and Louisiana salt domes usually are near the dome boundaries. The gas probably has organic origins and may have been entrapped in processes related to the shearing and disruption of the salt during doming. Another possible source for CO<sub>2</sub> gas [92] is the
breakdown of the unstable magnesium chlorocarbonate  $(MgCl_2 \cdot MgCO_3 \cdot 7H_2O)$ .

Pressures of gas inclusions are variable and difficult to measure. A common mining measurement is the weight of the rock salt that was shattered by the violent degassing of numerous concentrated inclusions. This weight often measures in the thousands of tons, and the estimates of gas released can range in the hundreds of thousands of cubic meters (at ambient surface pressures). Some rock salt deposits are capable of yielding 3 to 20 cubic meters of gas per ton [88] although the volume of the gas as inclusions is small under pressure.

Other pressure measurements are rare and scattered. Hoy and others [93] reported estimated pressures of 50 to 100 MPa in  $CO_2$  blowouts in the Winnfield salt dome in Louisiana. McClain and others [94] noted that the steady shut-in pressure after a blowout in the AEC (Atomic Energy Commission) No. 7 well, drilling through the Permian Salado and Castile Formations of New Mexico, was 0.79 MPa, a measurement made after a considerable amount of uncontrolled gas venting. Roedder [92] cited examples of gas inclusions in Mexican and German salt that expanded their volumes 250 times after release from the confining pressures.

The most common gas inclusions in rock salt contain methane (CH<sub>4</sub>), carbon dioxide (CO<sub>2</sub>), and nitrogen (N<sub>2</sub>) [95]. Methane and nitrogen have been reported in the potash mines of New Mexico [96,97]. The weight percent of constituents of blowout gases in the AEC No. 7 well, where six samples were collected for anlyses during a 1 month period [98], was given as:

$CO_2$	—	0 to 0.54 percent
$O_2$	—	0 to 0.81 percent
$CH_4$	—	0 to 2.14 percent
CO	—	0 percent
$\mathrm{C}_{2}\mathrm{H}_{6}$		0.031 to 0.05 percent
$N_2$	_	97.08 to 99.904 percent

Analyses have also been made on the gases associated with the Winnfield Dome in Louisiana. Belchic [99] reported the presence of  $H_2S$  and  $CO_2$ . Hoy and others [100] reported:

> CO<sub>2</sub> - 46.9 percent  $H_2O = 17.3$  percent  $N_2$ - 18.4 percent CO - 4.8 percent  $0_2$ - 4.4 percent  $SO_2$ — 3.7 percent  $H_2$ — 1.8 percent CH<sub>4</sub> — 1.5 percent Ar - 0.4 percent  $C_2H_2 - 0.4$  percent Other hydrocarbons-0.4 percent

#### 1.5.4. Brine Pockets and Seeps

Pockets and seeps of brine in rock salt deposits are commonly associated with pressured gas inclusions. Some of these brines may be large-scale entrapments of the original fluids that precipitated the deposits, but many are of secondary origin, remnants of metamorphic brines, or ground waters that became saturated with respect to the adjacent minerals and lost the ability to migrate by solution. Large but rare pockets containing "a few gallons" [85] of Ca-rich brines are found in the Goderich, Ontario, salt mine and the potash mines of Saskatchewan. Baar [101] has suggested that large pockets of Ca-rich solutions result from reactions of MgCl<sub>2</sub> brines (the liquors left in the last stages of precipitation) with Ca-bearing rocks, in the reaction:

 $MgCl_2$  (brine) + CaSO<sub>4</sub> (anhydrite) = CaCl<sub>2</sub> (brine) + (MgSO<sub>4</sub> or any number of magnesium sulfate minerals).

Brine seeps and associated gases (usually  $CO_2$ ) are often found in the salt domes of the Gulf Coast. Belchic [102], citing the facts that brine seeps come up from the floor of mines more often than down from the roof and that they never freshen, believe that their source is deep within the dome rather than from ground water. The seeps are usually associated with anhydrite bands and tend to move vertically along the banding, perhaps at the anhydrite-salt contacts.

The salt mine in Winnfield Dome, Louisiana, contains the best-known examples of brine seeps. Most of these gas and brine seeps are found nearer the outer walls of the dome, though they are irregular in distribution. Flow rates are greatest just after exposure by excavation in the mine and dwindle to cessation during a period of a few years [103] either because of the sealing of the fractures or the eventual draining of the pocket of brine. Small gas and brine pockets are also found by horizontal drill holes into mining faces, but the flow from them ceases after a few hours [104]. Exploratory wells in the Winnfield Dome have penetrated pressured gas and brine pockets. Taylor [105] reported brine and gas under a pressure of 1.55 MPa at a depth of 180 meters below the mine level, and Belchic and others [99, p. 34] noted a pressure of 0.90 MPa in a cavity full of water at the anhydrite-salt contact.

### **1.6.** Porosity and Permeability

#### 1.6.1. Porosity

Most of the porosity in rock salt is quickly filled in by crystal growth and plastic flowage during deposition. Baar [106] listed porosity as a function of depth as follows: 40 percent at the surface 30 percent under 0.15 meters of overburden 20 percent under 0.30 meters of overburden 15 to 20 percent under 0.60 meters of overburden 5 to 10 percent at depths of 6 to 12 meters gradually approaches 0 percent below 12 meters

Guido and Warner [69] calculated porosity in rock salt from the Winnfield Dome at 1.28 percent by using the formula

porosity  $(\theta) = 1 - \frac{\text{bulk density}}{\text{grain density}}$ .

Aufricht and Howard [107] measured porosity in three salt domes and one deposit of bedded rock salt by using both gas expansion and brine resaturation tests performed on 2.5 to 5 cm cubic samples as follows:

"For the gas-expansion determinations, the bulk volume of the samples was determined in a mercury pycnometer. Pore volumes then were measured directly. In determining the resaturation porosities, the bulk volumes were also determined in a mercury pycnometer. The dry samples were weighed, evacuated, pressure saturated with brine and reweighed. The pore volumes were taken as the weight gains occurring upon saturation."

Table 1.7 gives Aufricht and Howard's porosity data. The range of individual samples was from 0.62 to 7.17 percent porosity, that of the averages from the four localities from 1.0 to 6.0 percent. Reynolds and Gloyna [108] gives average porosity values of 1.71 percent and 0.59 percent for rock salt from Grand Saline Dome, Texas, and the bedded salt of the Hutchinson Salt Member of the Wellington Formation, Kansas. The laboratory procedure used for measurement was not detailed.

Stevens [109] measured porosities in Permian anhydrite beds associated with salt deposits in the upper Brazos region of Texas. In 14 anhydrite samples, porosity varied from 0.3 to 4.4 percent, averaging 1.9 percent.

Using Guido and Warner's bulk-to-grain density proportion method for calculating porosity [69], the volume of fluid inclusions as well as the intercrystalline pore spaces would be measured as porosity. Using the brine resaturation method, however, only the intercrystalline voids in communication with the surface of the sample would contribute to the total porosity figure.

#### 1.6.2. Permeability

Under low confining pressures, that is at shallow depths, dry halite allows fluid flow along crystal boundaries and cleavage planes. Laboratory tests on rock salt cores have measured these permeabilities with respect to various fluids and gases (table 1.8). Reynolds and Gloyna's data [108] illustrate the direct correlation between permeability of rock salt and the confining pressure. Baar [110] stated that the presence of trapped gases in salt deposits testifies to their absolute impermeability at depth, though Aufricht and Howard [111] noted significant permeability still present in rock salt samples at confining pressures less than 55 MPa.

Aufricht and Howard detailed their permeability measurement procedures which are summarized below:

1. Samples were cut into cores 7.5 cm in diameter and about 20 cm long.

2. Cores were cast in plastic or in bismuth alloy metal or were jacketed in copper to seal lateral surfaces.

3. Samples were placed in a pressure vessel, and simulated overburden pressures were created by injecting nitrogen gas into the vessel.

4. The sample was saturated with nitrogen or degassed saturated brine or liquid hydrocarbon.

5. The fluid was passed through the sample, and the flow was allowed to stabilize.

6. Pressure drops across the sample, flow rates, and the core dimensions were measured and used to calculate permeability by Darcy's law.

				Table 1	1.7			
verage	Porosities	of	Salt	Samples	Modified	From	References	[138]

	Average porosity percent bulk volume						
Mine	Number of samples	By gas expansion	By resaturation				
Grand Saline, Texas	3	1.7					
Winnfield, LA	3	1.8	1.8				
Hutchinson, Kansas	8	1.0	0.8				
Weeks Island, LA	3		6.0				

Table	e 1.	. 8	
Permeability	of	Rock	Salt

Samples	Permeabili initial/max	ty (md) minimum	Confining pressure (MPa)	Fluid Used	Source of Data
Grand Saline <sup>1/</sup> Dome, Texas	1.01-4.25	0.11-3.24	3.4	Kerosene or $brine^{2/2}$	[108]
	0.01-0.46	0-0.15	6.9	Brine <sup>2/</sup>	[108]
	0.05-0.21	0-0.05	10.3	Kerosene or $brine^{2/2}$	[108]
	0.51	0.0005	15.9	Kerosene	[108]
	0.06	0.0002	20.7	Brine <sup>2/</sup>	[108]
Hutchinson Salt	0	0	3.4	Helium or kerosene	[108]
beu, kansas	0-0.072	0	6.9	Brine <sup>2/</sup>	[108]
	0	0	10.3	Helium	[108]
	0.0015	0	13.8	Brine <sup>2/</sup>	[108]
	0.023	0.0005	15.9	Kerosene	[108]
	Average	Permeability			
Grand Saline Dome, Texas	1-9		< 0.7	Dry nitrogen	[139]
Hutchinson Salt Bed, Kansas	5.7		< 0.7	Dry nitrogen	[139]
Winnfield Salt Dome, LA	43		< 0.7	Dry nitrogen	[139]
Weeks Island Dome, LA	631		< 0.7	Dry nitrogen	[139]

Footnotes

 $\frac{1}{2}$  Quoted permeability converted to millidarcies

 $\frac{2}{}$  Brines used were NaCl, NaCl + CaSO<sub>4</sub>, or NaCl + Al(NO<sub>3</sub>)<sub>3</sub>

The permeability of halite is effectively zero when the pressure is sufficient to deform the halite plastically and close off the passageways at crystal interfaces. Observed permeability in rock salt samples at high confining pressures then, must be due to the presence of impurities or must be artifacts of laboratory techniques. Baar [112] asserted that "standard permeability tests on rock salt cores are usually of no use, for the cores are damaged when taken out of their tri-axial in-situ stress field. Such damage may be caused by stress relief deformation that results in intergranular loosening."

Another variable is the solution flowing through the sample. Fluids "inert" with respect to halite, such as hydrocarbons, flow more quickly and for longer periods of time than do saturated brines. (Fresh water would, of course, dissolve halite and enhance permeability until the fluid reached saturation.) Permeability using saturated brine decreases rapidly with time (figure 1.9a), probably owing to recrystallization of halite in the passageways and the enhanced plasticity of halite in the presence of water. Aufricht and Howard [111] believed that, after a certain time, however, stabilization may



FIGURE 1.9a. Laboratory permeability of rock-salt samples to saturated brine at one atmosphere. Modified from [148].

occur in the brine/rock salt system, would stabilize, and would contain a small remnant permeability.

The presence of brine also inhibits permeability through the shale partings and anhydrite lenses often found in rock salt deposits. Water may hydrate anhydrite stringers and the clays of shale partings and increase their volume, squeezing off permeability. The resolution and deposition of  $CaSO_4$  caused by brine in anhydrite also helps choke off the permeability.

Laboratory permeability of rock salt to nitrogen, oil, and brine under a simulated overburden pressure of 5.51 MPa [149] is shown in figure 1.9b.



FIGURE 1.9b. Laboratory permeability of rock salt to nitrogen, oil, and brine under simulated overburden pressure of 5.51 MPa. Modified from [149].

In spite of these theoretical and laboratory results, evidence for local movement of quantities of water through rock salt deposits is not uncommon. Anhydrite banding in salt domes is "variably porous and permeable, and often partially saturated with brine and CO<sub>2</sub> gas" [113]. Seeps and drips are known in most salt and potash mines, though those that come down from the roof may be ground water that has found its way down manmade passages.

The interfaces between halite and shale or halite and anhydrite are often suspected of having greater permeability than the beds themselves [114,115]. Permeability is greater parallel to bedding than it is perpendicular to it. The Winnfield Dome salt mine has numerous seeps of brine and gas from the floor and ceiling, yet "little or no brine or gas flow from the walls" [104].

The sheared "shale sheath" zone that encircles Gulf Coast salt domes is avoided by salt miners because of severe water leakage problems found there [116]. These leakage problems imply abundant and mobile water and high permeability. On the other hand, this zone is also avoided by well drillers because of overpressured gas pockets commonly associated with it, implying nonpermeable zones.

#### 1.6.3. Permeability in LPG Storage Caverns

The fluid integrity of many rock salt deposits with respect to hydrocarbons has been tested by oil companies who store liquid petroleum gas (LPG) in cavities artificially dissolved out of the rock salt. Beds of halite are rarely thick enough to enclose a full-scale storage cavern, but the associated anhydrite bands and other impurities seem to be largely impermeable in these caverns [60]. Aufricht and Howard [117], using gasoline as a fluid, found a range of permeabilities through salt from 0 to 6 md, the average permeability was 0.3 md. Table 1.9 gives estimated recovery percentages for storage caverns in the Salado Formation in New Mexico and several other locations.

Hawkins and Jirik [118, p. 17] stated "with some exceptions, the recovery of stored LPG products (from caverns in Louisiana salt domes) has been good, generally above 90 percent." The 1956 Interstate Oil Compact Commission [119] also puts the recovery figure at generally greater than 90 percent, and some of the loss is probably due to above-ground handling losses. The lowest recovery percentage given was 57 percent, but the circumstances for this low figure were not described. Recovery percentages usually increase after the initial withdrawal from the cavern, prior losses being contributed to by infilling of cavern irregularities with nonrecoverable oil. Aufricht and Howard [120], however, noted a slight decrease in permeability of salt with respect to oil (and nitrogen) with time. Table 1.9 shows a fair inverse correlation between storage pressure and percent recovery.

#### 1.7. Pore Fluids

#### 1.7.1. Composition

The character of pore fluids is a function of the composition and history of the rock salt. The only generalization that is possible is that the NaCl content of the pore fluid is saturated or nearly saturated in the mineral halite. Tables 1.10 through 1.19 give the concentration of NaCl that is in the aqueous solution containing KCl, MgCl<sub>2</sub>, CaCl<sub>2</sub>, and combinations of CaCl<sub>2</sub> with KCl between 0 and 100°C [121]. Table 1.21 gives the solubility of NaCl in halite saturated water above 100°C.

#### 1.7.2. Vapor Pressure

Table 1.20 gives the experimentally measured vapor pressures for various synthetic, halite-saturated brines

# Table 1.9 Percent Recovery of Stored Liquid Petroleum Gas Stored in Solution Cavities in Salt Deposits. Adopted from Reference [119], table 13

Location	Formation	Capacity of Cavern (gallons)	Storage Pressure (MPa)	Estimated Recovery %
New Mexico	Salado	781,200	4.1	90
New Mexico	Salado	1,500,000	2.1	90
New Mexico	Salado	1,848,672	1.4	98.0
New Mexico	Salado	1,000,000	1.5	97
New Mexico	Salado	1,456,980	1.4	98
New Mexico	Salado	2,000,000	2.1	90.0
New Mexico	Sal ado	2,005,580	3.6	95 <u>1</u> /
New Mexico	Salado	2,422,000	3.8	92.0
New Mexico	Salado	2,216,000	4.1	90.0
New Mexico	Salado	1,000,000	1.6	97
New Mexico	Salado	1,000,000	1.6	97
Louisiana	Pine Prairie Salt Dome			93.3
Kansas	Permian salt			92.86
Kansas	Permian salt			95
Kansas	Permian salt			92.5

1/ Originally shown in Table 13 as 9.7 percent - personal communication to Warren Petroleum Corp., Hobbs, N.M., indicated 95 percent as an approximate figure.

Table 1.10 Solubility of NaCl (weight percent) in KCl solutions as given. Data in parentheses, (), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [], for the 0°, 50°, and 100°C isotherms.

#### Temperature KC1 concentration in weight percent (0.0)

(°C)	0	2	4	6	8	10	12
		_	_	-	_		
0	(25.94) [.13]	(24.84) [.13]	(23.75) [.14]	(22.65) [.14]	(21.56) [.15]	(20.46) [.15]	(19.37) [.16]
1 0 20 30 40 5 0	(26.07) (26.23) 26.39 26.57 26.77 [.05]	(24.98) (25.13) 25.30 25.48 25.68 [.04]	(23.88) (24.04) 24.20 24.38 24.58 [.04]	(22.79) (22.94) 23.11 23.29 23.49 [.05]	(21.69) (21.85) 22.01 22.10 22.39 [.06]	(20.60) (20.75) 20.92 21.10 21.30 [.07]	(19.50) (19.66) 19.82 20.00 20.20 [.09]
60 70 80 90 100	26.99 27.22 27.46 27.73 28.00 [.08]	25.89 26.12 26.37 26.63 26.91 [.07]	24.80 25.03 25.27 25.54 25.81 [.07]	23.70 23.93 24.18 24.44 24.73 [.08]	22.61 22.84 23.08 23.35 23.62 [.08]	21.51 21.74 21.99 22.25 22.53 [.09]	20.42 20.65 20.89 21.16 21.43 [.10]

Table 1.11 Solubility of NaCl (weight percent) in  ${\rm MgCl}_2$  solutions as given. Data in parentheses, ( ), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [ ], for the 0°, 50°, and 100°C isotherms.

emperature	MgCl <sub>2</sub> concentration in weight percent									
(°C)	0	2	4	6	8	10	12	14	16	18
0	(25.94) [.13]	(23.62) [.13]	(21.37) [.13]	(19.17) [.13]	(17.04) [.14]	(14.96) [.14]	(12.95) [.15]	(10.99) [.16]	(9.09) [.17]	(7.26) [.19]
10 20 30 40 50	(26.07) 26.23 26.39 26.57 26.77 [.05]	(23.77) 23.93 24.11 24.30 24.51 [.04]	(21.53) 21.70 21.89 22.09 22.32 [.05]	(19.34) 19.53 19.73 19.94 20.18 [.06]	(17.22) 17.41 17.63 17.85 18.10 [.07]	(15.15) 15.36 15.58 15.82 16.08 [.07]	(13.15) 13.37 13.60 13.85 14.12 [.06]	(11.20) 11.43 11.68 11.94 12.22 [.06]	(9.32) 9.56 9.82 10.09 10.38 [.07]	(7.49) 7.75 8.01 8.30 8.60 [.08]
60 70 80 90 100	26.99 27.22 27.46 27.73 28.00 [.08]	24.74 24.98 25.24 25.51 25.80 [.07]	22.55 22.81 23.07 23.36 23.66 [.08]	20.43 20.69 20.97 21.27 21.58 [.09]	18.36 18.63 18.92 19.23 19.56 [.10]	16.35 16.64 16.94 17.26 17.59 [.11]	14.40 14.70 15.01 15.34 15.69 [.12]	12.51 12.82 13.15 13.49 13.85 [.13]	10.69 11.01 11.34 11.70 12.06 [.15]	8.92 9.25 9.60 9.96 10.34 [.17]

Table 1.12 Solubility of NaCl (weight percent) in  $CaCl_2$  solutions as given. Data in parentheses, ( ), are extrapolated; the solutions may be supersatured in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [ ], for the 0°, 50°, and 100°C isotherms.

#### Temperature

т

#### CaCl<sub>2</sub> concentration in weight percent

(°C)	0	2	4	6	8	10	12	14
0	(25.94) [.13]	(23.01) [.13]	(21.91) [.13]	(19.94) [.14]	(18.01) [.14]	(16.12) [.14]	(14.26) [.14]	(12.43) [.15]
10 20 30 40 50	(26.07) (26.23) 26.39 26.57 26.77 [.05]	(24.06) (24.22) 24.40 24.60 24.81 [.05]	(22.07) (22.25) 22.44 22.65 22.88 [.06]	(20.12) (20.31) 20.52 29.75 20.99 [.07]	(18.21) (18.41) 18.63 18.87 19.13 [.07]	(16.32) (16.55) 16.78 17.03 17.30 [.07]	(14.48) (14.71) 14.96 15.23 15.51 [.07]	(12.67) (12.92) 13.18 13.46 13.76 [.08]
60 70 80 90 100	26.99 27.22 27.46 27.73 28.00 [.08]	25.04 25.28 25.54 25.82 26.11 [.08]	23.12 23.38 23.66 23.95 24.25 [.08]	21.24 21.52 21.80 22.11 22.43 [.09]	19.40 19.68 19.99 20.30 20.64 [.09]	17.59 17.89 18.20 18.53 18.88 [.09]	15.81 16.12 16.45 16.80 17.16 [.10]	14.07 14.40 14.74 15.10 15.48 [.12]

Table 1.13 Solubility of NaCl (weight percent) in a solution containing 2 weight percent CaCl<sub>2</sub> plus the KCl concentration as given. Data in parentheses, ( ), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [ ], for the 0°, 50°, and 100°C isotherms.

Temperature		KC1 con	KCl concentration in weight percent						
<u>(°C)</u>	<u>0</u>	2	4	<u>6</u>	8	10	12		
0	(23.91) [.13]	(22.88) [.13]	(21.86) [.13]	(20.83) [.13]	(19.81) [.14]	(18.78) [.14]	(17.76) [.15]		
10 20 30 40 50	(24.06) (24.22) 24.40 24.60 24.81 [.05]	(23.03) (23.20) 23.38 23.57 23.78 [.04]	(22.01) (22.17) 22.35 22.55 22.76 [.04]	(20.98) (21.15) 21.33 21.52 21.74 [.05]	(19.96) (20.12) 20.30 20.50 20.71 [.06]	(18.93) (19.10) (19.29) 19.47 19.69 [.07]	(17.91) (18.07) (18.25) 18.45 18.66 [.09]		
60 70 80 90 100	25.04 25.28 25.54 25.82 26.11 [.08]	24.01 24.26 24.52 24.79 25.09 [.07]	22.99 23.23 23.49 23.77 24.06 [.07]	21.96 22.21 22.47 22.74 23.04 [.08]	20.94 21.18 21.44 21.72 22.01 [.09]	19.91 20.16 20.42 20.69 20.99 [.10]	18.89 19.13 19.39 19.67 19.96 [.11]		

Table 1.14 Solubility of NaCl (weight percent) in a solution containing 4 weight percent CaCl, plus the KCl concentration as given. Data in parentheses, ( ), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [ ], for the 0°, 50°, and 100°C isotherms.

#### Temperature

#### KC1 concentration in weight percent

<u>(°C)</u>	<u>0</u>	2	4	<u>6</u>	8	<u>10</u>	12
0	(21.91) [.13]	(20.89) [.13]	(19.88) [.13]	(18.87) [.13]	(17.86) [.13]	(16.84) [.14]	(15.83) [.14]
10 20 30 40 50	(22.07) (22.25) 22.44 22.65 22.88 [.05]	(21.06) (21.24) 21.43 21.64 21.87 [.04]	(20.04) (20.22) 20.42 20.63 20.86 [.04]	(19.03) (19.21) 19.41 19.62 19.84 [.04]	(18.02) (18.20) 18.39 18.60 18.83 [.05]	(17.01) (17.19) (17.38) 17.59 17.82 [.06]	(15.99) (16.17) (16.37) 16.58 16.80 [.08]
60 70 80 90 100	23.12 23.38 23.66 23.95 24.25 [.08]	22.11 22.37 22.64 22.93 23.24 [.08]	21.10 21.36 21.63 21.92 22.23 [.07]	20.08 20.34 20.62 20.91 21.21 [.07]	19.07 19.33 19.60 19.89 20.20 [.08]	18.06 18.32 18.59 18.88 19.19 [.09]	17.05 17.30 17.58 17.87 18.17 [.10]

Table 1.15 Solubility of NaCl (weight percent) in a solution containing 6 weight percent CaCl<sub>2</sub> plus the KCl concentration as given. Data in parentheses, ( ), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [ ], for the 0°, 50°, and 100°C isotherms.

Т

emperature	<u>K(</u>	C1 concei	ntration	in weigh	nt percer	nt
<u>(°C)</u>	<u>0</u>	2	4	<u>6</u>	8	10
0	(19.94) [.13]	(18.95) [.13]	(17.95) [.13]	(16.96) [.13]	(15.96) [.13]	(14.97) [.14]
10 20 30 40 50	(20.12) (20.31) 20.52 20.75 20.99 [.06]	(19.13) (19.32) 19.53 19.75 19.99 [.05]	(18.13) (18.32) 18.53 18.76 19.00 [.04]	(17.13) (17.33) 17.54 17.76 18.00 [.05]	(16.14) (16.33) 16.54 16.76 17.01 [.06]	(15.14) (15.34) (15.54) 15.77 16.01 [.08]
60 70 80 90 100	21.24 21.52 21.80 22.11 22.43 [.09]	20.25 20.52 20.81 21.11 21.43 [.08]	19.25 19.52 19.81 20.13 20.44 [.07]	18.26 18.53 18.82 19.12 19.44 [.08]	17.26 17.53 17.82 18.13 18.45 [.09]	16.27 16.54 16.83 17.13 17.45 [.10]

Table 1.16 Solubility of NaCl (weight percent) in a solution containing 8 weight percent  $CaCl_2$  plus the KCl concentration as given. Data in parentheses, ( ), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [ ], for the 0°, 50°, and 100°C isotherms.

Temperature		KC1 concentration in weight percent						
<u>(°C)</u>	<u>0</u>	1	2	3	4	5	<u>6</u>	7
0	(18.01) [.14]	(17.53) [.14]	(17.05) [.13]	(16.57) [.13]	(16.08) [.13]	(15.60) [.13]	(15.12) [.13]	(14.63) [.13]
10 20 30 40 50	(18.21) (18.41) 18.63 18.87 19.13 [.07]	(17.72) (17.93) 18.15 18.39 18.64 [.06]	(17.24) (17.45) 17.67 17.91 18.16 [.06]	(16.76) (16.96) 17.19 17.42 17.68 [.05]	(16.27) (16.48) 16.70 16.94 17.19 [.05]	(15.79) (16.00) 16.22 16.46 16.71 [.05]	(15.31) (15.51) 15.74 15.97 16.23 [.05]	(14.82) (15.03) 15.25 15.49 15.74 [.06]
60 70 80 90 100	19.40 19.68 19.99 20.30 20.64 [.10]	18.91 19.20 19.50 19.82 20.15 [.09]	18.43 18.72 19.02 19.34 19.67 [.08]	17.95 18.23 18.54 18.85 19.19 [.08]	17.46 17.75 18.05 18.37 18.70 [.08]	16.98 17.27 17.57 17.89 18.22 [.08]	16.50 16.78 17.09 17.40 17.74 [.08]	16.02 16.30 16.60 16.92 17.25 [.09]

#### Table 1.17

Solubility of NaCl (weight percent) in a solution containing 10 weight percent CaCl<sub>2</sub> plus the KCl concentration as given. Data in parentheses, (), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [], for the 0°, 50°, and 100°C isotherms.

emperature		KC1 co	oncentrat	tion in v	veight pe	ercent	
<u>(°C)</u>	<u>0</u>	1	2	3	4	5	<u>6</u>
0	(16.12) [.14]	(15.66) [.14]	(15.20) [.13]	(14.73) [.13]	(14.27) [.13]	(13.81) [.13]	(13.35) [.14]
10 20 30 40 50	(16.32) (16.55) 16.78 17.03 17.30 [.07]	(15.86) (16.08) 16.32 16.57 16.84 [.06]	(15.40) (15.62) 15.86 16.11 16.38 [.05]	(14.94) (15.16) 15.40 15.65 15.92 [.05]	(14.48) (14.70) 14.93 15.19 15.46 [.05]	(14.02) (14.24) 14.47 14.73 14.99 [.05]	(13.55) (13.77) 14.01 14.26 14.53 [.06]
60 70 80 90 100	17.59 17.89 18.20 18.53 18.88 [.09]	17.13 17.43 17.74 18.07 18.42 [.09]	16.66 16.96 17.28 17.61 17.96 [.08]	16.20 16.50 16.82 17.15 17.50 [.08]	15.74 16.04 16.36 16.69 17.04 [.08]	15.28 15.58 15.89 16.23 16.57 [.09]	14.82 15.12 15.43 15.76 16.11 [.09]

#### Table 1.18

Solubility of NaCl (weight percent) in a solution containing 12 weight percent  $CaCl_2$  plus the KCl concentration as given. Data in parentheses, (), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [], for the 0°, 50°, and 100°C isotherms.

remperature	Τe	em	p	e	r	а	tu	r	е	
-------------	----	----	---	---	---	---	----	---	---	--

Т

#### KC1 concentration in weight percent

<u>(°C)</u>	<u>0</u>	1	2	3	4	<u>5</u>
0	(14.26) [.14]	(13.83) [.14]	(13.39) [.13]	(12.96) [.13]	(12.53) [.13]	(12.10) [.14]
$10 \\ 20 \\ 30 \\ 40 \\ 50$	$(14.48) \\ (14.71) \\ 14.96 \\ 15.23 \\ 15.51 \\ [.07]$	(14.05) (14.28) 14.53 14.80 15.08 [.06]	(13.61) (13.85) 14.10 14.36 14.65 [.05]	$(13.18) \\ (13.42) \\ 13.67 \\ 13.93 \\ 14.21 \\ [.04]$	(12.75) (12.98) 13.23 13.50 13.78 [.05]	(12.32) (12.55) 12.80 13.07 13.35 [.05]
60 70 80 90 100	15.81 16.12 16.45 16.80 17.16 [.10]	15.38 15.69 16.02 16.37 16.73 [.09]	14.95 15.26 15.59 15.94 16.30 [.09]	14.51 14.83 15.16 15.50 15.86 [.09]	14.08 14.39 14.72 15.07 15.43 [.09]	13.65 13.96 14.29 14.64 15.00 [.09]

Table 1.19 Solubility of NaCl (weight percent) in a solution containing 14 weight percent  $CaCl_2$  plus the KCl concentration as given. Data in parentheses, (), are extrapolated; the solution may be supersaturated in one or more solid phases other than halite. Precision (3 sigma) is given in brackets, [ ], for the 0°. 50°, and 100°C isotherms.

Т

emperature	KCI	l concent	tration_	in weight	t percen	<u>t</u>
(°C)	0	1	2	3	4	5
0	(12.43) [.15]	(12.04) [.14]	(11.64) [.14]	(11.25) [.14]	(10.85) [.14]	(10.46) [.14]
10 20 30 40 50	(12.67) (12.92) 13.18 13.46 13.76 [.08]	(12.27) (12.52) 12.78 13.07 13.36 [.07]	(11.88) (12.12) 12.39 12.67 12.97 [.05]	(11.48) (11.73) 11.99 12.27 12.57 [.05]	(11.08) (11.33) 11.60 11.88 12.17 [.05]	(10.69) (10.94) 11.20 11.48 11.78 [.06]
60 70 80 90 100	14.07 14.40 14.74 15.10 15.48 [.12]	13.67 14.00 14.35 14.71 15.08 [.11]	13.28 13.61 13.95 14.31 14.69 [.10]	12.88 13.21 13.55 13.91 14.29 [.10]	12.49 12.81 13.16 13.52 13.89 [.10]	12.09 12.42 12.76 13.12 13.50 [.10]

Table 1.20

Total pressure over vapor-saturated solutions in the systems indicated by footnote. The vapor pressure for liquid  $H_2O$  is given in column a. Except for column a, all solutions are saturated in halite (solid NaCl). Precision is given at the bottom of each  $\overline{c}$ olumn. The cited precision is the percent departure from a second- (or third-) order polynomial through the experimental data. Units of pressure are xl0-1 MPa. Composition of the synthetic bittern NBT3 is given in the text

 $\begin{array}{c} 1 & 1 \\ 2 & 17 \\ 2 & 17 \\ 3 & 3 & 18 \\ 3 & 3 & 22 \\ 5 & 3 & 22 \\ 7 & 15 \\ 7 & 15 \\ 7 & 15 \\ 7 & 15 \\ 112 & 01 \\ 112 & 01 \\ 112 & 01 \\ 112 & 01 \\ 112 & 01 \\ 112 & 01 \\ 112 & 02 \\ 112 & 02 \\ 24 & 15 \\$ 0.08 1111 11 1 1 1  $\begin{array}{c} 1.98\\ 2.75\\ 3.54\\ 5.33\\ 5.33\\ 6.42\\ 7.68\\ 7.68\\ 7.68\\ 7.68\\ 7.68\\ 7.93\\ 221.05\\ 221.05\\ 233.20\\ 33.20\\ \end{array}$ 0.10 ļ I 1 L 11 Т 1 1 0.16 1 1 00 T. 41  $\begin{array}{c} 17.88\\ 21.10\\ 24.78\\ 28.96\\ 33.68\\ 38.98\\ 38.98\\ 44.89\\ \end{array}$ 0.16 انە 1111111 I 1 1 1 T 19.54 23.07 23.07 31.54 31.54 42.07 48.18 54.88 0.06 (20 weight percent) (10 weight percent) ١ď | 1 1 1 1 1 1 1 1 1 1 1 1 (saturated)-KC1 (saturated) 0.04 1 υI T 1 1 (saturated)-MgC1<sub>2</sub> (saturated)-MgCl<sub>2</sub> 118.50 131.62 145.71 160.80 176.92 0.09106.31 (saturated)  $\begin{array}{c} 1 & 43 \\ 1 & 99 \\ 2 & 2 & 70 \\ 2$ 1.01 H<sub>2</sub>0-NaCl System H<sub>2</sub>0-NaCl H<sub>2</sub>0-NaCl H,0-NaCl 150 1 System H<sub>2</sub>0 Temperature System System System Precision 1120. 1120. 1120. 1120. 1120. 1120. 1200. 1220. 1200. 1220. 1200. 390. (c)) 400. 10 00 ۱'n JU D नि मि ल मि

(saturated) - KC1  $(saturated) - CaC1_2$  (saturated) - NBT3

(saturated)-KCl (saturated)-NBT3

 $(saturated) - CaSO_{4}^{-}$  (saturated)

(saturated)-NBT3

System H<sub>2</sub>0-NaCl System H<sub>2</sub>0-NaCl

H,0-NaCl

System

H<sub>2</sub>0-NaCl

System

#### Table 1.21

Density of halite saturated solutions in the system  $H_2O$ -Nacl. From reference [122]. System  $H_2O$ -NaCl. The densities above 160°C are extrapolated to the saturation curve from densities measured at lower temperatures and at concentrations at and below 30 wt. percent. The precision between 0° and 110°C is  $0.5 \text{ kg/m}^3$ ; above 110°C the precision is 6 kg/m<sup>3</sup>.

emperature	Concentration	Density
(°C)	(wt. percent)	(kg/m <sup>3</sup> )
0	25.99	1208.9
10.	26.11	1204.5
20.	26.24	1200.1
30.	26.40	1195.8
40.	26.57	1191.5
50.	26.76	1187.2
60.	26.97	1182.9
70.	27.19	1178.7
80.	27.44	1174.4
90.	27.70	1170.3
100.	27.99	1166.1
110.	28.29	1162.0
120.	28.61	1158.
130.	28.95	1153.
140.	29.31	1148.
150.	29.69	1143.
160.	30.10	1138.
170.	30.52	1132.
180.	30.96	1127.
190.	31.42	1122.
200.	31.90	1116.
210.	32.40	1111.
220.	32.93	1106.
230.	33.47	1101.
240.	34.04	1097.
250.	34.62	1092.
260.	35.23	1088.
270.	35.86	1084.
280.	36.51	1080.
290.	37.18	1077.
300.	37.87	1073.

between 100° and 400°C. The precision of the data is given at the bottom of each column. NBT3 is a synthetic bittern having the following composition:

Component	Concentration
KCl	0.200 wt. pct.
$MgCl_2$	9.366
$CaCl_2$	37.821
tal dissolved solids	47.387 wt. pct.

#### 1.7.3. Density

To

The data for the densities of pore fluids are unreliable because the composition and the sampling temperature vary widely. The concentrations are higher than those usually used in research studies on solutions of inorganic salts. Table 1.21 gives the density of halite-saturated solutions as a function of temperature [122]. Pore fluids, containing less dissolved NaCl but more of the other components such as KCl, MgCl<sub>2</sub>, MgSO<sub>4</sub>, or CaCl<sub>2</sub>, would be denser than the fluids in the system  $H_2O-NaCl$  for which data are tabulated.

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#### **Symbols and Units**

Symbol	Name	Unit
р	Density	kg/m <sup>3</sup>
t	Temperature, degrees Celsius	°Č
Т	Temperature, kelvins	K
Р	Pressure, pascals	Pa
$\phi$	Porosity	
m	Permeability	md

#### **Conversion Factors**

Length To convert from feet	to meters	Multiply by 3.048	
Temperature			
To convert from	to	Add	
°C	K	273.15	
Density			
To convert from	to	Multiply by	
kg/m <sup>3</sup>	g/cm <sup>3</sup>	$1 \times 10^{-3}$	
Pressure			
To convert from	to	Multiply by	
MPa	bar	10-1	

\_ \_

2

## Chapter 2

## **Physical and Chemical Properties of Components in Salt Deposits**

## **Reginald P. T. Tomkins\***

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### 2. Physical and Chemical Properties of Components in Salt Deposits

#### 2.1. Introduction

The physical and chemical properties of the components found in salt deposits are presented in this chapter. The concern is largely with the principal constituent of such deposits, namely halite and some of the more common impurities, particularly anhydrite, CaSO<sub>4</sub>; gypsum, CaSO<sub>4</sub>  $\cdot$  2H<sub>2</sub>O; calcite, CaCO<sub>3</sub>; polyhalite, K<sub>2</sub>Ca<sub>2</sub>Mg(SO<sub>4</sub>)<sub>4</sub>  $\cdot$  2H<sub>2</sub>O, and various types of clay minerals.

The properties of chemical variability, density, crystallography, and thermodynamic parameters (entropy, enthalpy of formation and free energy of formation) have been evaluated and are reported herewith. An equation of state has been included if available. An assessment of the chemistry among the components  $H_2O$ -NaCl-CaSO<sub>4</sub>-CaCO<sub>3</sub>-KCl-MgCl<sub>2</sub> was also undertaken. The results for data on aqueous solubility, dehydration reactions, formation of solid solutions and phase diagrams for the systems indicated above are also reported in this chapter. A brief discussion of the techniques used for such measurements, together with remarks on the experimental accuracy, and precision is first given since an appreciation of this is basic to the data tabulations that follow.

#### 2.2. Experimental Techniques

The experimental aspects for property measurements, such as chemical compositions, density, crystallography,

thermodynamic properties, and solubility are considered in this section. References to recommended experimental investigations, in which the various techniques have been used, are included.

#### 2.2.1. Chemical Compositions

Most of the analyses of the components of salt deposits have been performed using atomic absorption spectroscopy. The limits of detection for the analysis of rock salt varied from 0.0025-0.00005 ppm.

An example of the experimental approach is that by Bloomberg [1]. The salt was dissolved in water and allowed to stand overnight, then filtered. The residue was washed with several portions of distilled water and the filter paper and insolubles were dried overnight at 383 K. The paper was separated and ashed, then the residue was added to the ash and the total weighed as insolubles. This portion was ground in an agate mortar and analyzed spectrographically.

The trace elements in the soluble fraction were precipitated with  $H_2S$  from slightly alkaline brine, using high purity lead as a carrier. The precipitate was allowed to settle overnight and was then separated from the alkaline brine by centrifuging, and washed several times with slightly alkaline  $H_2S$ -saturated distilled water. The washed precipitate was then transferred to a crucible, dried at 383 K, and analyzed spectrographically.

#### 2.2.2. Density

Methods available for the determination of the densities of solids are described in detail by Bauer and Lewin [2]. Most of the commonly used methods depend on immersing the solids in some inert fluid of known density. The methods may be conveniently divided into displacement methods (pycnometric, dilatometric) and buoyancy methods (Archimedean principle).

A common displacement method uses a pycnometer where the volume of a known mass of the solid is found by determining the changes in weight when the pycnometer is successively filled with a liquid of known density, solid plus air, and solid plus liquid. With due precautions an accuracy of about  $\pm 0.0005$  or  $\pm 0.1\%$  for the density can be achieved.

Hydrostatic weighing appears to be the most commonly employed buoyancy method, in which the apparent loss of weight is obtained by weighing the solid first in air and then immersed in the liquid. The accuracy of this method is about  $\pm 0.001$  or  $\pm 0.2\%$ . The main difficulty in these methods is that of completely removing all the air trapped by the solid. Variations of up to 5 percent have been obtained for individual crystals taken from the same source.

#### 2.2.3. Crystallography

X-ray diffraction techniques have been used to obtain the crystallographic parameters. The various techniques for determination of the structure of minerals are described by Gr'mshaw [3]. Large crystals are examined by means of a single crystal goniometer, with a Geiger-Müller counter attachment to accurately detect the positions and relative intensities of the spots. Interlattice spacings accurate to  $\pm 10^{-14}$ m are attainable using x-ray methods.

In cases where single crystal specimens are not available a powder sample can be used successfully. Most minerals lend themselves to the powder technique. However, it should be noted that the information obtained from a powder diffraction pattern is less complete compared to the single crystal pattern due to accidental overlap of powder lines with approximately the same Bragg angle. Another problem that is encountered with powder diffraction patterns is the existence of a stronger background leading to the possiblity of some weaker reflections being overlooked.

For measurements at higher pressures Jamieson [4] has described a new technique using "amorphous" boron as a pressure vessel for studies up to  $10^{10}$  pascal pressure. The cell consists of a boron water sandwiched between two carboloy platens. The x-rays are collimated so that the beam traverses the wafer normal to its axis. The use of a Bridgman-anvil high pressure apparatus has been reported by Sato [5], which adapts the x-ray Debye-Scherrer system using a high pressure cell of boron, solidified with a polyester resin. Readings accurate to  $\pm 0.02^{\circ}$  were attainable with this technique. There are two important methods for measuring x-ray intensities. In the photographic or densitometric method,  $I_0$  is the intensity of the incident light scanning the densitometer trace and consequently  $I_0 > I$ . The geiger method involves a direct measurement of x-ray scattering and accomplishes a comparison of the incident and scattered x-ray beam intensities. It is always advisable to check on the technique employed before using the reported values of intensities.

#### 2.2.4. Thermodynamic Properties

The thermodynamic properties have been measured (or derived from) either low temperature adiabatic calorimetry (heat capacities) or combustion bomb calorimetry (heats of combustion). A detailed discussion of these methods is given by Sturtevant [6]. Additional discussion of the precision and accuracy attainable with adiabatic calorimeters is reported by Staveley [7]. Depending on the temperature range the precisions expected for heat capacity data are as follows: 0.7% (10-30 K), 0.2% (30-100 K), and 0.1% (100-300 K). The expected accuracy is about 0.16%.

Heat capacities are obtained using the Nernst method, in which the material under investigation is contained in a metal calorimeter which is equipped with a heater and a temperature measuring device such as a resistance thermometer, thermocouple, or thermistor. The calorimeter is supported inside a jacket of large heat capacity and accurately measurable temperature. The jacket is contained within another vessel, such as a Dewar flask, which is cooled by liquid air or liquid hydrogen. Several adiabatic calorimeters exist in which the jacketcalorimeter temperature difference is kept so small that thermal leakage is negligible.

The enthalpies and free energies of formation reported in this chapter have been obtained from heats of combustion data using bomb calorimetry. Data having an accuracy of a few hundredths of a percent may be obtained using the bomb calorimeter. A detailed description of the bomb calorimeter is given by Sturtevant [6].

The selection of the best values for the thermodynamic parameters has been based on four major critical compilations, namely: The JANAF tables [31], the tabulations of Barin and Knacke [53], the NBS Circular 500 [55], and the U.S. Geological Survey Bulletin [117].

#### 2.2.5. Solubility

Methods for measuring solubilities and phase diagram data have been described concisely by Potter et al. [8]. Three major categories of experimental techniques exist for the determination of the solubility of a salt in an

aqueous solution as a function of temperature. These are quench methods, visual methods, and so-called indirect methods. Quench methods involve separating a representative sample of the saturated solution from the salt crystals at a certain temperature, quickly cooling the separated solution to room temperature, and finally analyzing its salt content using atomic absorption spectrophotometry or titration methods. Studies employing the visual method involving viewing a mixture of solution plus salt crystals plus vapor of known bulk composition as temperature is increased slowly until the last salt crystal dissolves. Solubility is determined with the indirect methods by utilizing changes in the intensive properties of a system of salt crystals plus saturated solution plus vapor of known bulk composition to detect the dissolution of the last salt crystal.

The quench method has been developed to obtain data at higher temperatures than were possible in earlier studies. Basically the modification consists of a "bomb in bomb" method, in which an empty bomb is sealed in a bomb filled with salt crystals plus solution in such a way that the inner bomb can be opened and closed. Some of the difficulties that are encountered with the quench method include density, stratification, super-saturation, analytical problems, precipitation on quench, and the criteria for establishing equilibrium. With the visual method, limiting factors include visibility during heating, density stratification, and the effect of devitrification on the ultimate strength of the glass.

Most of the geological solubility data have been obtained via indirect methods. An example of an indirect method consists of measuring the pressure as a function of volume of a known bulk composition at constant temperature. The dissolution of the last salt crystal is detected by discontinuities in the pressure-volume curves. Another indirect method used for solubility measurements is to measure vapor pressure of the solution as a function of the composition at constant temperature. The composition at which the pressurecomposition curve becomes constant is taken as the solubility of the salt at the temperature of the measurement. A limiting factor (with respect to the accuracy) is the spacing of the compositions; the more closely spaced, the greater the accuracy.

Potter et al. [8] have recently devised a new method for measuring the solubility of simple salts in water at elevated temperatures involving heating assemblages of salt crystals plus solution vapor at a constant rate in a platinum-lined bomb. The dissolution of the last salt crystal is evidenced by a distinct discontinuity in the pressure-temperature curve. The uncertainty of the solubility data obtained by this method was estimated to be  $\pm 0.1$  weight percent of salt. The preceding observations on accuracies and precision of the various techniques are summarized in table 2.1.

#### 2.2.6. Accuracy and Precision

The accuracy estimates are based on experimental details including method of measurement. techniques, analytical characterization of materials and, wherever possible, intercomparisons with results from different investigators. Where precision estimates were advanced by the investigators, these are reported accordingly; where the data were subjected to further analyses, the precisions advanced are based on the statistical analyses.

Temperature-dependent or pressure-dependent equations are reported wherever possible. The statistical analysis was performed on the computer facilities at Rensselaer Polytechnic Institute. The criterion for choosing the equation of best fit using a least-squares one-dimensional analysis is the standard error of estimate defined by

$$s = \frac{\sum_{e=1}^{n} (\gamma_e - \gamma_e)^2}{n - q}$$

where  $\gamma_e$  = the experimental value at each temperature,  $\gamma_c$  = the value calculated from the least squares equation at the same temperature as  $\gamma_e$ , n = the number of experimental data points, and q = the number of coefficients in the least squares equation (2 for linear, 3 for quadratic). Alternatively, in the case of a linear regression analyses, the measure of the precision of the data is  $r^2$ , defined as:

$$r^{2} = \frac{\left[\sum x_{i}y_{i} - \frac{\sum x_{i} \sum y_{i}}{n}\right]^{2}}{\left[\sum x_{i}^{2} - \frac{(\sum x_{i})^{2}}{n}\right]\left[\sum y_{i}^{2} - \frac{(\sum y_{i})^{2}}{n}\right]}$$

where  $x_i$  and  $y_i$  are the data pairs and n the number of data pairs. For an exponential curve fit,  $r^2$  is given by:

$$r^{2} = \frac{\left[\sum x_{i} \ln y_{i} - \frac{1}{n} \sum x_{i} \sum \ln y_{i}\right]^{2}}{\left[\sum x_{i}^{2} - \frac{(\sum x_{i})^{2}}{n}\right] \left[\sum (\ln y_{i})^{2} - \frac{(\sum \ln y_{i})^{2}}{n}\right]}$$

The closer the value of  $r^2$  is to unity the more precise is the data.

Property	Technique	Accuracy	Limits of Precision	Recommended Studies
Chemical composition	atomic absorbtion	0.0025- 0.00005ppm		[1]
Dongity	pycnometric	±0.1%	0.05%	[2]
Density	Archimedean	±0.01%	0.05%	[2]
Crystal- lography	x-ray diffrac- tion	±0.005%	0.002%	[3]
Thermodynamic properties	combustion or adiabatic calorimetry	±0.2%	0.1-0.7%	[6],[7]
	quench methods	±0.5%	0.8%	
Solubility	visual	±0.5%	0.8%	[8]
	indirect (e.g. pressure-com- position	±0.1%	0.5%	

#### Table 2.1. Summary of accuracies and precisions for physical and chemical properties of components in salt deposits

#### 2.3. Physical Properties: Halite

#### 2.3.1. Chemical Variability

The most common insoluble impurities in halite [9] are anhydrite, gypsum, dolomite, calcite, pyrite, quartz, and iron oxides. The most common soluble impurities include the following ions:  $Ca^{+2}$ ,  $Mg^{+2}$ ,  $K^+$ , Cl,  $CO_3^{-2}$ , and  $SO_4^{-2}$ ; in addition,  $Ba^{+2}$ ,  $Sr^{+2}$ ,  $B^{+3}$  and Br may be present in minor amounts. In some deposits associated minerals are present. These minerals include the following:

Sylvite, KCl Carnallite, KMgCl<sub>3</sub>  $\cdot$  6H<sub>2</sub>O Tachydrite, 2MgCl<sub>2</sub>  $\cdot$  12H<sub>2</sub>O Bischofite, MgCl<sub>2</sub>  $\cdot$  6H<sub>2</sub>O Kainite, MgSO<sub>4</sub>  $\cdot$  KCl  $\cdot$  3H<sub>2</sub>O Anhydrite, CaSO<sub>4</sub> Vanthoffite, MgSo<sub>4</sub>  $\cdot$  3Na<sub>2</sub>SO<sub>4</sub> Glaserite, K<sub>3</sub>Na(SO<sub>4</sub>)<sub>2</sub> Langbeinite, 2MgSO<sub>4</sub>  $\cdot$  K<sub>2</sub>SO<sub>4</sub> Syngenite, CaSO<sub>4</sub>  $\cdot$  K<sub>2</sub>SO<sub>4</sub>  $\cdot$  H<sub>2</sub>O Leonite, MgSO<sub>4</sub>  $\cdot$  K<sub>2</sub>SO<sub>4</sub>  $\cdot$  4H<sub>2</sub>O Picromerite, MgSO<sub>4</sub>  $\cdot$  K<sub>2</sub>SO<sub>4</sub>  $\cdot$  6H<sub>2</sub>O Gypsum, CaSO<sub>4</sub>  $\cdot$  2H<sub>2</sub>O Kieserite, MgSO<sub>4</sub>  $\cdot$  7H<sub>2</sub>O  $\begin{array}{l} Glauberite, \ CaSO_4 \ \cdot \ Na_2SO_4 \\ Bloedite, \ MgSO_4 \ \cdot \ Na_2SO_4 \ \cdot \ 4H_2O \\ Loeweite, \ MgSO_4 \ \cdot \ Na_2SO_4 \\ Polyhalite, \ 2CaSO_4 \ \cdot \ MgSO_4 \ \cdot \ K_2SO_4 \ \cdot \ 2H_2O \\ Krugite, \ 4CaSO_4 \ \cdot \ MgSO_4 \ \cdot \ K_2SO_4 \ \cdot \ 2H_2O \end{array}$ 

In natural halite there does not appear to be much replacement of Na by K, although sylvite (KCl) is isomorphous with halite. Moisture is normally present as saturated brine inclusions within the salt crystals. Gas bubbles are sometimes found within the inclusions and consist mainly of air,  $CO_2$  and hydrocarbons. Some typical analyses of halite are listed in table 2.2. These analyses [10] cover samples found in Michigan, New York, Ohio, Louisiana and Kansas, which account for the bulk of production of rock salt in the United States. Commercial rock salt (halite) varies in purity from about 97% (Kansas) to about 99% (Louisiana).

#### 2.3.2. Density

The summary of density values advanced by Doelter and Leitmeier in 1929 [11] still appears authoritative. Later values are given for halite from several sources [12-16] at one temperature with accuracies of about  $\pm 0.1\%$ . The samples varied from recrystallized salt to halite samples from various sources.

	Source							
Comment	USA							
Component	Louisiana	New York	Michigan	Ohio	Kansas			
		Weight	Percent (%)					
NaC1	99.01	98.24	98.08	97.87	97.27			
CaSO <sub>4</sub>	0.84	1.48	1.55	1.84	2.22			
CaCO <sub>3</sub>	0.10	0.05	0.11	0.11				
MgCO <sub>3</sub>	0.01	0.06	0.06	0.06	0.19			
sio <sub>2</sub>	0.02	0.11	0.03	0.04	0.23			
Fe <sub>2</sub> 03	0.00	0.04	0.01	0.01	0.01			
н <sub>2</sub> 0	0.02	0.02	0.16	0.07	0.08			

Table 2.2. Chemical variability of rock salt

Hunt [12] used the buoyancy method with oil of turpentine, whereas Moseley [14] reported the density of halite as part of a calibration experiment for the determination of the x-ray spectra of some elements. Retgers [13] used a carefully calibrated pycnometer for the measurement of density, but no other information was provided. The publications by Spencer [15] and Spannenberg [16] are both review articles. There have been no more recently determined values for the density of halite. In 1960 Kaufmann [17] undertook a further critical assessment of the density data for halite using the references cited in the 1929 compilation. The results of Kaufmann's assessment are recommended as the best values for density of halite. The densities are in table 2.3.

#### 2.3.3. Compressibility

The values of the compressibility of halite are in table 2.4. These are based on the work of Richards and Jones [19] and Slater [20]. Some details of these studies follow.

In the low pressure study by Richards and Jones [19] a Cailletet compression pump was used to attain the pressures and the apparatus was immersed in a constant temperature bath which was maintained at  $\pm 0.005^{\circ}$ C. The essential feature of the method was the comparison of the unknown compressibility with the known compressibility of mercury, by first compressing mercury in a given apparatus, measuring both pressure and change of volume and then displacing most of the mercury by the substance to be studied, and again noting the relationship of pressure to volume. The experiments were performed on both sodium chloride precipitated from reagent grade salt and on two specimens of clear, natural halite. The pressure gauge used in the experiments was calibrated by using the difference between the compressibility of water and mercury at 293 K.

Slate [20] used sodium chloride samples grown from the melt and reported that the error in the values of compressibility at zero pressure was less than 1%. The values obtained for variation with pressure and temperature were stated to be of the order of 5% and 20% respectively.

#### 2.3.4. Crystallography

The crystal symmetry of halite is cubic hexoctahedral; this symmetry class is represented as  $4/m\overline{3}$  2/m[Hermann-Mauguin (International) symbols].

X-ray crystallographic data for halite have been reported by several investigators [22-30]. The radiation sources used in these investigations were either molybdenum [22-24, 27] or copper [25, 28-30]. In view of several discrepancies in the intensities published on the ASTM cards, a critical analysis of existing data was undertaken by Swanson [30] in 1953, together with a redetermination of the crystal parameters using sodium chloride, twice recrystallized from hydrochloric acid. The results are in table 2.5. These values are recommended as the best values.

Table 2.3. Halite:	Density (kg/m <sup>3</sup> )
Т <u>(К)</u>	ρ (±2)
273	2168
283	2165
293	2163
298	2161
303	2160
313	2158
323	2155

Temperature-dependent equation, and precision  $\rho = 2237.2057 - 0.254286 T_{:} (r^{2} = 0.995)$ 

#### 2.3.5. Thermodynamic Properties

Table 2.6 reports the recommended values for the entropies, standard enthalpies of formation, standard Gibbs free energies of formation and standard heat capacities as a function of temperature. These are the values advanced by Stull, Prophet et al. [31] from the JANAF thermochemical tables, and are recommended as the best values. The heat of formation is based on  $\Delta H_{\rm f}^{\circ}$ , 298.15 = -240.12 and -167.15 kJ/mol for Na<sup>+</sup> ( $^{\circ}$ H<sub>2</sub>O) and Cl<sup>-</sup> ( $^{\circ}$ H<sub>2</sub>O), respectively, and on the

heat of solution  $\Delta H^{\circ}_{\infty}$ , 298.15 = 3857.6 J/mol for NaCl.

The heat capacities were obtained by high temperature precision calorimetry [32-42]. Temperature drift was reduced to a value less than  $0.1^{\circ}$ /min during a temperature measurement. Pt/10% Rhodium thermocouples were calibrated against the melting points of NBS samples of lead, tin and zinc. The sample container was fabricated from Pt/10% Rhodium and contained a thermocouple well. The results were estimated to be accurate to  $\pm 0.3\%$  with a standard deviation of 54J/mol.

#### 2.3.6. Equation of State

No information on **an equation** of state is available for halite.

### 2.4. Physical Properties of Major Impurities in Halite

The major impurities in halite considered here are anhydrite, gypsum, calcite, polyhalite and clays. The properties of chemical variability, density, crystallography, thermodynamic properties and equation of state have been evaluated and are reported herewith.

Anhydrite, CaSO₄

#### 2.4.1. Chemical Variability

Anhydrite occurs as a monomineralic rock in many textural varieties and grain sizes [43]. It is found mixed

Low Pressu	ires			
	Temp (K)	Pressure Range Pa/m <sup>2</sup> (x10 <sup>-4</sup> )	βx10 <sup>-3</sup> m2/Pa	Ref.
	273	9.8-1471.0	4.13	[18]
	293	980.7-4903.3	4.11	[19]
	303	0	4.20	[20]
High Press	ures [	21]		
Pres Pa(x	sure (10-7)	<u>в(293 K)</u>	Pressure Pa(x10 <sup>-7</sup> )	β(293 K)
5	50	0.0196	300	0.0932
10	00	0.0371	350	0.1043
15	50	0.0531	400	0.1145
20	0	0.0677	4 5 0	0.1239
2 5	50	0.0810	500	0.1325

Table 2.4. Coefficient of compressibility,  $\beta$ , for halite

Pressure-dependent equation, and precision

 $\beta = 5.2008 \times 10^{-4} + 3.9836 \times 10^{-4} P - 3.4203 \times 10^{-7} P^2 + 1.4663 \times 10^{-10} P^3 (s = 0.10\%)$ 

Table 2.5.	Crystallographic	parameters	for	halite
------------	------------------	------------	-----	--------

Cubic system

5)	s	cer	n					
	а	=	Ъ	=	c =	5.6402x10	-10 <sub>m ±</sub>	0.0001×10 <sup>-10</sup> m
	а	Ŧ	β	=	γ =	90°		
					da		Ip	hk1 <sup>c</sup>
					3.25	58	13	111
					2.82	21	100	200
					1.99	94	55	220
					1.70	)1	2	311
					1.62	28	15	400
					1.41	10	6	400
					1.29	94	1	331
					1.26	51	11	420
					1.15	515	7	422
					1.08	355	1	511
					0.99	69	2	440
					0.95	533	1	531
					0.94	01	3	600
					0.89	17	4	620
					0.86	01	1	533
					0.85	503	3	622
					0.81	.41	2	444

<sup>a)</sup>d is the interlattice spacing, in  $m \times 10^{10}$ .

b) I is the intensity scaled to the strongest line which was assigned a value of 100

c)<sub>hkl</sub> are the Miller indices

(a) 1	Entropy, ent	halpy of formati	ion and free ener	gy of formation
	T(K)	S°(J/mo1 K) (±0.21)	∆H°(kJ/mo1) f(±0.5)	∆G°(kJ/mo1) (±0.5)
	298	72.115	-411.260	-384.212
	300	72.429	-411.107	-384.005
	400	87.228	-413.461	-374.837
	500	99.081	-413.024	-365.229
	600	109.052	-412.352	-355.730
	700	117.729	-411.456	-346.356
	800	125.499	-410.352	-337.136
	900	132.629	-409.064	-328.064
	1000	139.298	-407.593	-319.133

Table 2.6. Thermodynamic parameters for halite

Temperature-dependent equations, and precision

 $S^{\circ} = 47.211 + 0.096428 \text{ T}; (r^2 = 0.982)$  $\Delta G^{\circ}_{f} = -411.863 + 0.093137 \text{ T}; (r^2 = 0.999)$ 

(b) <u>Heat capacity</u> C<sup>o</sup><sub>p</sub>

T(K)	C <sub>p</sub> (J/mo1 K) (±0.2)					
10.0	0.000					
15.0	0.490					
20.0	1.224					
25.0	2.937					
50.0	15.175					
75.0	25.945					
100.0	33.533					
150.0	41.855					
200.0	46.505					
250.0	48.953					
293.0	50.177					
300.0	50.421					
400.0	52.869					
500.0	54.827					
600.0	56.296					
700.0	57.520					
800.0	58.743					
900.0	59.722					
1000.0	60.701					
1074.0	61.436					

Temperature-dependent equation, and precision

 $C_p^{\circ}$  = 47.494881 + 0.013561 T (temp. range 300-1074 K);

 $(r^2 = 0.973)$ 

with calcite, dolomite, magnesite, clay and many other minerals, including halite. Anhydrite frequently occurs in bands alternating with massive fibrous gypsum. Table 2.7 gives the chemical analyses for several samples of anhydrite. It is apparent that only minor variations occur in its composition. Small amounts of strontium and barium sometimes occur replacing calcium; oxides are probably present as impurities and  $H_2O^+$ , when present, is mainly due to the presence of gypsum.

#### 2.4.2. Density

Density data for anhydrite have been reported in two investigations [44, 45]. Both sets of density data for anhydrite are in table 2.8. There is insufficient information for value judgements. No information on the experimental technique or sample preparation was given by Braitsch [44]. Ludwig and Müller [45] used a pycnometer, which was calibrated with n-heptane. Due precautions were taken to eliminate air from the apparatus. The pressure was normal atmospheric pressure.

#### 2.4.3. Crystallography

The unit cell of anhydrite is orthorhombic. The structure of anhydrite is very different from that of the barytes group of sulfates and shows more similarity with the zircon type of structure. Sulfur atoms, (which are at the centers of regular tetrahedra of oxygen) and calcium atoms, lie on the lines of intersection of the two sets of mirror planes. Planes containing evenly spaced Ca and SO<sub>4</sub> ions lie parallel to (100) and (010), whereas layering is not so well defined parallel to (001). X-ray crystallographic data for anhydrite have been reported by several investigators [24, 46-52]. The radiation sources used in these investigations were either molybdenum [24, 46, 51, 52] or copper [47, 50]. In view of several discrepancies in the intensities published on the ASTM cards, Swanson [50] undertook a critical analysis of

	Source							
	USA	Japan		Ger				
Component	Illinois <sup>a</sup>	Kano <sup>b</sup>	USSR-	Stassfurt	Celle	Australia		
		W	eight P	ercent (%)				
SiO <sub>2</sub>	0.50		2.73		0.01			
A1203		0.07	1 0 6		0.07			
Fe <sub>3</sub> 0 <sub>3</sub>	0.10	0.06	1.06	0.04	0.03			
MgO	0.60		0.17		0.03			
CaO	40.86	41.13	39.12	41.22	41.08	40.47		
Sr0			0.00	0.01		0.71		
BaO			0.00			0.05		
Na <sub>2</sub> 0								
к <sub>2</sub> 0				}0.02	}0.07			
so <sub>3</sub>	57.10	58.37	56.63	58.95	58.50	58.94		
co <sub>3</sub>	0.37	0.17						
н <sub>2</sub> 0 <sup>+</sup>	0.69		0.10	0.01	0.04			
H <sub>2</sub> 0 <sup>-</sup>	0.01		0.68			0.40		
Total	100.61	99.75	100.49	100.25	99.76	100.57		

Table 2.7. Chemical variability of anhydrite

<sup>a)</sup> Includes 0.38 NaCl; SiO<sub>2</sub> figure includes insoluble residue.

b) Includes FeS<sub>2</sub> 0.02.

<sup>c)</sup>Fibrous anhydrite, dolomite rock.

Table 2.8.	Density of	anhydrite
Density (kg/m <sup>3</sup> )(±2)	T(K)	Ref.
2960-2980	298	[44]
2920-2950	298	[45]

existing data and redetermined the crystal parameters using calcium sulfate prepared from the reaction between potassium sulfate and calcium chloride solutions, the product being heated at 973 K for 16 hours. Spectrographic analysis showed the following impurities: 0.01 to 0.1% each of Bi, Sr and Ti; 0.001 to 0.01% each of Ag, Al, Fe, Mg, Ni and Sn; 0.0001 to 0.001% each of Ba, Cr, Cu and Pb, and less than 0.0001% of Mn. The values reported by Swanson [50] are recommended as the best values; the results are in table 2.9.

#### 2.4.4. Thermodynamic Properties

The critical assessment of Barin and Knacke [53] is regarded as the most reliable. The results are advanced herewith as the recommended values in table 2.10 for entropies, standard enthalpies of formation, standard Gibbs free energies of formation and standard heat capacities for anhydrite. Temperature dependent equations and precisions are also included in table 2.10. For earlier studies, refer to references [54–57].

#### 2.4.5. Equation of State

Müller and Siemes [114] carried out compression tests to examine the dependence of strength, ductility, and preferred orientation of polycrystalline anhydrite upon confining pressure (up to 5 kbar), temperatures (up to 300°C) and strain (up to 30%). It was observed that as the mantle pressure was increased at room temperature the strength and the ductility increased. Anhydrite was found to be brittle up to 1 kbar with failure occurring by tension and shear fractures. Between 1 and 3 kbar pressure homogeneous flow occurs, this being due to intercrystalline slip which is sensitive to pressure. Beyond the elastic limit it was found that the stressstrain curves were nearly horizontal, with no preferred orientation developing. However, the intracrystalline mechanisms become noticeable between 3 and 4 kbar. Under these conditions the stress-strain curves show a weak strain hardening and the (210) planes exhibit a weak preferred orientation perpendicular to the axis of compression.

As the temperature is increased the strength of anhydrite decreases at low strains (< 5%), and intracrystalline mechanisms become more dominant. At high strains (> 15%) both strength and ductility increase at

Orthorhombic system

 $a = 6.238 \times 10^{-10} m$ ;  $b = 6.991 \times 10^{-10} m$ ;  $c = 6.996 \times 10^{-10} m$ (±0.0001×10<sup>-10</sup>)

$\beta = \gamma = 90^{\circ}$		
d <sup>a</sup>	Ip	hk1 <sup>C</sup>
3.873	6	111
3.498	100	002,020
3.118	3	200
2.849	33	210
2.797	4	121
2.473	8	022
2.328	22	202,220
2.208	20	212
2.183	8	103
2.086	9	113
1.993	6	301
1.938	4	222
1.869	15	230
1.852	4	123
1.749	11	004
1.748	10	040
1.648	14	232
1.594	3	133
1.564	5	024,042
1.525	4	204,240
1.515	1	313, <b>331</b>
1.490	5	214
1.424	3	402,420
1.418	1	323
1.398	3	242
1.396	2	412
1.365	1	143
1.319	4	422
1.296	2	430
1.277	5	234
1.237	2	044
1.216	4	432
1.1993	2	252
1.1781	< 1	135
1.1663	4	006
1.1651	1	060
1.1483	1	414
1.1062	5	026
1.1044	4	424,442
1.0785	2	216

a) d is the interlattice spacing, in  $m \times 10^{10}$ .

b) I is the intensity scaled to the strongest line which was assigned a value of 100.

c)hkl are the Miller indices.

T(K)	S°(J/mo1 K) (±0.2)	∆H°(kJ/mo1) (±0.5)	∆G°(kJ/mo1) f(±0.5)	C <sub>p</sub> (J/mo1 K) (±0.2)
298	106.692	-1434.110	-1321.696	99.646
300	107.307	-1434.418	-1320.803	99.830
400	137.382	-1436.727	-1282.908	109.704
500	162.920	-1437.948	-1244.262	119.579
600	185.594	-1438.205	-1205.527	129.453
700	206.292	-1437.601	-1166.775	139.327
800	225.543			149.201
900	243.685			159.076
1000	260.956			168.950

Table 2.10. Thermodynamic properties of anhydrite

Temperature-dependent equations and precisions

S°	=	46.736846 +	0	.2211239	T	; $(r^2)$	=	0.	.992)
∆G°f	=	-1436.80866	+	0.38549	57	T; (:	r <sup>2</sup>	=	0.999)
$C_n^{\circ}$	=	70.206518 +	0	.048744	Τ;	(r <sup>2</sup>	=	1.	.000)

higher temperatures. As the strain is increased further, strain hardening ceases once again and the stress-strain curves become nearly horizontal.

Gypsum,  $CaSO_4 : 2H_2O$ 

#### 2.4.6. Chemical Variability

Gypsum shows very little variation in chemical composition. Table 2.11 gives the analyses of several samples of gypsum [43]. Most gypsum deposits contain clay minerals and fine sands as well as chemical sediments such as limestones and dolomites.

#### 2.4.7. Density

Density data for gypsum have been reported in two studies [45, 58]. There is insufficient information for value judgements. No information on the experimental technique or sample preparation was given by Appleyard [58]. Ludwig and Muller [45] used a pycnometer, which was calibrated with n-heptane. Due precautions were taken to eliminate air from the apparatus. In both cases the measurements were at room temperature. The pressure was normal atmospheric pressure. Both sets of density data for gypsum are in table 2.12.

#### 2.4.8. Crystallography

The crystal structure of gypsum was determined by Wooster [59] from two dimensional x-ray diffraction data with Fourier methods. It was further refined by Atoji and Rundle [60] using neutron diffraction data. Gillery [61] undertook a further refinement of the crystallographic data, the details of which are in agreement with conclusions drawn by other workers from spectroscopic data. The values advanced by Gillery [61] are regarded as the best values and are given in table 2.13.

#### 2.4.9. Thermodynamic Properties

The critical assessment of Barin and Knacke [53] is considered still to be valid. The results are advanced herewith as the recommended values in table 2.14 for the entropies, standard enthalpies of formation, standard Gibbs free energies of formation and standard heat capacities for gypsum. Temperature dependent equations and precisions are also included in table 2.14. For earlier studies refer to [62].

#### 2.4.10. Equation of State

Heard and Rubey [115] have examined the stressstrain behavior of gypsum. The effect of dehydration on the strength of gypsum was investigated because of the known occurence of evaporites along many thrust faults. A series of stress-strain curves were obtained at a 5 kbar confining pressure and at different temperatures. The resulting curves showed large reductions in strength over a relatively narrow temperature range  $(100^{\circ}-150^{\circ}C)$ , which was attributed to the transformation of gypsum to metastable hemihydrate (anhydrite plus water). The stress-strain data at 2 kbar confining pressure showed identical results but at slightly lower

	Source					
Component	U.	ş.A.	Germany	US	SR	
component	Illinois <sup>a</sup>	Illinois <sup>b</sup>	Neutershausen <sup>C</sup>	Zaleschiki <sup>d</sup>	Zaleschiki <sup>e</sup>	
	Weight Percent (%)					
Si0 <sub>2</sub>	1.46	0.68				
A1203	0.16	0.18	0 11			
Fe <sub>2</sub> 0 <sub>3</sub>	0.10	0.18	0.11			
MgO	1.14	0.28	0.09			
CaO	33.64	32.76	32.08	33.30	32.36	
so3	45.88	45.88	45.37	45.30	46.00	
co2	2.04	0.28	0.95	1.26	0.28	
11 <sub>2</sub> 0 <sup>+</sup>	16.04	20.23	20.10	19.74	20.82	
н <sub>2</sub> 0 <sup>-</sup>	0.01	0.01				
Total	100.71	100.99	98.88	99.69	99.62	

#### Table 2.11. Chemical variability of gypsum

<sup>a)</sup>St. Louis limestone.

<sup>b)</sup>St. Louis limestone.

d) Coarse-grained gypsum, (Includes 0.09

c) Includes SrO 0.08, (Na<sub>2</sub>0 +  $K_2$ 0) 0.06, Cl 0.04. e) Fine-grained gypsum, (Includes 0.16 resi-

residue).

due).

 Table	2.12.	Density	of	gypsum

Density (kg/m <sup>3</sup> )	T(K)	Ref.
2320-2330	298	[45]
2200-2400	298	[58]

temperatures. In addition it was observed that with increased preheating periods  $(80^\circ - 130^\circ C)$  and a thousand-fold decrease in the strain rate (to  $3 \times 10^{-7} s^{-1}$ ) the strength sensitive region was depressed further.

Calcite, CaCO3

#### 2.4.11. Chemical Variability

Some analyses of calcite [43] to show compositional variations are given in table 2.15. A common substitution is that of Mg for Ca giving magnesian calcites. Barium and strontium may also substitute for calcium in calcite. Although many divalent cations may partially replace Ca in calcite, most calcite is relatively free from other ions and is fairly close in composition to pure CaCO<sub>3</sub>.

#### 2.4.12. Density

The value for the density of calcite reported by Humbert and Plicque [63] was calculated from x-ray diffraction data. There is insufficient information for a value judgement. No information was provided on sample preparation. The value reported is given in table 2.16.

#### 2.4.13. Crystallographic Properties

The crystallographic structure of calcite is analogous to that of halite, where the Na and Clions are replaced by Ca and CO<sub>3</sub> ions, respectively, and the unit cell is distorted by compression along a triad axis to yield a facecentered rhomobohedral cell. X-ray crystallographic data for calcite have been reported by several investigators [24, 25, 64–68]. The radiation sources used in these investigations were either molybdenum [25, 64, 66] or copper [24, 68]. In view of several discrepancies in the intensities published on the ASTM cards, a critical analysis of existing data was undertaken by Swanson [68] in 1953, together with a redetermination of the crystal parameters of calcite. These values are recommended as the best values and the results are in table 2.17.

#### 2.4.14. Thermodynamic Properties

The critical assessment of Barin and Knacke [53] is regarded as the most reliable. The results are advanced herewith as the recommended values in table 2.18 for the entropies, standard enthalpies of formation, standard Gibbs free energies of formation and standard heat

с	system			
-	5.68x10 <sup>-10</sup> m; b	= 15.18×10 <sup>-</sup>	10  m;  c = 6.51  x 10	-10 <sub>m</sub>
=	$\gamma = 90^{\circ}; \beta = 11$	8°23′		
	_ d <sup>a</sup>	I b	hkl <sup>c</sup>	
	7.56	100	020	
	4.27	51	121	
	3.79	21	031,040	
	3.163	3	112	
	3.059	57	14ī	
	2.867	27	002	
	2.786	5	211	
	2.679	28	022,051	
	2.591	4	150,20Ž	
	2.530	<1	060	
	2.495	6	200	
	2.450	4	222	
	2.400	4	141	
	2.216	6	152	
	2.139	1	242	
	2.080	10	123	
	2.073	8	112,25Ī	
	1.990	4	170	
	1.953	2	211	
	1.898	16	080,062	
	1.879	10	143	
	1.864	4	312	
	1.843	1	231	
	1.812	10	262	
	1.796	4	321	
	1.778	10	260	
	1.711	1	253	
	1.684	1	323	
	1.664	4	34Ī	
	1.645	2	163	
	1.621	6	204,181,053	
	1.599	<1	352,190	
	1.584	2	224	
	1.532	1	282	
	1.522	1	222,134	

Table 2.13. Crystallographic parameters for gypsum

Monoclini

a α

<sup>a)</sup>d is the interlattice spacing, in  $m \times 10^{10}$ .

b) I is the intensity scaled to the strongest line which was assigned a value of 100.

c) hkl are the Miller indices.

T(K)	S°(J/mol K) (±0.2)	∆H°(kJ/mol) f(±0.5)	∆G°(kJ/mol) (±0.5)	C <sub>p</sub> (J/mol K) p(±0.2)
298.15	193.970	-2022.628	-1797.197	250.521
300	195.523	-2022.023	-1796.024	250.705
400	268.998	-2041.700	-1746.756	260.580
500	328.206	-2068.548	-1699.288	270.454
600	378.384	-2088.364	-1653.940	280.328
700	422.341	-2110.387	-1610.566	290.202
800	461.738			300.076
900	497.649			309.951
1000	530.816			319.825

Table 2.14. Thermodynamic properties of gypsum

Temperature-dependent equations and precisions

 $S^{\circ} = 68.397727 + 0.48417 \text{ T}; (r^{2} = 0.983)$   $\Delta G_{f}^{\circ} = -1934.894425 + 0.46659241 \text{ T}; (r^{2} = 0.999)$  $C_{p}^{\circ} = 221.08187 + 0.098743 \text{ T}; (r^{2} = 1.000)$ 

Tubic 2.15. Chemical variability of calcice	Table	2.15.	Chemical	variability	of	calcite
---	-------	-------	----------	-------------	----	---------

	Source					
Component	Australia Mariatrost <sup>a</sup>	Poland <sub>b</sub> Vistura <sup>b</sup>	Rujevac <sup>C</sup>	Japan Hokkaido <sup>d</sup>		
	Weight Percent (%)					
MgO	0.04		1.13	0.32		
FeO	0.00			0.29		
MnO	tr.			3.19		
CaO	55.92	54.56	54.43	52.83		
NiO			0.65			
co2	43.95	44.37	44.13	42.78		
Total	99.91	100.08	100.58	99.91		

a)Colorless or pale yellowish calcite.

- <sup>b)</sup>Calcite, occurring as "rock-milk" (lublinite), (Includes  $Fe_2O_3 + Al_2O_3 0.18$ , insol. 0.76, ign. loss 0.21).
- c)Ni-Mg calcite, as yellowish or greenish rhombohedra associated with altered serpentine and marble, (Includes Al<sub>2</sub>O<sub>3</sub> 0.11, insol. 0.13).

d)Pale pink manganoan calcite, (Includes insol. 0.50).

Table 2.16.	Density	ot	calcite	
Density (kg/m <sup>3</sup> )	T(K)			Ref.
2712	299			[63]

capacities for calcite. Temperature-dependent equations and precisions are also included in table 2.18. For earlier studies, refer to [54-57].

#### 2.4.15. Equation of State

Vaidya et al. [116] examined the compressibility of calcite up to 45 kilobars pressure. The data were fitted to an equation of the form:

 $V/V_0 = a_0 + aP + bP^2 + cP^3 + dP^4$ 

where V is the volume of the material at a given pressure and  $V_0$  the volume at normal atmospheric pressure.

The values of the coefficients obtained in this study for the pressure range 0–15 kbar were  $a_0 = 0$ ;  $a \times 10^4 =$ 7.906;  $-b \times 10^5 = 14.580$ ;  $c \times 10^7 = 58.756$ ; and for the pressure range 20–45 kbar were  $a_0 = 0.02814$ ;  $a \times 10^4 =$ 28.653;  $-b \times 10^5 = 3.177$ ;  $c \times 10^7 = 1.205$ .

Polyhalite,  $K_2Ca_2Mg(SO_4)_4 \cdot 2H_2O$ 

#### 2.4.16. Chemical Variability

The main impurity in polyhalite is Kieserite (MgSO<sub>4</sub>  $\cdot$  H<sub>2</sub>O). An analysis of a polyhalite-Kieserite rock [69] is given in table 2.19. When polyhalite is heated to 573 K it loses its water of hydration and the residual salts form a heterogeneous mixture comprising at least two phases.

#### 2.4.17. Density

Density data for polyhalite have been reported in two studies [44, 70]. There is insufficient information for value judgements. No information on the experimental technique, sample preparation or temperature range was given in either study. Both sets of density data for polyhalite are in table 2.20.

#### 2.4.18. Crystallography

X-ray crystallographic data for polyhalite have been reported by several investigators [71-73]. In view of the discrepancies occurring in the earlier studies, a critical analysis of existing data was undertaken by Braitsch [71] in 1961 together with a redetermination of the crystal parameters of polyhalite using more carefully designed optical orientation methods. These values are recommended as the best values. The results are in table 2.21.

#### 2.4.19. Thermodynamic Properties

No information is available on the thermodynamic properties of polyhalite.

#### 2.4.20. Equation of State

No information is available on the equation of state for polyhalite.

#### Clays

The main types of sheet silicates found in salt deposits are talc, Mg<sub>3</sub>Si<sub>4</sub> O<sub>10</sub> (OH)<sub>2</sub>; chlorites; amesite, (Mg<sub>2</sub> Al) (Al,Si)<sub>2</sub> O<sub>5</sub> (OH)<sub>4</sub>; daphnite, (Fe<sub>2</sub>Al) (Al,Si)<sub>2</sub> O<sub>5</sub> (OH)<sub>4</sub>; penninite, (Mg, Fe, Al)<sub>3</sub> (Al, Si)<sub>2</sub> O<sub>5</sub> (OH)<sub>4</sub>; corrensite (chlorite-vermiculite clay mineral); and muscovite, KAl<sub>2</sub>(AlSi<sub>3</sub>)O<sub>10</sub>(OH)<sub>2</sub>; and serpentines (antigorite, Mg<sub>3</sub>Si<sub>2</sub>O<sub>5</sub>(OH)<sub>4</sub>; ferroantigorite, Fe<sub>3</sub>Si<sub>2</sub>O<sub>5</sub>(OH)<sub>4</sub>); chrysotile, Mg<sub>3</sub>Si<sub>2</sub>O<sub>5</sub>(OH)<sub>4</sub>). The properties of chemical variability, density, crystallographic parameters, thermodynamic data, and equation of state are reported for the clay minerals given above.

#### 2.4.21. Chemical Variability

The principal impurities in talc are carbonates (magnesite, breunnerite), chlorites, and quartz. An analysis of a talc-carbonate rock [74] is given in table 2.22.

Chlorite is the predominant clay mineral of many salt clays and many chloridic salt rocks. There are two varieties: normal chlorite (penninite-clinochlorite group) and chlorite (amesite-berthierite group). Both forms are normally found together. The chemical composition of dioctahedral chlorite [75] is given in table 2.23.

Corrensite is the predominant clay mineral in rock salt. It is always associated with varying amounts of a penninite-like chlorite.

Muscovite strongly predominates in the carbonate part of the salt clays, but in the noncarbonate salt clays its abundance relative to the other clay minerals diminishes.

#### 2.4.22. Density

Grimshaw [3] has determined the density of several clay minerals using a pycnometric technique. There is insufficient information provided for value judgments. The density data are in Table 2.24.

#### 2.4.23. Crystallography

Grimshaw [3] undertook a critical analysis of existing data in 1971 and the values advanced in that study are still considered to be authoritative. The values reported by Grimshaw [3] include the three principal lines and are

Table 2.17.	Crystallog	raphic	parameters	for	calcite
-------------	------------	--------	------------	-----	---------

Rhombohedral axes and hexagonal axes

a =  $4.989 \times 10^{-10}$  m; c =  $17.062 \times 10^{-10}$  m (±0.001×10<sup>-10</sup>)

 $\alpha = \beta = \gamma = 90^{\circ}$ 

1 50	ь	C
d <sup>a</sup>	I D	hkl
3.86	12	102
3.035	100	104
2.845	3	006
2.495	14	110
2.285	18	113
2.095	18	202
1.927	5	204
1.913	17	108
1.875	17	116
1.626	4	211
1.604	8	212
1.587	2	1.0.10
1.525	5	214
1.518	4	208
1.510	3	119
1.473	2	215
1.440	5	300
1.422	3	0.0.12
1.356	1	217
1.339	2	2.0.10
1.297	2	218
1.284	1	306
1.247	1	220
1.235	2	1.1.12
1.1795	3	2.1.10
1.1538	3	314
1.1425	1	226
1.1244	<1	2.1.11
1.0613	1	2.0.14
1.0473	3	404
1.0447	4	138
1.0352	2	0.1.16,1.1.1
1.0234	<1	1.2.13
1.0118	2	3.0.12
0.9895	<1	231
0.9846	1	322
0.9782	1	1.0.17
0.9767	3	2.1.14
0.9655	2	234

<sup>a)</sup> d is the interlattice spacing, in  $m \times 10^{10}$ .

b) I is the intensity scaled to the strongest line which was assigned a value of 100.

c) hkl are the Miller indices.

T(K)	S°(J/mol K) (±0.2)	$\Delta H^{\circ}_{f(kJ/mol)}_{(\pm 0.5)}$	∆G°(kJ/mol) (±0.5)	C°(J/mo1 K) p(±0.2)
298.15	92.885	-1207.370	-1128.842	
300	95.324	-1206.871		
323				86.734
400	115.035	-1206.301	-1102.155	97.073
500	137.633	-1204.822	-1076.292	105.102
600	157.293	-1203.276	-1050.723	110.466
700	174.640	-1201.719	-1025.427	114.570
800	190.171	-1201.145	-1000.238	118.001
900	204.246	-1199.789	-975.195	121.047
1000	217.145	-1198.689	-950.299	123.846
1100	229.074			126.491
1200	240.191			129.022

Table 2.18. Thermodynamic properties of calcite

Temperature-dependent equations and precisions

 $S^{\circ} = 51.38356 + 0.1652209 T;$  (r<sup>2</sup> = 0.986)  $\Delta G_{f}^{\circ} = -1203.759955 + 0.2541190 T;$  (r<sup>2</sup> = 0.999)  $C_{p}^{\circ} = 80.3668348 + 0.0436905;$  (r<sup>2</sup> = 0.925)

#### Table 2.19. Analysis of polyhalite-Kieserite rock

### Table 2.20. Density of polyhalite

Mineral	% Composition
Polyhalite	85.2
Kieserite	3.6
Magnesite	4.4
Dolomite	0.2
Halite (from excess chlorine)	1.3
Siliceous material	5.3
	100.00

Density	
$(kg/m^3)$	Ref.
2780	[44]
2800	[70]

Triclinic system

a =  $6.962 \times 10^{-10}$  m; b =  $6.974 \times 10^{-10}$  m; c =  $8.967 \times 10^{-10}$  m (±0.001×10<sup>-10</sup>)

 $\alpha = 104.5^{\circ}; \beta = 101.5^{\circ}; \gamma = 113.9^{\circ}$ 

d <sup>a</sup>	Ip	hk1 <sup>C</sup>
6.0	12	100
5.95	8	011
5.82	6	110
4.802	6	111
4.15	4	012
4.04	2	102
3.48	6	210,121
3.406	12	211
3.353	2	021,201
3.175	70	211
2.97	6	102
2.943	12	220
2.912	100	012
2.89	100	012
2.846	16	103
2.766	4	111,113
2.404	6	222,123
2.350	б	Ī22
2.334	6	222 <b>,</b> 213
2.25	4	120,123
2.213	4	130,103
2.18	4	014,013
2.035	4	004
1.948		214
1.904	6	331,214
1.897	6	222
1.873	6	322,233
1.859	4	221
1.810	6	232
1.806	6	323

a) d is the interlattice spacing, in  $m \times 10^{10}$ .

c) hkl are the Miller indices.

b) I is the intensity scaled to the strongest line which was assigned a value of 100.

Component	Weight Percent (%)	Component	Weight Percent (%)
sio <sub>2</sub>	31.04	Ti0 <sub>2</sub>	0.08
MgO	35.15	CaO	0.23
A1203	0.54	к <sub>2</sub> о	0.01
Fe <sub>2</sub> 0 <sub>3</sub>	3.02	Na <sub>2</sub> 0	0.01
FeO	4.32	Cr <sub>2</sub> 0 <sub>3</sub>	0.33

Table 2.22. Chemical analysis of talc

Table 2.23.	Chemical	analysis	of	chlorite	
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Component	Weight Percent (%)	Component	Weight Percent (%)
si0 <sub>2</sub>	35.63	CaO	1.13
TiO <sub>2</sub>		Na <sub>2</sub> 0	0.24
A1203	34.87	к <sub>2</sub> 0	0.46
Fe <sub>2</sub> 0 <sub>3</sub>	5.01	Н <sub>2</sub> О	1.91
FeO	0.43	Ign. loss.	12.24
MnO	0.05	S	
MgO	8.63		

#### Table 2.24. Density of clay minerals

Clay	Density kg/m <sup>3</sup> (±2)
talc	2750
antigorite	2570
amesite	2800
daphnite	3000
ferro-antigorite	3200
penninite	2700
chrysotile	2550
muscovite	2900

recommended as the best values; the results are in table 2.25.

#### 2.4.24. Thermodynamic Properties

Robie et al. [117] has tabulated the thermodynamic parameters for several sheet silicates. In addition Tardy and Garrels [118] have discussed a method of estimating the Gibbs energies of formation of layer silicates. The thermodynamic parameters for a selection of sheet silicates are given in table 2.25A.

#### 2.4.25. Equation of State

No information on equation of state is available for the clay minerals.

Table 2.25. Crystallographic parameters for clays

Clay	Crystal System	d <sup>a</sup>	Ip
talc	monoclinic	9.30	80
		3.10	100
		1.53	80
antigorite	orthorhombic	7.14	90
		3.59	100
		2.52	70
amesite	monoclinic	7.00	100
		3.50	100
		2.47	90
daphnite	monoclinic	6.9	80
		3.51	100
		4.69	50
ferro-	monoclinic	7.12	100
antigorite		3.50	100
		2.63	40
penninite	monoclinic	14.30	60
		7.17	100
		4.78	100
chrysotile	orthorhombic	7.07	40
		3.59	100
		2.45	60
muscovite	monoclinic	9.98	100
		3.33	90
		2.57	100

### Table 2.25. Crystallographic parameters for clays

a) d is the interlattice spacing, in  $m \times 10^{10}$ 

b) I is the intensity scaled to the strongest line which was assigned a value of 100
Substance	Т(К)	S°(J/mol K) (±0.2)	∆H <sup>°</sup> <sub>f</sub> (kJ/mo1) (±0.5)	∆G°(kJ/mo1) (±0.5)	C°(J/mol K) (±0.2)
ſalc	298.15	260.83	-5915.900	-5536.048	321.70
4g3Si4010(OH)2	400	365.30	-5917.050	-5405.971	386.59
	500	455.61	-5914.990	-5278.425	420.63
	600	534.40	-5911.596	-5151.383	444.26
	700	604.91	-5906.844	-5024.997	475.20
	800	669.80	-5898.951	-4898.009	525.95
	`empera	ature-depende	nt equations an	nd precisions	
	S° = 36	5.46201 + 0.8	$101748 \text{ T} (r^2 =$	0.992)	
	$\Delta G_f^\circ = -5$	914.45145 '+ 1	.27097788 T; (1	$r^2 = 0.999$ )	
	$C_p^{\circ} = 22$	23.666881 + 0	.3736424 T; (r	<sup>2</sup> = 0.977)	
Chrysotile	298.15	221.30	-4361.660	-4034.024	273.70
tg <sub>3</sub> Si <sub>2</sub> 0 <sub>5</sub> (OH) <sub>4</sub>	400	309.13	-4362.729	-3921.820	323.22
	500	385.05	-4360.883	-3811.788	356.33
	600	452.14	-4357.294	-3702.258	378.95
	700	511.78	-4352.759	-3593.454	394.26
	800	565.13	-4347.832	-3485.318	404.32
	900	613.14	-4342.911	-3377.752	410.47
	Tempera	ature-depende	nt equations a	nd precisions	
	$S^{\circ} = 4$	8 9012637 + 0	6467995 T. (r	2 = 0.990	
	$AC^{\circ} = -4$	357 940316 +	1 00075860 T (	$r^{2} = 0.000$	
	40 f - 4.	337.940310 +	1.090/5800 1 (	2 0.999)	
	р				
Muscovite KA1 <sub>2</sub> [A1Si <sub>3</sub> 0 <sub>10</sub> ](0H	1) <sub>2</sub> 298.1	5 306.40	-5976.740	-5600.671	326.10
	400	411.12	-5981.048	-5471.333	385.54
	500	501.73	-5979.503	-5344.043	425.67
	600	582.02	-5975.746	-5217.261	454.42
	700	653.74	-5970.644	-5091.248	475.56
	800	718.32	-5964.809	-4965.994	491.35
	900	776.92	-5958.697	-4841.485	503.24
	Tempe	rature-depend	lent equations	and precision	15
	S° =	98.64806443 +	- 0.776464288 T	$r^2 = 0.990$	))
	∧G° = -	5975.82273 +	1.26215765 T:	$(r^2 = 0.999)$	,
	$^{20}f = $	267 805767 +	0 28280067 T.	$(r^2 - 0.939)$	
	р —	207.003707	0.2020007 1,	(1 = 0.929)	
Pyrophyllite	208 1	5 239 40	- 5643 300	5260 784	207 70
2014 10 001/2	400.1	274 14	- 5045.500	-5209.584	293.70
	400	334.16	-5645.141	-5141.250	349.62
	500	416.33	-5643.939	-5015.389	386.06
	600	489.17	-5640.906	-4889.921	412.41
	700	554.32	-5636.692	-4765.087	432.59
	800	613.17	-5631.707	-4640.892	448.71
	800  Tempe	613.17 rature-depend	-5631.707	-4640.892 and precision	448.71
	800 Tempe S° =	613.17 rature-depend 33.39804167	-5631.707	-4640.892 and precision $r (r^2 = 0.993$	448.71
	800 Tempe S° = ΔG° =	613.17 rature-depend 33.39804167 +	-5631.707 lent equations • 0.741676925 T • 1.25281441 T •	-4640.892 and precision ; (r <sup>2</sup> = 0.993 (r <sup>2</sup> = 0.993)	448.71 15 5)

Table 2.25A.	Thermodynamic	properties	of	sheet	silicates

# 2.5. Chemical Properties Among Components in Salt Deposits

The chemistry among components in salt deposits includes data on aqueous solubility, dehydration reactions, formation of solid solutions and vapor phases and includes phase diagrams.

### 2.5.1. The Systems NaCl-KCl-MgCl<sub>2</sub>-H<sub>2</sub>O

The determination of the solubility of sodium chloride in water has been the subject of several investigations [8, 76-80]. The earlier measurements were subject to an error of  $\pm 0.1$  weight percent of salt below 373 K and  $\pm 0.3$ weight percent salt above 373 K. Potter et al. [8] undertook a redetermination of the solubility using a specially designed bomb lined with platinum (see section 2.2.5) and attained a precision of  $\pm 0.01$  or  $\pm 0.1$  weight percent of salt over the entire temperature range. A comparison of the solubilities obtained by various investigators is shown in figure 2.1. The data reported by Potter et al. [8] have been reanalyzed and values of the solubility of sodium chloride at rounded temperatures are advanced as recommended values in table 2.26, together with a temperature-dependent equation.

A temperature-composition phase diagram for the  $NaCl-H_2O$  system is shown in figure 2.2. As indicated three solid phases exist in this system namely: NaCl,

NaCl  $\cdot 2H_2O$  (hydrohalite) and ice. The solubility of NaCl increases slightly with increasing pressure, reaching a maximum at about 4053  $\times 10^2$  Pa and decreases slowly until at around 1266562 Pa it has the same value as at atmospheric pressure. At 298 K between 800467 and 1175370 pascals hydrohalite is the stable form. A temperature-pressure-composition model for the NaCl-H<sub>2</sub>O system is presented in figure 2.3.

This figure shows the compositions of gas in equilibrium with solid, the melting surface with coexisting gases, liquids, and solids, the envelope of curves relating the composition of the two fluid phases and the critical composition and pressure for each temperature studied. The system was studied to pressures of 1240 bars and through the temperature interval 250-700°C.

The temperature coefficient for the solubility of KCl in water is strongly positive and this effect is also found for the NaCl-KCl-H<sub>2</sub>O system as shown in figure 2.4. The addition of similar ions reduces the actual solubility but has no marked effect on the temperature coefficient. The solubility of NaCl in the presence of KCl is similarly reduced and in fact below 373 K the temperature coefficient for the solubility of NaCl becomes negative. Absolute solution concentrations can be gained using figure 2.4 directly for this system. At any given temperature the unsaturated solutions lie between the



FIGURE 2.1. A comparison of the solubilities of sodium chloride in water.

zero point and the appropriate isotherm. At points P and N in figure 2.4, there are five phases: i.e., solid phases.

P: halite, hydrohalite, sylvite

N: hydrohalite, sylvite, ice and at both points also liquid solution and vapor phases.

When the solution is evaporated the composition changes linearly. For example sylvite precipitates first when at 20°C the point a is reached. On further evaporation point b is eventually attained. After this NaCl and KCl precipitate simultaneously and the composition of the solution remains constant. At 60°C, NaCl precipitates (point c) and the solution composition changes along the 60° isotherm in the direction of a lower NaCl concentration. After reaching the curve RP (at point d) the concentration remains constant until completely evaporated.

The four component system NaCl-KCl-MgCl<sub>2</sub>-H<sub>2</sub>O is characterized by the existence of a ternary compound, carnallite, KCl  $\cdot$  MgCl<sub>2</sub>  $\cdot$  6H<sub>2</sub>O. In figure 2.5 are the solubility isotherms for KCl at various temperatures and the NaCl isotherm at 293 K. In this figure the carnallite isotherms have been extrapolated using the saturation concentrations at the boundaries between the sylvite and bischofite fields. Figures 2.6 and 2.7 present information on the temperature coefficients of solubility of NaCl at

Solubility of

different temperatures at either KCl+NaCl saturation or as a function of  $MgCl_2$  concentration. It is observed that the temperature coefficient of solubility is negative at low  $MgCl_2$  concentrations, while at medium and high concentrations it is positive. Also from about 50 mol  $MgCl_2/1000$  mol  $H_2O$  it remains approximately constant and independent of temperature.

#### 2.5.2. The System Anhydrite-Water-NaCl

Several studies have been undertaken on the solubility of anhydrite in water [82-88]. With the exception of two studies [85, 87], all of the previous work was carried out at atmospheric pressure at temperatures above 373 K or at the vapor pressure of the system at temperatures above 373 K.

Dickson, Blount and Tunell [82] used a special hydrothermal solution apparatus to determine the solubility of anhydrite in water from 373 K to 548 K and from 10<sup>5</sup> to 10<sup>8</sup> pascals pressure. The equipment consisted of a deformable teflon sample cell held in a stainless steel pressure vessel and sealed in such a way as to prevent interchange of material between the sample cell and the steel bomb. Liquid and solid phases were allowed to attain equilibrium in the teflon cell at constant

Nacl in water	as a function of	temperature
T(K)	Wt. % NaCl (±0.05)	
425	29.76	
450	30.81	
475	31.99	
500	33.31	
525	34.75	
550	36.34	
575	38.05	
600	39.90	
625	41.87	
650	43.98	
675	46.23	
700	48.60	

Table 2.26.

Temperature-dependent equation and precision

weight percent salt in solution =  $32.161 - 0.05071 \text{ T} + 0.000106 \text{ T}^2$ 

 $s = \pm 0.05$  Wt. % NaCl



FIGURE 2.2. Ref. [44]. A temperature-composition phase diagram for the NaCl-H<sub>2</sub>O system. The metastable areas are indicated by broken lines. Below K (=cryohydric point) 'all phases are solid with stable paragenesis (ice + hydrohalite), left of K with ice inclusions, right of K with hydrohalite inclusions. SW refers to seawater.



FIGURE 2.3. Ref. [81] Pressure-temperature composition model for the system NaCl-H<sub>2</sub>O.



FIGURE 2.4. Ref. [44]. Solubility isotherms in the system NaCl-KCl-H<sub>2</sub>O for the temperature range 0-100 °C.



FIGURE 2.5. Ref [44]. Solubility isotherms in the system NaCl-KCl-MgCl<sub>2</sub>-H<sub>2</sub>O, saturated with respect to NaCl, for the temperature range 0-100°C.

E: at this point there is no joint precipitation of carnallite and sylvite.

D: upon final evaporation at this point the residual solution can yield bischofite, carnallite and halite.



FIGURE 2.6. Ref. [44]. Solubility isotherms in the system KCl-NaCl-MgCl<sub>2</sub>-H<sub>2</sub>O at KCl + NaCl saturation for the temperature range 0-70 °C. The MgCl<sub>2</sub> content in mol/1000 mol H<sub>2</sub>O serves as a parameter.



temperature and pressure. This procedure minimized the contamination of the solutions.

The solubility data obtained with the use of the hydrothermal solution equipment at pressure slightly above the vapor pressure of the system are in good agreement with previous data as shown in figure 2.8. The data reported by Dickson et al. [82] have been reanalyzed and values of the solubility of anhydrite in water at various pressures and at rounded temperatures are advanced as recommended values in tables 2.27-2.30. Temperature-dependent equations, together with standard errors of estimate are also given.

It is seen that the solubility of anhydrite decreases with rising temperature.

Templeton and Rodgers [89] have determined the solubility of anhydrite in a number of salt solutions at elevated temperatures and at pressures just above the vapor pressure. The CaSO<sub>4</sub>-NaCl-H<sub>2</sub>O system was investigated at 523, 548, 573 and 598 K from essentially zero to about 6 molal NaCl. A high temperature flow solubility apparatus was used in this study with the temperature controlled to  $\pm 1$  K. Reagent grade salts were used for all the measurements and distilled water was used to prepare solutions. Spectrophotometric or EDTA methods were employed to measure either calcium or sulfate. The precision of the data was reported to be  $\pm 2\%$ 

of the value of  $c_{m_{CaSO_4}}$ . The data of Templeton and Rodgers [89] have been reanalyzed and values of the solubility of anhydrite at rounded concentrations of NaCl are advanced in tables 2.31 and 2.32. Equations representing the solubility of anhydrite as a function of sodium chloride concentration are also given. In addition, Templeton and Rodgers [89] measured the solubility of anhydrite in the systems CaSO<sub>4</sub>-CaCl<sub>2</sub>-H<sub>2</sub>O and CaSO<sub>4</sub>-MgCl<sub>2</sub>-H<sub>2</sub>O. These data have been similarly reanalyzed and values of the solubility of anhydrite at rounded concentrations of either CaCl<sub>2</sub> or MgCl<sub>2</sub> are given in tables 2.33 and 2.34, respectively. Finally the quaternary systems CaSO<sub>4</sub>-CaCl<sub>2</sub>NaCl-H<sub>2</sub>O and CaSO<sub>4</sub>-MgCl<sub>2</sub>-NaCl-H<sub>2</sub>O were also investigated and values are advanced in table 2.35.

#### 2.5.3. The System Gypsum-Water-NaCl

Blount and Dickson [90] used the hydrothermal solution apparatus to measure the solubility of gypsum in water at various pressures and temperatures. Reagent grade material was used and the maximum estimated uncertainty in the values was  $\pm 2.5\%$  for the solubility and  $\pm 4$  bars ( $4 \times 10^5$ Pa) for the pressure. The data were reanalyzed and values of solubility at rounded pressures are advanced in table 2.36. The gypsum solubility in water at one atmosphere pressure changes only slowly



FIGURE 2.8. Comparsion of the hydrothermal method for solubilities of anhydrite at 1 atmosphere below 100°C and at the vapor pressure of the system above 100°C. (The curve represents a fit to all of the data.)

501u	Diffly of annyurice	in water	as a function of
te	mperature at a pres	sure of 10	00x10 <sup>5</sup> pascals
<u>T(K)</u>	Wt. % anhydrite	Т(К)	Wt. % anhydrite
380	0.073	440	0.017
390	0.058	450	0.014
400	0.046	460	0.011
410	0.036	470	0.009
420	0.028	480	0.007
430	0.022	490	0.007

# Table 2.27.

Temperature-dependent equation and precision

Wt % = 5.2255961 - 3.21053.10<sup>-2</sup> T + 6.6167237.10<sup>-5</sup> T<sup>2</sup> - 0.4568792.10<sup>-7</sup> T<sup>3</sup>

precision s = 2.123%

Table 2.29.

		Table	e 2	.28.				
Solubility	of	anhydrite	in	water	as	a	function	of
tompora	ture	at a pre	ssii	re of !	500:	x1(	<sup>5</sup> pascals	5

	temperature at a pre	<u>35010 01</u>	Storio Fusicio
<u>T(K)</u>	Wt. % anhydrite	T(K)	Wt. % anhydrite
375	0.119	465	0.016
385	0.097	475	0.013
395	0.079	485	0.011
405	0.063	495	0.010
415	0.050	505	0.008
425	0.039	515	0.007
435	0.031	525	0.005
445	0.024	535	0.003
455	0.019		

Temperature-dependent equation and precision Wt % =  $5.978863 - 3.5464.10^{-2}$  T +  $7.04671.10^{-5}$  T<sup>2</sup> -  $0.4683758.10^{-7}$  T<sup>3</sup>

precision s = 3.550%

#### Table 2.30.

Solubility of anhydrite in water as a function of temperature at pressures slightly greater than the vapor pressure of the system.

<u>T(K)</u>	P(x10 <sup>-5</sup> ) Pa	Wt % anhydrite
369	2	0.0781
378	6	0.0682
404	5	0.0357
430	15	0.0198
583	100	

Solubility of	anhydrite in water as a function of
temperature	at a pressure of 1000x10 <sup>5</sup> pascals

T(K)	Wt. % anhydrite	T(K)	Wt. % anhydrite
380	0.176	470	0.023
390	0.145	480	0.018
400	0.118	490	0.015
410	0.095	500	0.013
420	0.076	510	0.011
430	0.060	520	0.009
440	0.047	530	0.007
450	0.037	535	0.006
460	0.029		

Temperature-dependent equation and precision

Wt % = 7.4676808 - 0.4118806.10<sup>-1</sup> T + 7.1843308.10<sup>-5</sup> T<sup>2</sup> - 3.0831114.10<sup>-8</sup> T<sup>3</sup> - 1.5485214.10<sup>-11</sup> T<sup>4</sup>

precision s = 5.767%

# Table 2.31.

# Solubility of anhydrite in NaCl- $H_2^0$ solutions at

Т(К)	anhydrite (c <sub>m</sub> )				
	$m_{\text{NaC1}}^{\text{c}} = 2.0$	$m_{\text{NaC1}}^{\text{c}} = 4.0$	$m_{NaC1} = 6.0$		
375	0.0261	0.0280	0.0255		
395	0.0207	0.0240	0.0235		
415	0.0168	0.0210	0.0220		
435	0.0139	0.0187	0.0209		
455	0.0116	0.0168	0.0201		
475	0.0098	0.0154	0.0196		
495	0.0083	0.0142	0.0193		
515	0.0070	0.0133	0.0191		
535	0.0059	0.0125	0.0191		
555	0.0049	0.0118	0.0191		
575	0.0041	0.0112	0.0192		
595	0.0033	0.0107	0.0193		
615	0.0026	0.0102	0.0194		
635	0.0020	0.0097	0.0195		
655	0.0015	0.0092	0.0194		
675	0.0011	0.0087	0.0193		
695	0.0008	0.0082	0.0190		
715	0.0005	0.0076	0.0185		

constant NaCl concentrations.

# Temperature-dependent equations

$c_{Mac1} = 2.0$
$\ln m = 10.16 - 0.07407T + 1.329.10^{-4} T^{2} - 8.95.10^{-8} T^{3}$ $^{c} m_{\text{NaCl}} = 4.0$
$\ln m = 4.943 - 0.04246 T + 6.640.10^{-5} T^{2} - 3.667.10^{-8} T^{3}$
$m_{NaC1} = 6.0$
$In m = 5.2542 - 5.741.10 - T + 6.443.10 - T^2 - 3.670.10 - T^2$

# Table 2.32.

Solubilities of anhydrite in NaCl-H $_2$ O solutions from 523 K to 598 K

NaCl (c <sub>m</sub> )	523 K	548 K	573 K	598 K
0.00025	0.000176	0.000078		
0.00050	0.000177	0.000079		
0.00075	0.000178	0.000079		
0.00100	0.000179	0.000080		
0.00250	0.000185	0.000084		
0.00500	0.000194	0.000091		
0.00750	0.000203	0.000098	0.000026	
0.01000	0.000213	0.000105	0.000032	
0.02500	0.000269	0.000146	0.000065	0.000051
0.05000	0.000362	0.000215	0.000119	0.000072
0.07500	0.000455	0.000284	0.000173	0.000094
0.10000	0.000548	0.000353	0.000227	0.000118
0.25000	0.001104	0.000765	0.000537	0.000297
0.50000	0.002024	0.001453	0.001042	0.000705
0.75000	0.002933	0.002143	0.001563	0.001210
1.00000	0.003832	0.002838	0.002127	0.001775
2.00000	0.007329	0.005699	0.004968	0.004325
3.00000	0.010665	0.008796	0.008352	0.007373
4.00000	0.013841	0.012265	0.011473	0.011444
5.00000	0.016856	0.016242	0.014734	0.016227
6.00000	0.019711	0.020862	0.021596	0.018813

.

# Table 2.32.

Solubilities of anhydrite in NaCl-H<sub>2</sub>O solutions

from 523 K to 598 K "--Continued"

Concentration-dependent equations and precision  ${}^{C}m_{anhydrite} = a + b M + c M^{2} + d M^{3} + e M^{4} + f M^{5}$ M = the molal concentration of sodium chloride

Temp (K)	a.10 <sup>4</sup>	b.10 <sup>2</sup>	c.10 <sup>4</sup>
523	1.7516	0.37371	-0.80182
548	0.772789	0.27549	-0.17102
573	0.098800	0.22202	-6.0258
598	0.32922	0.069153	16.399
Temp (K)	d.10 <sup>3</sup>	e.10 <sup>3</sup>	f.10 <sup>4</sup>
523			
548	0.02248	0.00109	
573	0.066368	-0.17952	0.15337
598	-0.74941	0.17449	-0.13965
	Temp (K)	precision (s)	
	523	2.37%	
	548	1.08%	
	573	3.12%	
	598	0.53%	

				<u> </u>	-
CaCl <sub>2</sub> (c <sub>m</sub> ) <sup>2</sup>	523 K	573 K	CaCl <sub>2</sub> (c <sub>m</sub> ) <sup>2</sup>	523 K	573 K
	c <sub>mCaSO4</sub> (x1	0 <sup>3</sup> )		<sup>c</sup> m <sub>CaSO4</sub> (x	10 <sup>3</sup> )
0.04	0.134	0.045	0.17	0.249	0.131
0.05	0.142	0.052	0.18	0.258	0.138
0.06	0.151	0.059	0.19	0.267	0.144
0.07	0.160	0.065	0.20	0.275	0.151
0.08	0.169	0.072	0.21	0.284	0.157
0.09	0.178	0.078	0.22	0.293	0.164
0.10	0.187	0.085	0.23	0.302	0.170
0.11	0.196	0.092	0.24	0.311	0.177
0.12	0.204	0.098	0.25	0.320	0.184
0.13	0.213	0.105	0.26	0.329	0.190
0.14	0.222	0.111	0.27	0.337	0.197
0.15	0.231	0.118	0.28	0.346	0.203
0.16	0.240	0.124	0.29	0.355	0.210

Table 2.33.

Solubilities of anhydrite in the CaSO<sub>4</sub>-CaCl<sub>2</sub>-H<sub>2</sub>O system

Concentration-dependent equations and precision

c <sup>m</sup> CaSO⊿	=	0.98183.10 <sup>-4</sup>	+	0.88596.10 <sup>-3</sup> cm <sub>CaCl<sub>2</sub></sub>	(523	K);	s	=	4.01%
<sup>c</sup> <sup>m</sup> CaSO <sub>4</sub>	=	0.19131.10 <sup>-4</sup>	+	0.60801.10 <sup>-3 c</sup> mCaCl <sub>2</sub>	(573	K);	s	=	6.32%

Table	2.	34.

Solubilities of anhydrite in the  $CaSO_4$ -MgCl<sub>2</sub>-H<sub>2</sub>O system

MgC1 <sub>2</sub>			MgC12		
(c <sub>m</sub> ) -	523 K	573 K	(c <sub>m</sub> ) -	523 K	573 K
	c <sub>m</sub> CaSO <sub>4</sub>	(x10 <sup>2</sup> )		<sup>c</sup> mCaSO <sub>4</sub>	(x10 <sup>2</sup> )
0.04	0.2125	0.1454	0.17	0.5852	0.4739
0.05	0.2467	0.1706	0.18	0.6100	0.4992
0.06	0.2797	0.1959	0.19	0.6346	0.5245
0.07	0.3116	0.2212	0.20	0.6592	0.5498
0.08	0.3423	0.2465	0.21	0.6839	0.5750
0.09	0.3721	0.2717	0.22	0.7087	0.6003
0.10	0.4010	0.2970	0.23	0.7337	0.6256
0.11	0.4291	0.3223	0.24	0.7589	0.6509
0.12	0.4564	0.3476	0.25	0.7846	0.6762
0.13	0.4831	0.3728	0.26	0.8108	0.7014
0.14	0.5093	0.3981	0.27	0.8375	0.7267
0.15	0.5349	0.4234	0.28	0.8648	0.7520
0.16	0.5602	0.4487	0.29	0.8929	0.7773

Concentration-dependent equations and precision

 $c_{m_{CaSO_{4}}} = 0.61341.10^{-3} + 0.409.10^{-1} c_{m_{MgCl_{2}}} - 0.83632.10^{-1} c_{m_{MgCl_{2}}}^{2} + 0.14303 c_{m_{MgCl_{2}}}^{3} (523 \text{ K}); \text{ s} = 0.20\%$   $c_{m_{CaSO_{4}}} = 0.44251.10^{-3} + 0.25276.10^{-1} c_{m_{MgCl_{2}}} (573 \text{ K}); \text{ s} = 0.27\%$ 

#### Table 2.35.

# Solubilities of anhydrite in solutions of constant ionic

strength for some quaternary systems

=

strength	for some qua	iternaly systems	_		
CaSO <sub>4</sub> -CaCl <sub>2</sub> -NaCl-H <sub>2</sub> O System					
c <sub>m</sub> CaCl <sub>2</sub>	c <sub>mNaCl</sub>	c <sub>m</sub> CaSO <sub>4</sub>			
	523 K, I =	0.50			
	0.492	0.00199			
0.0080	0.4747	0.000496			
0.0080	0.4747	0.000517			
0.0250	0.4246	0.000263			
0.0250	0.4246	0.000262			
0.0700	0.2898	0.000236			
0.0700	0.2898	0.000244			
0.1666		0.000237			
	523 K, I =	0.90			
	0.8868	0.00330			
0.0040	0.8763	0.00186			
0.0100	0.8653	0.00109			
0.0180	0.8434	0.000746			
0.0250	0.8231	0.000532			
0.0400	0.7788	0.000420			
0.0800	0.6594	0.000372			
0.0800	0.6594	0.000370			
0.0800	0.6594	0.000364			
0.100	0.5995	0.000360			
0.200	0.2996	0.000366			
0.200	0.2996	0.000385			
0.300		0.000364			
	573 K, I =	0.50			
	0.496	0.00100			
0.0080	0.4747	0.000184			
0.0250	0.4246	0.0000939			
0.0250	0.4246	0.0000970			
0.0700	0.2898	0.0000889			
0.0700	0.2898	0.0000913			
0.1666		0.000110			
	573 K, I =	0.90			
	0.892	0.00189			
0.0040	0.8763	0.000802			
0.0180	0.8434	0.000315			
0.0400	0.7788	0.000210			
0.0400	0.7788	0.000217			
0.0800	0.6594	0.000166			
0.200	0.2996	0.000208			
0.200	0.2996	0.000195			
0.300		0.000223			

Table 2.35.

CaSO <sub>4</sub> -MgCI	2-NaC1-H2C	) System
c <sub>mMgCl2</sub>	m <sub>NaCl</sub> c	<sup>m</sup> CaSO <sub>4</sub>
523	K, I = 0.5	50
	0.492	0.00199
0.00295	0.4853	0.00204
0.00811	0.4694	0.00218
0.00811	0.4694	0.00214
0.0204	0.4320	0.00262
0.0240	0.4320	0.00260
0.0608	0.3070	0.00358
0.0608	0.3070	0.00360
0.1219	0.1240	0.00490
0.1219	0.1240	0.00492
0.1631		0.00568
573	K, I = 0.5	50
	0.496	0.00100
0.00295	0.4853	0.00107
0.00295	0.4853	0.00107
0.00811	0.4694	0.00131
0.0204	0.4320	0.00166
0.0608	0.3070	0.00251
0.0608	0.3070	0.00265
0.1219	0.1240	0.00378
0.1631		0.00456
0.1631		0.00455

#### Table 2.36.

# The solubility of gypsum in water as a function

of temperature	and	pressure
----------------	-----	----------

$Px10^{-5}$ Pa	313 K	323 K	333K	340 K	352 K	356 K
	-		CaSO <sub>4</sub> (c <sub>m</sub> )			
3					0.0138	
5					0.0139	
25		0.0155	0.0147		0.0140	
50		0.0159	0.0151		0.0143	
75		0.0162	0.0155		0.0146	
100		0.0166	0.0159		0.0149	
125		0.0170	0.0163		0.0152	
150		0.0173	0.0167		0.0155	
175		0.0177	0.0171		0.0158	
200		0.0181	0.0174		0.0162	
225		0.0185	0.0178		0.0165	
250		0.0189	0.0182		0.0168	
275		0 0193	0.0186		0 0172	
300		0 0198	0 0190		0.0175	
325		0.0202	0.0195		0.0179	
323		0.0202	0.0199		0.0175	
275		0.0200	0.0203		0.0182	
375		0.0211	0.0203		0.0180	
400		0.0215	0.0207		0.0190	
425		0.0219	0.0211		0.0194	
450		0.0224	0.0215		0.0198	
475		0.0229	0.0219		0.0202	
500		0.0233	0.0223	0.0226	0.0206	
525		0.0238		0.0229	0.0210	
545	0.0259					
550	0.0260	0.0243		0.0232	0.0214	
555	0.0262					
560	0.0263					
565	0.0264					
570						
575		0.0248		0.0235	0.0218	
600		0.0253		0.0219	0.0222	
625		0.0258		0.0242	0.0227	
650		0.0263		0.0247	0.0231	
675		0.0268		0.0251	0.0236	
700		0.0273		0.0256	0.0240	
725		0.0278		0.0261	0.0245	
750		0.0284		0.0266	0.0250	
775		0.0289		0.0272	0.0255	
800		0.0294		0.0278	0.0259	
825		0.0300		0.0284	0.0264	
850		0.0305		0.0290	0.0269	
875		0.0311		0.0297	0.0274	
900		0 0317		0.0304	0.0279	
925		0.0323		0 0312	0 0285	
950		0.0329		0 0310	0 0200	
075		0.0320		0.0327	0.0295	
000		0.0334		0.0527	0.0295	0 0311
990						0.0511
999				0.0776	0.0701	0.0311
1000				0.0336	0.0301	0.0311
1001						0.0311
1002						0.0311
1003						0.0310
1004						0.0310

Tai	b1e	2	.3	6.
-				

The solubility of gypsum in water as a function

of temperature and pressure "--Continued"

Pressure-dependent equations and precision  $c_{m}_{CaSO}$  = a + b P + c P<sup>2</sup>

		-		
Т(К)	a.10	b.10 <sup>9</sup>	c.10 <sup>18</sup>	precision (s)
313	0.13106	0.23528		0.00%
323	0.15165	0.13797	0.50605	0.72%
333	0.14332	0.15290	0.14252	0.00%
340	0.23529	-0.13725	2.3769	1.50%
352	0.13747	0.10966	0.53396	0.94%
356	0.51140	-0.20040		1.05%

with temperature and passes through a very weak maximum at about 313 K.

A study of the solubility of gypsum in NaCl-H<sub>2</sub>O solutions from 273-383 K has been performed by Marshall and Slusher [91]. A small high pressure titanium alloy vessel incorporating a Teflon gasket was used for the measurements, with the special feature of the design being the containment of the Teflon above its transition temperature of 600 K. Selected mixtures of solid and solution were sealed in the vessels. The solution phases were sampled by means of flexible capillary tubing and valves. Since the liquid phase was sampled at its equilibration temperature and subsequently analyzed, a correction for loss of water or other constituents to the vapor was unnecessary. The temperature of equilibrium was approached from both lower and higher temperatures; agreement of analyses was used to show that equilibrium had been attained. The data of Marshall and Slusher [91] were reanalyzed and values of the solubility of gypsum were generated at rounded concentrations of sodium chloride over the temperature range from 273-383 K. The recommended values, compositiondependent equations and precisions are in tables 2.37 - 2.39.

#### 2.5.4. Comparison of the Systems Anhydrite-Water and Gypsum-Water

A comparison of the solubilities of anhydrite and gypsum in water with added sodium chloride is shown in figure 2.9. The solubility of gypsum and anhydrite is in general influenced by the presence of additional ions, increasing through the addition of foreign ions, and conversely being reduced by the addition of the same ions. These effects for both gypsum and anhydrite are shown in figure 2.10. Because of the different temperature coefficients, the point of intersection of the gypsum and anhydrite solubility curves is displaced towards lower temperatures as the NaCl content of the solution increases. With an additional  $SO_4^{-2}$  content the solubility of gypsum and anhydrite is reduced and the maximum becomes broader.

#### 2.5.5. The System Calcite-Water + (NaCl, CaCl<sub>2</sub>...)

The solubility of calcite in water as a function of  $CO_2$  pressure and temperature is presented graphically in figures 2.11–2.15. The curves in these figures represent fits to all of the data.

Macdonald and North [97] investigated the effect of pressure on the solubility of calcite in water between 273 and 308 K and for pressures up to 101325 Pa. The distilled water used in the measurements was de-ionized water which was boiled vigorously prior to use to expel any dissolved  $CO_2$ . The calcium carbonate was in the form of small natural calcite crystals. An analysis of the calcite showed that it contained less than 0.1% of magnesium. In the determination of solubility the solutions were saturated by allowing the water to percolate, at a known rate, through the reaction column which was packed with the dissolving solid. The particular method used in this study produces a large surface area to liquid volume ratio and so allows a relatively rapid attainment of equilibrium. The solutions were analyzed for calcium by atomic absorption, and all determinations had an accuracy of at least  $\pm 2\%$ . The data of Macdonald and North [97] were reanalyzed and values of both solubility and thermodynamic solubility products were derived at rounded pressures and are advanced as recommended values in tables 2.40-2.43, together with pressure dependent equations.

Akin and Lagerwerff [98] studied the effects of added electrolytes on the solubility of calcite in water, using an apparatus designed to minimize  $CO_2$  fluctuations. Calcium was determined by EDTA titration, while sodium was monitored with a flame photometer. The values reported by Akin and Lagerwerff [98] were reevaluated using statistical analysis and results are given for the solubility of calcite at rounded concentrations of sodium chloride in tables 2.44–2.48. Concentration-dependent equations and precisions are also reported.

#### 2.5.6. Dehydration of Gypsum

The main point of interest in the chemistry of gypsum concerns the products of its dehydration. Four principal phases have been reported [99] in the system calcium

# Table 2.37

The solubility of gypsum in  $NaCl-H_2O$ 

NaCl (c <sub>m</sub> )			$CaSO_4 \cdot 2H_2O_{(c_m)}$		
	273.5 K	278 K	283 K	288 K	293 K
0.01	0.0148	0.0154	0.0162	0.0168	0.0165
0.02	0.0152	0.0158	0.0166	0.0173	0.0170
0.03	0.0156	0.0163	0.0171	0.0177	0.0175
0.04	0.0160	0.0167	0.0175	0.0182	0.0179
0.05	0.0165	0.0171	0.0179	0.0186	0.0184
0.06	0.0169	0.0175	0.0184	0.0190	0.0188
0.07	0.0173	0.0180	0.0188	0.0195	0.0193
0.08	0.0177	0.0184	0.0192	0.0199	0.0197
0.09	0.0181	0.0188	0.0196	0.0203	0.0202
0.10	0.0185	0.0192	0.0200	0.0207	0.0206
0.20	0.0230	0.0231	0.0239	0.0247	0.0248
0.30	0.0258	0.0266	0.0275	0.0283	0.0286
0.40	0.0291	0.0298	0.0308	0.0316	0.0320
0.50	0.0320	0.0328	0.0338	0.0347	0.0352
0.60	0.0348	0.0355	0.0366	0.0374	0.0380
0.70	0.0373	0.0379	0.0390	0.0399	0.0405
0.80	0.0395	0.0401	0.0413	0.0421	0.0428
0.90	0.0416	0.0421	0.0433	0.0442	0.0448
1.00	0.0435	0.0439	0.0451	0.0460	0.0465
2.0	0.0542	0.0535	0.0547	0.0553	0.0553
3.0	0.0564	0.0553	0.0560	0.0566	0.0562
4.0	0.0556	0.0554	0.0554	0.0563	0.0563
5.0	0.0530	0.0537	0.0534	0.0553	0.0556
6.0	0.0451	0.0447	0.0455	0.0489	0.0473

solutions at 273-293 K

Concentration-dependent equations and precisions

c <sub>m</sub> gypsum	=	а	+	b	М	+	с	м <sup>2</sup>	+	d	м <sup>3</sup>	+	e	М4
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M = molal concentration of sodium chloride

Temp (K)	a.10	b.10	c.10	d.10 <sup>2</sup>	e.10 <sup>3</sup>	precision (s)
273.5	0.1436225	0.4279379	-0.1623401	0.2766863	-0.1845770	1.67%
2.78	0.1496224	0.4394013	-0.1815735	0.3388285	-0.2408431	1.96%
283	0.1574711	0.4445050	-0.1814384	3.276261	-2.248609	1.97%
288	0.163198	0.4512401	-0.1873406	3.423325	-2.339645	2.25%
293	0.1605044	0.4775160	-0.2102661	0.4057587	-0.2891751	2.73%

Table 2.38.

The	solubility	of	gypsum	in	NaC1-H <sub>2</sub> O	solutions	at	298-	343	K
-----	------------	----	--------	----	-----------------------	-----------	----	------	-----	---

NaCl (c <sub>m</sub> )		CaSO (c	4 <sup>•2H</sup> 20 m)	
_	298 K	303 K	313 K	343 K
0.01	0.0174	0.0164	0.0169	0.0170
0.02	0.0178	0.0171	0.0175	0.0174
0.03	0.0182	0.0178	0.0181	0.0178
0.04	0.0187	0.0184	0.0187	0.0182
0.05	0.0191	0.0191	0.0193	0.0186
0.06	0.0196	0.0197	0.0198	0.0190
0.07	0.0200	0.0203	0.0204	0.0194
0.08	0.0204	0.0209	0.0210	0.0198
0.09	0.0208	0.0215	0.0215	0.0202
0.10	0.0213	0.0221	0.0220	0.0205
0.20	0.0252	0.0271	0.0268	0.0242
0.30	0.0288	0.0311	0.0307	0.0277
0.40	0.0321	0.0342	0.0339	0.0308
0.50	0.0351	0.0366	0.0366	0.0338
0.60	0.0377	0.0385	0.0388	0.0365
0.70	0.0401	0.0402	0.0407	0.0390
0.80	0.0423	0.0418	0.0424	0.0413
0.90	0.0442	0.0436	0.0441	0.0434
1.00	0.0459	0.0458	0.0458	0.0453
2.00	0.0541			0.0558
3.00	0.0553			0.0567
4.00	0.0561			0.0566
5.00	0.0569			0.0643
6.00	0.0511			0.0883

Concentration-dependent equations and precisions

 $c_{m_{gypsum}} = a + b M + c M^{2} + d M^{3} + e M^{4}$ 

M = molal concentration of sodium chloride

Temp (K)	a.10	b.10	c.10	d.10 <sup>2</sup>	e.10 <sup>3</sup> pr	ecision (s)
298	0.1690221	0.4549512	-0.2017596	0.3924890	-0.2891751	2.16%
303	0.1573776	0.7053267	-0.7498029	3.449260	-0.2779556	1.34%
313	0.1624119	0.6350437	-0.5876340	2.798339		1.40%
343	0.1660804	0.4073127	-0.1344950	1.446642		5.51%

#### Table 2.39.

The solubility of gypsum in NaCl-H $_2$ O solutions at 353-383 K

NaCl (c <sub>m</sub> )		$(c_{-})$	
	353 K	368 K	383 K
0.01	0.0176	0.0158	0.0119
0.02	0.0178	0.0161	0.0124
0.03	0.0180	0.0164	0.0129
0.04	0.0182	0.0166	0.0135
0.05	0.0184	0.0169	0.0140
0.06	0.0186	0.0172	0.0145
0.07	0.0188	0.0174	0.0150
0.08	0.0190	0.0177	0.0155
0.09	0.0192	0.0180	0.0160
0.10	0.0194	0.0183	0.0165
0.20	0.0214	0.0209	0.0213
0.30	0.0234	0.0236	0.0257
0.40	0.0254	0.0261	0.0299
0.50	0.0273	0.0287	0.0338
0.60	0.0292	0.0312	0.0374
0.70	0.0311	0.0336	0.0408
0.80	0.0330	0.0360	0.0439
0.90	0.0349	0.0384	0.0468
1.00	0.0367	0.0407	0.0494
2.00	0.0538	0.0612	0.0647
3.00	0.0688	0.0771	0.0670
4.00	0.0814	0.0883	0.0661
5.00	0.0919	0.0950	0.0717
6.00	0.1001	0.0970	0.0934

Concentration-dependent equations and precisions  $c_m_{gypsum} = a + b M + c M^2 + d M^3$ M = molal concentration of sodium chloride

Temp (K)					precision (s)
353	0.1735577	0.2046287	-0.1109989		6.3%
368	0.1552855	0.2745152	-0.2312935		6.7%
383	0.1137741	0.525739	-1.619548	0.1618607	5.8%



FIGURE 2.9. Ref. [86]. Solubility of gypsum, hemihydrate, and anhydrite in water.



FIGURE 2.10. Solubility of gypsum and anhydrite in saline solutions from 25-70°C. Solid phases; anhydrite = solid and broken lines; gypsum-dotted lines (heavy and light). 1 [93]; 2-4 [94]; 5 [95] 6, extrapolated from 3 and 4; 7, seawater and its alterations in concentration.



CO2 PRESSURE (atm.)

FIGURE 2.11. The solubility of calcite in water at 75°C as a function of CO<sub>2</sub> pressure.



FIGURE 2.12. The solubility of calcite in water at 100°C as a function of CO2 pressure.



FIGURE 2.13. The solubility of calcite in water at 125°C as a function of CO<sub>2</sub> pressure.



FIGURE 2.14. The solubility of calcite in water at 150°C as a function of CO2 pressure.



FIGURE 2.15. The solubility of calcite in water at 200  $^\circ$ C as a function of CO<sub>2</sub> pressure.

Table 2.40.

Effect of pressure on the solubility of calcite in water at 274 K and thermodynamic solubility products  $[CaCO_3(s) = Ca^{2+} + CO_3^{2-}]$ 

Px10 <sup>-5</sup> (pascals)	Ca <sup>2+</sup> (µkg/kg)	Kp (x10 <sup>9</sup> )
95	4.627	6.51
135	4.856	7.39
175	5.087	8.27
210	5.292	9.04
250	5.532	9.97
290	5.779	10.96
330	6.034	12.03
370	6.299	13.21
410	6.576	14.52
450	6.866	15.98
490	7.171	17.62
530	7.492	19.47
570	7.831	21.53
610	8.189	23.85
645	8.519	26.09
685	8.918	28.93
725	9.340	32.08
765	9.788	35.57
805	10.262	39.42
845	10.765	43.66

Pressure-dependent equations and precisions

 $[Ca^{2+}] = 4.084933 + 5.7517223x10^{-8} P - 8.6390113x10^{-17} P^{2} + 4.039419x10^{-24} P^{3}$ standard error of estimate = 0.89%  $K_{p} = 4.26629 + 2.5594748x10^{-7} P - 2.6248554x10^{-15} P^{2} + 6.0507034x10^{-23} P^{3}$ precision s = 1.96%

#### Table 2.41.

Effect of pressure on the solubility of calcite in water

$Px10^{-5}$ (pascals)	$Ca^{2+}$ (µkg/kg)	<sup>K</sup> p (x10 <sup>9</sup> )
35	4.585	5.48
75	4.824	6.32
120	5.095	7.24
160	5.337	8.06
200	5.583	8.88
240	5.833	9.75
280	6.088	10.67
320	6.350	11.67
360	6.620	12.77
400	6.899	13.98
440	7.188	15.34
480	7.488	16.85
520	7.800	18.55
560	8.126	20.44
600	8.466	22.56
640	8.823	24.91
680	9.196	27.53
725	9.638	30.82
765	10.051	34.06
805	10.485	37.62

at 281 K and thermodynamic solubility products

Pressure-dependent equations and precisions  $[Ca^{2+}] = 4.374741 + 6.0105456x10^{-8} P - 4.4776231x10^{-17} P^{2} + 2.9932948x10^{-24} P^{3}$ precision s = 0.76%  $K_{p} = 4.702247 + 2.2867598x10^{-7} P - 2.0448748x10^{-15} P^{2} + 53.224503x10^{-24} P^{3}$ precision s = 4.99%

#### Table 2.42.

# Effect of pressure on the solubility of calcite in water at 300 K

		. <u> </u>
 Px10 <sup>-5</sup> (pascals)	Ca <sup>2+</sup> (µkg/kg)	(x109)
45	5.296	4.91
85	5.415	5.17
130	5.576	5.57
170	5.743	6.03
210	5.929	6.57
250	6.133	7.21
290	6.355	7.95
330	6.593	8.77
370	6.845	9.69
410	7.110	10.71
450	7.386	11.81
490	7.673	13.01
530	7.969	14.30
570	8.272	15.68
615	8.620	17.35
655	8.934	18.93
695	9.252	20.60
735	9.571	22.37
775	9.891	24.23
815	10.210	26.18
855	10.526	28.22

and thermod	ynamic	solubi	lity	products
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Pressure-dependent equations and precisions  $[Ca^{2+}] = 5.190895 + 1.9778396 \times 10^{-8} P + 8.0679045 \times 10^{-16} P^{2}$   $- 3.6058291.10^{-24} P^{3}$ precision s = 1.05%  $K_{p} = 4.731204 + 2.6838933 \times 10^{-8} P + 2.8998339 \times 10^{-15} P^{2}$ precision s = 2.96%

#### Table 2.43.

Effect of pressure on the solubility of calcite in water at

298 K and thermodynamic solubility products

Px10 <sup>-5</sup> (pascals)	Ca <sup>2+</sup> (µkg/kg)	(x10 <sup>9</sup> )	
25	4.898	5.04	
7 5	5.151	4.68	
130	5.431	4.71	
180	5.687	5.10	
230	5.945	5.80	
280	6.205	6.76	
330	6.468	7.95	
380	6.734	9.34	
430	7.003	10.88	
480	7.276	12.55	
530	7.553	14.31	
580	7.834	16.11	
630	8.121	17.93	
685	8.442	19.91	
735	8.739	21.64	
785	9.043	23.28	
835	9.353	24.78	
890	9.702	26.23	
940	10 027	27 33	

Pressure-dependent equations and precisions  $[Ca^{2+}] = 4.7712206 + 5.0521587x10^{-8} P + 1.0647239x10^{-17} P^{2} + 4.9697389x10^{-25} P^{3}$ precision s = 3.4%  $K_{p} = 5.3800985 - 1.5579606x10^{-7} P + 8.6712745x10^{-15} P^{2} - 4.818458x10^{-23} P^{3}$ precision s = 3.78% Table 2.44.

The solubility of calcite in solutions containing NaCl and  $NaHCO_3$ [concentration of  $NaHCO_3 = 0.04 \text{ mol/m}^3$ ); P = 26000 pascals,

\_

\_\_\_\_

T = 300  K				
	NaC1 mo1/m <sup>3</sup>	CaCO <sub>3</sub> mo1/m <sup>3</sup>	NaCl mol/m <sup>3</sup>	CaCO <sub>3</sub> mo1/m3
	4	.5175	32	.465
	6	.5280	34	.436
	8	.5400	36	.408
	10	.5530	38	.382
	12	.5640	40	.359
	14	.5730	42	.343
	16	.5790	44	.335
	18	.5805	46	. 338
	20	.5775	48	.356
	22	.5695	50	.391
	24	.5565	52	.447
	26	.5390	54	.527
	28	.5175	56	.639
	30	.4930		

Concentration-dependent equation and precision  $c_{m}_{CaCO_{3}} = 0.511263 - 1.91324 \times 10^{-3} \text{ M} + 1.07952 \times 10^{-3} \text{ M}^{2}$  $- 5.3719 \times 10^{-5} \text{ M}^{3} + 6.38586 \times 10^{-7} \text{ M}^{4}$ 

M = molal concentration of sodium chloride

precision, s = 1.70%

95

#### Table 2.45.

The solubility of calcite in solutions containing NaCl

NaCl mol/m <sup>3</sup>	CaCO3 mol/m3	NaCl mol/m <sup>3</sup>	CaCO <sub>3</sub> mo1/m <sup>3</sup>
8	.6050	36	.7065
10	.6085	38	.7090
12	.6140	40	.7105
14	.6220	42	.7115
16	.6305	44	.7115
18	.6400	46	.7115
20	.6500	48	.7120
22	.6600	50	.7130
24	.6695	52	.7150
26	.6780	54	.7185
28	.6860	56	.7240
30	.6930	58	.7330
32	.6985	60	.7450
34	.7030		

[P = 35700 pascals; T = 301 K]

Concentration-dependent equation and precision  $c_{m} = 0.629765 - 0.0824625 \text{ M} + 7.882835 \times 10^{-4} \text{ M}^{2}$  $- 9.92469 \times 10^{-5} \text{ M}^{3} + 1.488825 \times 10^{-8} \text{ M}^{4}$ 

M = molal concentration of sodium chloride

precision, s = 0.00%

_	P = 35000  pascals; T = 302  K]				
	NaCl mol/m <sup>3</sup>	CaCO <sub>3</sub> mol/m3	NaCl mol/m <sup>3</sup>	CaCO <sub>3</sub> mol/m3	
	0	.353	5 5	.502	
	5	.374	60	.520	
	10	.390	65	.539	
	15	.402	70	.557	
	20	.412	75	.572	
	25	.422	80	.584	
	30	.431	85	.591	
	35	.442	90	.590	
	40	.454	95	.579	
	45	.468	100	.555	
	50	.484			

The solubility of calcite in solutions containing CaCl<sub>2</sub> and NaCl

[concentration of  $CaCl_2 = 1.00 \text{ mol/m}^3$ ;

Concentration-dependent equation and precision

$$c_{m}_{CaCO_{3}}$$
 = 0.3530265 + 4.8765 x 10<sup>-3</sup> M - 1.4755 x 10<sup>-4</sup> M<sup>2</sup>  
+ 2.907575 x 10<sup>-6</sup> M<sup>3</sup> - 1.717735 x 10<sup>-8</sup> M<sup>4</sup>  
M = molal concentration of sodium chloride  
precision, s = 0.89%

#### Table 2.47.

The solubility of calcite in solutions containing  $CaCl_2$  and NaCl [concentration of  $CaCl_2$  = 2.47 mol/m<sup>3</sup>;

Ρ

NaCl mol/m <sup>3</sup>	CaCO <sub>3</sub> mol/m3	NaCl mol/m <sup>3</sup>	CaCO <sub>3</sub> mol/m <sup>3</sup>
0	.250	55	.335
5	.263	60	. 339
10	.275	65	. 343
15	.285	70	. 347
20	.294	75	.352
25	.302	80	.357
30	.309	85	. 363
35	.315	90	.369
40	.321	95	. 377
45	.326	100	.385
50	.330		

Concentration-dependent equation and precision

 $c_{m_{CaCO_3}} = 0.250000 + 2.78839 \times 10^{-3} M - 3.31517 \times 10^{-5} M^2$ + 1.87678 x 10<sup>-7</sup> M<sup>3</sup>

M = molal concentration of sodium chloride

precision, s = 0.00%

Table 2.48. The solubility of calcite in solutions containing NaCl. NaHCO- and CaCl.

NaHCO3 mo1/m <sup>3</sup>	NaCl mol/m <sup>3</sup>	CaCl <sub>2</sub> mol/m <sup>3</sup>	P (Pax10 <sup>-5</sup> )	T (K)	CaCO <sub>3</sub> mo1/m <sup>3</sup>
19.3	0.53	0	0.254	300	0.015
2.10	19.79	0	0.254	300	0.150
0	56.38	0	0.274	299	0.700
0	18.65	0.84	0.254	300	0.400

sulfate-water:  $CaSO_4 \cdot 2H_2O$  (gypsum),  $CaSO_4 \cdot \frac{1}{2}H_2O$ (bassanite),  $\gamma$ -CaSO<sub>4</sub> (soluble anhydrite), and  $\beta$ -CaSO<sub>4</sub> (anhydrite). A good deal of controversy exists as to the actual existence of two distinct compounds other than the dihydrate and anhydrite; however, both thermal dehydration studies [99] and x-ray studies [100] providé substantial evidence for the existence of the hemihydrate. On the dehydration of gypsum, water is removed zeolitically but with slight changes in cell parameter due to lack of collapse of the Ca-SO<sub>4</sub> framework until  $n = \frac{1}{2}$ . Further heating expels the remaining water molecules yielding  $\gamma$ -CaSO<sub>4</sub>, again with a slight deformation of the structure and corresponding change in cell parameters. The hemi-hydrate $\rightarrow \gamma$ -CaSO<sub>4</sub> may not be recognized.

Of the four principal phases in the system  $CaSO_4$ - $H_2O$ , only two, the hemihydrate and  $\gamma$ -CaSO<sub>4</sub>, exist metastably. Thus under equilibrium conditions the reaction

# gypsum ⇄ anhydrite + water

occurs without the formation of intermediate compounds. The temperature of the transition of gypsum to anhydrite in pure water is 315 K. Gypsum persists metastably above this temperature where it inverts to the metastable hemi-hydrate at 370 K [92]. The solubilities of gypsum and anhydrite in various saline solutions are shown in figure 2.10. This shows that at 303 K gypsum is the stable phase up to a concentration of 4.8 times the normal salinity of sea water.

The effects of pressure and of different concentrations of NaCl on the gypsum-anhydrite equilibrium temperature have been calculated by Macdonald [101] and are illustrated in figures 2.16 and 2.17. At 314 K dP/dT = $85.4 \times 10^5$  Pa/K if the same pressure acts on all phases, but  $dP/dT = -39.45 \times 10^5$  Pa/K if the rock pressure is assumed to act on the solid and hydrostatic pressure on the liquid phase.

Gypsum in contact with aqueous salt solutions is converted to natural anhydrite at 363.5 K. The mechanism of the reaction is the conversion of gypsum first to the hemi-hydrate and then to natural anhydrite. The investigation shows that gypsum is the stable phase of calcium sulfate precipitated from water solutions at temperatures as high as 370 K. The solid phases occurring during the dehydration of gypsum [102] are summarized in table 2.49.

#### 2.5.7. Additional Information

#### a. Thermodynamics of brine-salt equilibria.

Wood [103] has developed a thermodynamic model for concentrated brines which is capable of predicting the solubilities of many of the common evaporite minerals in chloro-sulfate brines. Solubility curves and solution compositions were predicted for the systems NaCl-KCl-MgCl<sub>2</sub>-CaCl<sub>2</sub>-H<sub>2</sub>O and NaCl-MgSO<sub>4</sub>-H<sub>2</sub>O. The model requires data on the constituent binary and quaternary systems only. Data on the binary systems must include measurements on the unsaturated solutions but solubility data is all that is required for the quaternary systems.

Pitzer et al. [110,111] have discussed several approaches which use equations to provide a convenient analytical representation of the thermodynamic properties of sodium chloride.

b. Models for calculating density and vapor pressure of geothermal brines.

Potter and Haas [104] have developed a model for estimating the density of a brine at a known temperature, pressure and composition using the densities of the component salt solutions in the complex brine. In addition a model for estimating the vapor pressure is also reported. The methods can be used to estimate the partial molal volume and partial molal enthalpy of H<sub>2</sub>O in the natural brine and the partial molal volume change and partial molal heat change for the H<sub>2</sub>O component in the vaporization process. Preliminary steam tables are available [105,106] that give the thermodynamic data for the coexisting liquid and gas phases for the NaCl-H<sub>2</sub>O system, for liquid concentrations between 0 mol NaCl/kgH<sub>2</sub>O and halite saturation at temperatures between 353 and 598 K. The densities of aqueous sodium chloride solutions from 273 to 773 K at pressures up to 2  $\times 10^8$  Pa have also been reported using a regression analysis of available data [107].

At a pressure of 10<sup>5</sup> Pa and with 93 parts per thousand of chlorine by weight, the transition of anhydrite to gypsum is predicted to occur at 303 K. The depth to which gypsum is found in nature will depend on the temperature gradient, composition of groundwaters and ratio of lithostatic to hydrostatic pressure acting on the calcium sulfate deposit.



FIGURE 2.16. Pressure-temperature relations for the reaction gypsum = anhydrite + water.

A. Pure water; same pressure on all phases.

B. Pure water; rock pressure on solid phases, hydrostatic pressure on water.

C. Saturated NaCl solution; same pressure on all phases.

D. Saturated NaCl solution; rock pressure on solid phases; hydrostatic pressure on NaCl solution.



FIGURE 2.17. Ref. [101]. Dependence of the dehydration temperature of gypsum on concentration of NaCl in solution at 10<sup>5</sup> pascal pressure.

Table 2.49. Dehydration of gypsum to anhydrite at 363.5 K

Time (sec)	Initial water lost (%)	Solid Phase
30	0	CaSO <sub>4</sub> ·2H <sub>2</sub> O
120	3.7	CaSO <sub>4</sub> ·2H <sub>2</sub> O and CaSO <sub>4</sub> ·½H <sub>2</sub> O
240	6.2	CaSO4 <sup>2</sup> H <sub>2</sub> O and CaSO4 <sup>1</sup> H <sub>2</sub> O
978	3.1	CaSO4 · 2H2O and CaSO4 · 2H2O
2508	14.9	CaSO <sub>4</sub> ·2H <sub>2</sub> O and CaSO <sub>4</sub> ·½H <sub>2</sub> O
2880	11.7	CaSO <sub>4</sub> ·2H <sub>2</sub> O and CaSO <sub>4</sub> ·½H <sub>2</sub> O
5400	26.8	CaSO4·2H20 and CaSO4·2H20
5700	31.5	CaSO <sub>4</sub> ·2H <sub>2</sub> O and CaSO <sub>4</sub> ·½H <sub>2</sub> O
8178	68.8	CaSO <sub>4</sub> ·½H <sub>2</sub> O
11442	95.2	Anhydrite
15342	95.2	Anhydrite

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Symbols and Units

Symbol	Physical Quantity	Unit
ρ	density	kg m <sup>-3</sup>
S°	entropy	J·mol <sup>-1</sup> K <sup>-1</sup>
$\Delta H_{\rm f}^{\rm o}$	standard enthalpy of formation	kJ mol <sup>-1</sup>
$\Delta G_{\rm f}^{\rm b}$	free energy of formation	kJ mol <sup>1</sup>
C°	heat capacity	J ⋅ mol <sup>-1</sup> K <sup>-1</sup>
$P^{P}$	pressure	N m <sup>-2</sup>
c <sub>m</sub>	concentration	mol dm <sup>3</sup>
K <sub>n</sub>	solubility product	

#### **Conversion Factors from Non-SI Units to SI Units**

0°C	=	273.15 K
1 <b>Å</b>	=	$10^{-10}$ m
l bar	=	10 <sup>5</sup> Pa
l atm	=	101325 Pa
l cal	=	4.184 J
l g cm <sup>−3</sup>	=	$1 \times 10^{3} \text{ Kg m}^{-3}$

### Chapter 3 Mechanical Properties

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#### **3.1.** Introduction

As a general introduction, some typical in situ values of the elastic constants of rock salt are presented as well as a brief introduction to the geological environment and some of the factors affecting the mechanical behavior of rock salt.<sup>1</sup>

#### **3.2. Review of Measurement Methods**

#### **3.2.1. Elastic Constants**

Compression: Data shown in figure 3.2 on compression were obtained by Voronov and Grigor'ev [2] and by Heard et al. [7]. Voronov and Grigor'ev applied

Physical constants of rock salt obtained in situ

These results (salt dome) were obtained in the Winnfield salt dome, Louisiana, using surface geophysical techniques; the bedded salt results are from the GNOME drift, New Mexico.

	Salt Dome	Deviation, %	Bedded Salt	Deviation, %
Longitudinal velocity	4370 m s <sup>-1</sup>	±0.7	4085 m s <sup>-1</sup>	±2.3
Shear velocity	2550 m s <sup>-1</sup>	$\pm 1.2$	2150 m s <sup>-1</sup>	±2.6
Poisson's ratio	0.241	±6.1	0.31	
Modulus of elasticity	35.6 GPa	±4.5	24.5 GPa	
Modulus of rigidity	14.4 GPa	±3.3	9.8 GPa	
Lame's constant	13.4 GPa		16.1 GPa	
Bulk modulus	23.0 GPa		21.7 GPa	
Density	2160 kg m <sup>-3</sup>		2020 kg m <sup>-3</sup>	

Mechanical properties of salt are strongly temperature dependent since deformation and work hardening, due to a specific load, increase and decrease, respectively, with a rise in temperature. Confining pressure (fig. 3.1) also exerts an influence on the mechanical behavior of salt; however, it is less significant than that exerted by temperature. In addition there are several other factors which influence the mechanical properties of in situ rock salt: stress rate application, magnitude of stress difference, grain size, thickness of salt body or formation, and the amount and nature of the impurities present.

Since the pertinent data available at present are inconclusive, and the composition of rock salt and the location of defects strongly influence the mechanical behavior, it has been decided not to present recommended values. It should be noted that there is some doubt (Baar [17]) about the extrapolation of laboratory obtained parameters for use as in situ parameters.

The data are presented as a series of figures and corresponding combined specification and data tables. The curve numbers in circles shown in the figures correspond to the data set numbers in the tables. ultrasonic methods under hydrostatic conditions  $\sigma_1 = \sigma_2$  using two high pressure chambers at 298 K. Heard et al. tested four samples (50 × 32 mm) under hydrostatic conditions to 0.8 GPa, two samples (25 × 22 mm) under quasihydrostatic ( $\sigma_1 = \sigma_3$ ) conditions from 0.8 to 3.2 GPa and applied uniaxial strain loading ( $\epsilon_2 = \epsilon_3$ ) on single sample with single strain gauge.

Elastic Moduli: Dynamic moduli of NaCl give more consistent values than static moduli and, therefore, all modern investigators prefer to use ultrasonic techniques for their measurement, i.e., to calculate them from a measurement of longitudinal and shear wave velocities. Voronov and Grigor'ev measured acoustic velocities of NaCl samples, 6-10 mm long and 15 mm in diameter, using two high pressure chambers of 2.7 cm<sup>3</sup>. The time taken by the ultrasonic wave to travel through the investigated samples was measured with a two channel ultrasonic system to an accuracy of  $\pm 0.01 \ \mu$ s. The experimentally determined pressure dependence of the length of a sample and the change in the travel time of the ultrasonic signal were used to calculate the velocities which were then used to determine Young's modulus, shear modulus, bulk modulus, and Poisson ratio. The measurements were made up to a pressure range of 0-10 GPa and at a temperature of 300 K. It is noteworthy that at pressures less than 0.1 MPa dynamic methods probably give extrinsic values of constants due to open cracks in the samples. The results of these investigations are shown in figures 3.3, 3.4, 3.5, 3.6, 3.7, and 3.8.

<sup>&</sup>lt;sup>1</sup>A comprehensive report [28] was released as this manuscript was completed, treating a number of physical aspects of in-situ rock salt masses. This work should be of value in engineering studies.

Heard et al. [7] measured loading and unloading moduli in uniaxial stress and strain at pressures to 0.7 GPa. They also measured ultrasonic velocities at pressures to 0.4 GPa to find the dynamic values of shear modulus, bulk modulus, and Poisson's ratio. The samples used for static tests were 19 mm in diameter and 38 mm in length, while those for dynamic tests measured 19 mm in diameter and 25 mm in length. The temperature for all tests was 298 K. The range of pressures used by Heard et al. was small—up to 3.2 GPa, but the data obtained is useful in studying the variation of static and dynamic moduli at low confining pressures. The data from these studies are shown in figures 3.5, 3.6, 3.7, 3.8, and 3.9.

In order to study the effect of very high confining pressures on the elastic moduli, Frankel, Rich, and Homan used a pressure range of 2.5-27.0 GPa to measure the velocities. The highest range to which the acoustic velocities had previously been measured was 10 GPa by Voronov and Grigor'ev. To measure the acoustic velocities at these very high pressures it was necessary to use a solid pressure device with a large specimen. Details of the apparatus can be found in Reference [16] and the data have been plotted in figure 3.7.

Morris, Jamieson, and Yarger [4] used the ratio of longitudinal to shear wave velocity, measured up to a pressure of 9 GPa, to determine directly the Poisson's ratio and used shock wave data to determine other moduli. The Poisson ratio was derived from the equation below:

$$\sigma = 0.5 (R^2 - 2) / (R^2 - 1)$$

R being the ratio of the velocities. Before determining the velocities, Morris, Jamieson, and Yarger used third order elasticity theory to correct for a probable uniaxial superimposed stress component. This was an improvement upon the previous methods. They also modified the ultrasonic interferometer so that thicker samples with higher and more uniform pressure distribution could be used. The details of the apparatus can be found in reference [4] and the data have been plotted in figure 3.7.

#### 3.2.2. Stress-Strain and Creep-Strain Data

Data related to figures 3.10 and 3.11 were obtained on samples of halitic rock with a mean grain diameter of 2 mm. Samples were cubical with an 0.106 m edge length. Stresses up to 44.471 GPa were applied using a 444.8 MN triaxial testing machine with an  $0.1 \text{ m} \times 0.1 \text{ m} \times 0.1$ m loading platen.

Three experiments were conducted under triaxial conditions and one test under multiaxial loading

conditions at 293 K. Sample No. 1 was loaded uniaxially, 3 and 4 were triaxially loaded at 4.447 GPa and 13.341 GPa, respectively. Sample No. 2 was multiaxially loaded with lateral stresses of 2.223 GPa and 4.447 GPa.

The differential stress versus confining pressure data shown in figure 3.13 were obtained using uniaxial strain loading. A single sample utilizing a single strain gauge was used. Maximum confining pressure was 700 MPa because of limitations in strain gauge accuracy.

Heard et al. [7] used a single cylinder of fine grained NaCl with 1% porosity for the determination of data shown in figure 3.14 (confining pressure  $\sigma_3 = 100$  MPa). The cylinder dimensions were 19 mm diameter, 38 mm length. Axial and circumferential strain gauges were fitted to the sample which was subjected to uniaxial stress loading and unloading. Several other similar tests were run using different confining pressures. Their results followed the same trend as indicated by the data given in figure 3.14.

Artificial rock salt samples were used by Dreyer [12], to obtain the data in figure 3.36. Mean grain size diameter was 0.1 to 0.6 mm. Time-strain tests were run on samples at temperatures of 302 K, 377 K and 471 K and at pressures of 45.36 GPa, 9.07 GPa, and 0 GPa.

The creep behavior illustrated in figure 3.37 was determined on square rock salt prisms  $(0.04m \times 0.04 \text{ m} \times 0.1 \text{ m})$  using a 44.48 MN constant load lever testing apparatus. Deformation was accurate to  $10^{-2}\%$  and temperature could be controlled to within 0.5 K (Dreyer, [12] 1972). The untempered specimen was banded white rock salt with a mean rock salt content of 98.64%, 1.05% anhydrite, 0.29% Keserite, and 0.02% clay. The tempered sample had a different composition, having 7.56% anhydrite, 1.03% keserite and 0.23% clay.

For details concerning test methods for data shown in figure 3.12, the reader is referred to reference [5].

Nair and Deere [23], Burke [19], Thompson [25], Odé [24], and Baar [17] all presented various forms of straintime data for rock salt. These data are displayed in figures 3.23 to 3.35.

Burke [19] used a dead load compression creep unit fitted with fine grained aluminum oxide platens. Sample deflections were measured using a colinearly mounted dial gauge. Commercially obtained high purity artificial salt samples were used in all cases. Extruded single crystals of  $0.64 \times 10^{-2}$  m diameter and 0.305 m long were used. These crystals were extruded at 573 to 623 K an hour at extrusion rates of 0.254 m to 0.381 m per hour. Certain samples were annealed and then slow cooled. Test temperatures were kept constant at approximately 275 K.

The values produced by Thompson [25] were achieved using a triaxial creep testing machine. The confining pressure provided by oil was measured by a Bourdon gage and kept constant by use of a hydraulic accumulator filled with nitrogen. The axial load was read using a dynamometer between the hydraulic ram and the line leading to the test chamber. The entire test chamber was temperature controlled thermostatically by means of a heating tape wrapped around the chamber. The specimens themselves were of various lengths between 0.203 m - 0.305 m with a diameter of 0.102 m having been drilled from blocks taken in situ from Grand Saline, Texas and Hockley, Texas.

Heard [21] used artificial samples of reagent grade NaCl compacted hydrostatically at 170 MPa for 2 h at 403 K. The apparatus used consisted of an externally heated pressure vessel fitted with an internal force transducer to measure axial strain. Differential stress-strain behavior of annealed jacketed samples of the above NaCl was then determined in tension at a confining pressure of 2 kbar and temperatures of 296 K to 673 K and strain rates ranging from  $10^{-1}$  to  $10^{-5}$  s<sup>-1</sup>

Creep data obtained by Le Comte [22] were achieved using creep apparatus capable of achieving greater than 573 K, and a confining pressure of 100 MPa at a stress difference of 13.8 MPa. Le Comte's results were obtained in compression on artificially made specimens consisting of chemically pure NaCl. Prior to testing these samples were annealed at 573 K and then slowly cooled. For details of the apparatus used refer to reference [22].

Odé [24] and Baar [17] present a synthesis of data collected by other researchers and for identification of the original data the user is referred to each of these documents.

#### 3.2.3. Hardness

The data shown in figure 3.38 were obtained by Strelkov, Shpunt, and Nabutovskaya [15] by using methods developed by them earlier and referred to in Reference [15]. The vibration on the automatic indentor was only 0.3-0.4  $\mu$ m causing the error due to this factor to be negligible.

Ksishsh and Sharkezi [14] used NaCl crystals  $(2 \times 2 \times 6 \text{ mm})$  grown by the Kiropolous method and with cation impurities introduced in them. High purity NaCl crystals were developed by the Bridgeman method. All samples were primarily annealed at 923 K and then cooled at 2°/h. The microhardness was then determined on Model 32 of the Zeiss type instrument with an indentor load of 4 g. The microhardness of each sample was estimated from 30-40 impressions. The results are plotted in figures 3.39 and 3.40.

#### 3.2.4. Joffé Effect

The method described below was used to obtain the data shown in figure 3.41. Polishing of crystals was

achieved by submersing the crystal and agitating in water for 30 seconds. Thereafter a 5–10 second methyl alcohol bath and then a 5 second ether bath was given again using agitation. The crystal was then dried in a hot air stream. If the time in the methyl alcohol and ether was shortened not all the water from the initial bath was removed. This resulted in a small amount of sodium chloride being precipitated on the surface of the crystal as a "stain" or tarnish.

"Painting" of polished crystals was achieved using a drop of saturated sodium chloride solution or distilled water. This drop was "painted" on a specific area of a crystal and then the crystal was air dried. This "painting" produced a precipitate on the surface of the crystal which seems to introduce microflaws in its immediate vicinity.

The crystals had a 1.27 cm gauge length and were water polished, rinsed, and dried so that the cross section was 0.254 cm square. Each crystal was sealed in aluminum grips with Duco cement and heated to 323 K for 24 hours in order to dry the cement. The tests themselves were done on a conventional hard tensile machine at a strain rate of  $5 \times 10^{-5}$  s<sup>-1</sup>.

#### **3.2.5. Radiation Effect Determinations**

Bradshaw et al. [13] used two inch cubes prepared from large blocks of bedded and dome salt to study the effects of ionizing radiation on stress-strain and creep behavior as shown in figures 3.42, 3.43 and 3.47. The test cubes were accurately machined to assure uniform application of pressure and were subjected to irradiation in a gamma field of  $3.2 \times 10^6$  R per hour with a temperature of 343 K inside the chamber. Radiation doses of 0,  $10^6$ ,  $10^7$ ,  $10^8$ , and  $5 \times 10^8$  R were used first at room temperature and then at 473 K.

Most of the investigations done in connection with radiation effects on NaCl were on macrocrystals. Demidova and Gol'denberg [8] used NaCl whisker crystals measuring  $10-100 \,\mu$ m in diameter and irradiated them at room temperature with unfiltered x-radiation for 2-16 hours. This makes it possible to study the difference between macro and whisker crystal behavior on irradiation. The data from these experiments are shown in figures 3.44 and 3.45.

In order to investigate the dislocation density and the correlation existing between interstitials and dislocations which might explain why small irradiation doses produce very little hardening compared to coloration, Inabe and Takeuchi [9] used NaCl crystals grown by the Kiropolous technique. Speciments measuring  $7 \times 7 \times 3$  mm<sup>3</sup> were annealed in air at 923 K for 80 hours and cooled at  $20^{\circ}$ /h to room temperature. Some of these

crystals were heated again and then querch. I The dislocation density of a specimen was determined by counting etch pits on a unit area. Each specimet was irradiated with an exposure rate of 500 R/mon using a rays from a tungsten target. Their results are presented in figure 3.4.7.

#### 3.3. Elastic Properties-Static and Dynamic

Considerable interest has been shown in the invession of the researchers of rock salt in recent y fits. Some of the researchers in this field are Voronov. Grigor'ev, Morris, Yarger, Frank d. Burke and Beard. Although their work provides important information, the data are not sufficient to generate recommended values except in a few cases.

A word of caution is sounded since some withors, notably Baar [17] and Handin [2h] are critical of the significance of elastic properties in the case of work salt. Baar, in particular, regards elastic parameters as insignificant when regarded from a design viewpoint, given the extremely low limits of elastic behavior of rock salt.

In general, dynamic elastic constants are less pensitive to pore crush-up (closing of pore spaces within the salt) that occurs somewhere between 0.05 GPa and 0.2 GPa during the loading of salt specimens than are the static constants. For example, Poisson's ratio,  $\sigma$ , for the static case shows a marked variation at low confining pressures because of pore crush. The dynamically obtained values on the other hand do not show such a pronounced variation. This applies also to both the shear modulus and bulk modulus.

Voronov and Grigor'ev [2] measured the velocities of longitudinal and transverse elastic waves on polycrystalline NaCl samples under quasi-hydrostatic conditions using ultrasonic methods at pressures from 0-10 GPa at 298 K. These velocities were then used to calculate compression, Poisson ratio, bulk modulus, shear modulus, and Young's modulus. Heard et al. [7] investigated in detail the variation of these properties at a low range of pressure under different conditions. They tested NaCl samples with 1.0% porosity to determine loading and unloading moduli in uniaxial stress and uniaxial strain at pressures up to 0.7 GPa, in hydrostatic compression up to 0.8 GPa, and in quasi-hydrostatic compression up to 3.2 GPa. They also determined ultrasonic velocities at pressures up to 0.4 GPa. Morris, Jamieson, and Yarger [4] measured transit times of longitudinal and transverse ultrasonic waves in NaCl as a function of quasi-hydrostatic pressure up to 9.0 GPa. They utilized the ratio of the longitudinal to shear wave velocity to determine Poisson's ratio and shock wave data to obtain other elastic moduli. They also corrected their values for a probable experimposed uniaxial stress component. Frankel et al. [6] used ultrasonic interferometry to measure room te operature longitudinal and shear about the velocities in g decrystalline NaCl at static pressures from 2.5 to 27. CPa.

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The average density of rot' It measured in situ using suffare grophysic metho. is 2160 kg m<sup>-3</sup>. The relationship of lengers ith fining pressure has been studied by Voron , 1 1 (TT ∠ ev [2] up to 8.0 GPa and Pa. The data from these by Heard at ... I gote U investigations are solved in the 3.1 and plotted in figure 3.1. Density van a vie confining pressure is nonlinear but as a standa appartition linearity can be assumed, at least , 1000 Pa. Hydrostatic, quasihydrostatic, and incie cading all yield fairly consistent values.

#### 3. 4 de l'éssion

For a plastic of white Cl, the pressure-volume relationship is of i cost <sup>7</sup>alues of compression at various confining prosente and/or hydrostatic conditions, as calculated Vo ov and Grigor'ev [2] and Heard et al. [7] and in a in table 3.2 and shown in r'ev's values are representfigure 3.2. Voronov e d.Gr. ed by curve 1 and a sup of 1 by them to match closely with the values found on Iridgeman, Albuerne and Drickamer, and De Las Salas an, and Kabalkina. Curves 2 and 3 represent fill and et al [7] values for hydrostatic and uniaxial strain boaders conditions respectively. Their values for a urosta ic and quasi-hydrostatic conditions fall or the same composite curve. For a pressure of 300 c e the variation in compression between curves 1 and 2 as compared with the total compression is a little The masons for this discrepancy are not appare if

Voronov and the general evisional alues of compression, being the average of the minimum stigations, are recommended as the more dependence which.

#### 3.3 C. Vamg's Modulus

The energy states are dynamic values of Young's modulus can be taken as  $2^{-6}$  for and 36.9 GPa, respectively. Voronov and Griger and  $2^{-6}$  used pressure dependencies of the velocities of a main p to 10.0 GPa to calculate Young's modulus repeated by The relationship of Young's modulus repeated for any p, some is shown in figure 3.3 and the corresponding set  $1^{-6}$  given in table 3.3. Burke [19] presents double of the variation of Young's

Data Set	Author(s), Year [Ref.]	Р	ρ	Remarks
1	Voronov, F.F. and Grigor'ev, S.B., 1976 [2]	0 1 2 3 4 5 6 7 8	2614 2248 2322 2388 2449 2506 2559 2610 2658	Densities calculated from wave velocities at 298 K.
2	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	0 0.1 0.2 0.3 0.4	2140 2151 2164 2181 2192	Results obtained dynamically from tests on polycrystalline halite at 298 K.

TABLE 3.1. PRESSURE DEPENDENCE OF DENSITY OF ROCK SALT [Confining Pressure, P, GPa; Density,  $\rho,~kg~m^{-3}$ ]



FIGURE 3.1. Variation of density with confining pressure (curve numbers correspond to data set numbers in matching table).

Data Set	Author(s), Year [Ref.]	Р	/p Loading ۱	ρ <sub>0</sub> Jnloading	Remarks
1	Voronov, F.F. and	0.97	0.965		Polycrystalline samples of sodium
	Grigor'ev, S.B., 1975	1.00	0.963		chloride; quasihydrostatic condi-
	[2]	1.03	0.963		tions; two high-pressure chambers
		1.95	0.931		used at 298 K; ultrasonic method
		2.0	0.932		employed.
		2.62	0.925		
		2.67	0.917		
		3.00	0.906		
		3.03	0.907		
		3.03	0.904		
		3.9	0.885		
		4.0	0.884		
		4.05	0.885		
		4.10	0.88/		
		5.18	0.862		
		5.30	0.858		
		5.70	0.852		
		5.85	0.847		
		6.0	0.846		
		7.0	0.829		
		7.03	0.832		
		7.95	0.817		
		8.00	0.814		
		8.70	0.803		
		8.87	0.803		
		9.23	0.798		
		9.60	0.793		
		9.70	0.790		
		9.90	0.789		
		10.05 10.10	0.788 0.792		
2	Heard, H.C., Abey,	0.0001	1.000	0.9933	Six samples of polycrystalline NaCl
	A.E., Bonner, B.P.,	0.01	0.9991		tested; four samples (50 mm x 32 mm
	and Duba, A., 1975 [7]	0.02	0.9985		dia) tested hydrostatically to 0.8
		0.03	0.9981		GPa $(\sigma_1 - \sigma_3)$ ; two samples (25 mm x
		0.09	0.9976		from 0.8 to 3.2 CPa at 208 K
		0.05	0.9967		110m 0.0 CO 3.2 Hra at 290 K.
		0.07	0.9961		
		0.08	0.9957		
		0.09	0.9952		
		0.10	0.9947	0.9892	
		0.20	0.9893	0.9852	
		0.30	0.9828	0.9814	
		0.40	0.9//5	0.9769	
		0.50	0.9735	0.9727	
		0.80	0.9623	0.9613	
		1.00	0.9544	0.9613	
		1.50	0.9377	0.9377	
		2.00	0.9225	0.9225	
		2.50	0.9090	0.9090	
		3.00	0.8969	0.8969	
		3.20	0.8928	0.8928	

#### TABLE 3.2. PRESSURE DEPENDENCE OF COMPRESSION OF ROCK SALT

[Confining Pressure, P, GPa; Compression,  $\rho_0/\rho$ ]

Data Set	Author(s), Year [Ref.]	Р	q\ <sub>o</sub> q	Remarks
3	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	$\begin{array}{c} 0.76\\ 0.74\\ 0.73\\ 0.48\\ 0.45\\ 0.43\\ 0.39\\ 0.37\\ 0.32\\ 0.27\\ 0.22\\ 0.20\\ 0.18\\ 0.15\\ 0.12\\ 0.10\\ 0.09\\ 0.08\\ 0.07\\ 0.06\\ 0.05\\ 0.05\\ 0.04\\ 0.03\\ 0.02\\ 0.01\\ \end{array}$	0.9656 0.9659 0.9662 0.9749 0.9758 0.9768 0.9782 0.9792 0.9816 0.9847 0.9881 0.9892 0.9908 0.9925 0.9946 0.9953 0.9959 0.9966 0.9975 0.9966 0.9975 0.9981 0.9988 0.9988 0.9988	Uniaxial strain loading, $\varepsilon_2 = \varepsilon_3 = 0$ ; single sample with single strain gauge; maximum confining pressure 689 KPa.



FIGURE 3.2. Pressure dependence of the compression of rock salt (curve numbers correspond to data set numbers in matching table).

modulus with temperature in figure 3.4 and the corresponding table.

The dynamic values of Young's modulus are more consistent as compared with static values. This is a fortunate situation as the data on longitudinal and shear wave velocities in NaCl by various investigators agree closely. Therefore, the corresponding values of Young's modulus could be calculated with a reasonable degree of accuracy using the data on velocities.

#### 3.3.4. Shear Modulus

Table 3.5 shows the values of shear modulus (dynamic) for various values of confining pressure as calculated by Voronov and Grigor'ev [2] while curve 3 in

figure 3.5 is a plot of the same values. Static and dynamic values of shear modulus calculated by Heard et al. [7] are also given. As can be seen from the figure, the dynamic shear modulus increases continuously with pressure in both cases, but the static modulus shows a marked variation at low confining pressures (< 0.1 GPa). Heard et al. related this variation to pore crush-up that occurs somewhere between 0.05 GPa to 0.2 GPa. According to them, static moduli at low pressures are sensitive to closing of pores while dynamic moduli are not.

As the sonic velocities are generally consistent, they can be used to find the values of shear modulus. On this basis, Voronov and Grigor'ev's values may be used as the provisional values.

TABLE 3.3. PRESSURE DEPENDENCE OF YOUNG'S MODULUS OF ROCK SALT [Confining Pressure, P, GPa; Young's Modulus, E<sub>s</sub>, GPa]

Data Set	Author(s), Year [Ref.]	Р	Es	Remarks
1	Voronov, F.F. and Grigor'ev, S.B., 1976 [2]	0 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0	36.91 40.72 44.02 46.85 49.30 51.44 53.39 55.25 57.16	Values calculated from pressure-velocity-density relationship - sonic method; samples were com- posed of compacted, fine, chemically pure NaCl powder.



FIGURE 3.3. Relationship between Young's Modulus and confining pressure (curve numbers correspond to data set numbers in matching table).

Data Set	Author(s), Ye [Ref.]	ear	Т	E	Remarks
1	Burke, P.M., 1	968	290.262	36.830	d = 2  mm
_	[19]		337.036	36,100	d 2 min.
			411,993	34,750	
			456.947	34,240	
			484.788	33,740	
			506.179	33.740	
			544.738	32,900	
			594.027	31.540	
			666.880	29.680	
			711.874	28,580	
			797.520	27,320	
			881.091	25.120	
2	D 1 D M	0(0	006 105		
2	Burke, P.M., I	968	296.400	36.010	d = 2  mm.
	[19]		349.950	34.910	
			401.332	34.240	
			433.440	33.900	
			491.257	32.970	
			531.938	32.380	
			613.313	31.030	
			643.305	30.360	
3	Burke, P.M., 1	968	287.804	36.600	d = 2 mm.
	[19]		309.211	36.350	
			317.796	35.930	
			330.613	36.180	
			433.412	34.330	
			587.639	31.120	
			654.074	29.250	
			951.895	21.900	
			984.015	21.390	
4	Burke, P.M. 1	968	296.303	37,450	$d = 50  \mu m$
	[19]		379.856	35.510	а – эо нш.
			489.135	32,720	
			581.273	30, 350	
			630,556	29.080	
			684.175	26,970	
			754.911	24.760	
			844.978	21,380	
			907.136	19.520	
			941,400	18,920	
			990,609	18 760	

TABLE 3.4. EFFECT OF TEMPERATURE ON DYNAMIC YOUNG'S MODULUS OF NaC1 [Temperature, T, K; Young's Modulus, E, MPa]

#### 3.3.5. Bulk Modulus

Voronov and Grigor'ev's [2] values of bulk modulus have been plotted as curve 2 of figure 3.6 while curves 1, 3, and 4 represent bulk modulus data from Heard et al. [7] under various conditions of testing. These data are also tabulated in table 3.6. The minimum difference between dynamic bulk modulus measured by Voronov and Heard, respectively, is 2.4 GPa. The values for other conditions also differ considerably. As a general trend, both static and dynamic values of bulk modulus increase with confining pressure at pressure values > 0.2 GPa. Recommended values cannot be generated at this stage.

#### 3.3.6. Poisson's Ratio

The relationship between Poisson's ratio and confining pressure is shown in figure 3.7 for dynamic and static cases and the corresponding values are tabulated in table 3.7. The dynamic values of Poisson's ratio calculated by Voronov and Grigor'ev [2] agree closely with those calculated by Morris et al. [4]. However, the corresponding values as determined by Heard et al. [7] differ from other data by approximately 8.0%. Voronov's values of Poisson's ratio may be used as provisional values because of their close agreement with Morris' data.

#### 3.3.7. Wave Velocities

Data on longitudinal and shear wave velocities from Voronov and Grigor'ev [2], Heard et al. [7], Morris, Jamieson, and Yarger [4], and Frankel, Rich, and Homan [16] have been plotted in figure 3.8 and also given in table 3.8. These values are seen to agree within the uncertainty of measurements. Frankel et al. [16] values represent the largest range of pressure and may be used as the recommended values. These longitudinal and shear acoustic velocities in polycrystalline NaCl were measured at static pressures in the range of 2.5-27.0 GPa at 300 K. The measurements were made by ultrasonic



FIGURE 3.4. Temperature dependence of Young's Modulus.

TABLE 3		TAE.	STRE	PEPENDENCE	Ē	SHL	MODULUS	0F	ROCK	SALI
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...... Plastore, P, GPL She and Har, C, GPa]

Data Set	Er(s), Year (s.a.			Remarks
1	H .C. H.C., U.	1. Jan 19	12.5	e: is values; five cylindrical samples
	A.L., Bonner, B.T	10	13.4	is its as 38 mm length); uniaxial load-
	and Duba, A., 197. 199	· 0-0	14.41	img; strain measured with axial and circum-
		1. 175	14.81	ial merain gauges.
		0 100	15.00	
		0.150	15.23	
		0.500	15.31	
		0.250	15.43	
		2.300	15.35	
		0.350	15.59	
		1 300	15.91	
2	Ford D.C. et	610	13,80	for the salues: uniaxial strain loading
	19 5 171	1.020	11.50	hiti ag.
	· · · · · · · · · · · · · · · · · · ·	1.100	15.20	
		400	14.00	
3	V. may F.F. ut		14.61	anic values obtained using ultrasonic
0	Griori, v. C. 1	· )	15.97	(1995) (1 298 K.
	100	2.0	17.05	
	•	1.0	17.97	
	ŝ	4.U	18.75	
		5 0	19 44	
		6	20.08	
		7.0	20.72	
		5. (1	21.39	



FIGURE 3.5. Variation of shear modulus with confining pressure (curve numbers correspond to data set numbers in matching table).

Data Set	Author(s), Year [Ref.]	Р	K <sub>s</sub>	Remarks
1	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	$\begin{array}{c} 0.00\\ 0.02\\ 0.02\\ 0.11\\ 0.12\\ 0.15\\ 0.17\\ 0.21\\ 0.24\\ 0.26\\ 0.29\\ 0.31\\ 0.33\\ 0.38\\ 0.45\\ 0.54\\ 0.70\\ 0.90\\ \end{array}$	$11.15 \\ 12.30 \\ 15.08 \\ 17.71 \\ 20.00 \\ 20.66 \\ 20.66 \\ 20.34 \\ 19.03 \\ 17.55 \\ 16.22 \\ 16.08 \\ 16.08 \\ 17.07 \\ 18.71 \\ 21.01 \\ 22.82 \\ 25.12 \\ 27.26 \\ 100 \\ 10$	Hydrostatic and quasi-hydrostatic loading; samples were dry, polycrystalline, fine grained NaCl (99.4-99.9% pure); porosity 1.1%; samples were partially work hardened; measurements made at 296 K.
		1.15 1.51 1.86 2.33 2.85 3.09 3.22	29.73 32.38 35.35 38.32 41.63 43.12 41.11	
2	Voronov, F.F. and Grigor'ev, S.B., 1976 [2]	0.0 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0	25.23 30.18 35.07 39.79 44.24 48.36 52.08 55.34 58.10	Dynamic test results; longitudinal and trans- verse wave velocities are ultrasonic at pres- sures 0-10 GPa; sample material pure, fine polycrystalline NaCl; measurements made at 298 K.
3	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	0.0 0.1 0.2 0.3 0.4	18.98 22.63 23.20 24.27 24.19	Two different dynamic test techniques were used to obtain shear wave velocity and longi- tudinal wave velocity; variability between two methods greatest at ambient temperature - $11\%$ in $V_{long}$ and $8\%$ in $V_{shear}$ ; sample composition as for Data Set 1.
4	Heard, H.C., et al., 1975 [7]	0.01 0.02 0.1 0.4	21.3 17.3 23.8 22.0	Static uniaxial loading was used; sample compo- sition as for Data Set 1; measurements made at 296 K.

TABLE	3.6.	PRES	SSURE	DEPER	NDEN	ICE O	F BULI	K MODULUS	OF	ROCK	SALT
	[Config	ning	Press	sure,	Ρ,	GPa;	Bu1k	Modulus,	К_	GPa]	



FIGURE 3.6. Variation of bulk modulus with confining pressure (curve numbers correspond to data set numbers in matching table).

)ata Set	Author(s), Year [Ref.]	Р	μ	Remarks
1	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	0.01 0.02 0.1 0.2	0.26 0.32 0.24 0.29	Static uniaxial loading test; ratio obtained by using transverse and axial strain gauges; measurements made at 298 K.
2	Voronov, F.F. and Grigor'ev, S.B., 1976 [2]	0.0 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0	0.256 0.275 0.291 0.304 0.314 0.323 0.329 0.334 0.336	Dynamic results calculated from sound veloci- ties; measurements made at 298 K.
3	Morris, C.E., Jamieson, J.C., and Yarger, F.L., 1976 [4]	0.00 1.50 3.06 4.50	0.250 0.280 0.300 0.315	Dynamic results calculated from measurements obtained using a specially modified pressure cell; samples composed of reagent grade NaCl (99.5% pure).
4	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	0.0 0.1 0.2 0.3 0.4	0.230 0.229 0.230 0.236 0.230	Dynamic results calculated from ultrasonic velocities for pressures between 0 and 0.4 GPa and at a temperature of 298 K.

TABLE	3.7.	PRESSI	JRE DEPEND	ENCI	E OF	POISSON'S	RATIO	OF	ROCK	SAL
		[Confining	Pressure,	Ρ,	GPa;	Poisson':	s Ratio	o, (	ז]	



FIGURE 3.7. Variation of Poisson's Ratio with confining pressure (curve numbers correspond to data set numbers in matching table).

interferometry in a variable lateral support Bridgeman anvil device. The previous measurements of velocities in the range of 0-1) GPa agree with these values. As can be seen from the figure, at higher pressures the shear wave velocity is almost constant or increases very gradually with increasing pressure. Figure 3.9 (after Heard) also indicates that at lower values of confining pressure the velocity increases rapidly with increasing pressure, but at higher values of confining pressure, the increase in velocity is gradual and small.

#### 3.4. Strength and Creep

Due to the low limit of elasticity of rock salt, it is hard to divorce strength and creep. To quote Handin [20], "Strength is a meaningless term unless all environmental conditions are specified". In tests of short duration, the terms yield strength or ultimate strength or stress at a given strain are appropriate provided pressure, temperature, and chemical environment are specified. To quote Handin [20] further, with reference to the term strength, "It is better to avoid the term altogether for tests of long duration since there is no obvious connection between rigidity and creep". Odé [24] makes the following statement: "It is not known yet whether rock salt has a true yield limit, but, if it does the limit is low". From these quotes by both Handin and Odé, it is apparent that difficulties exist in the definition of strength for an elasto-plastic material like rock salt.

Bearing such comments in mind, it is difficult to reconcile the claims and statements of various researchers. It is suggested that possibly the elastic-ductile transition is perhaps a distinction criterion between strength and creep provided all conditions are specified.

Baar [17] claims much of the technical and scientific literature on salt rocks is misleading. The reason given is that laboratory testing gives different behavior than that found in-situ. Laboratory strength testing causes "work hardening" which does not occur in-situ. From an engineering viewpoint it appears that laboratory obtained parameters are possibly not valid. An example occurs in underground excavations where most rocks behave elastically; however, this does not occur in salt rocks because they display stress relief creep.

Generally, salt rocks are elasto-plastic and behavior will be elastic unless the  $(\sigma_1 - \sigma_3)$  stress difference exceeds the limit of elasticity. Such rocks reassume elastic behavior once the stress difference has dropped below a certain critical value. It should be noted that stress difference initiates creep and not stress magnitude.

In particular, Baar [17] disagrees with the ideal creep curves obtained by many researchers. It is his contention that the decreasing creep rates displayed by such curves are a manifestation of work hardening, something not often found in situ.

Assuming a viscous analogue, salt may be assigned an equivalent viscosity. This viscosity behavior is a

Data Set	Author(s), Year [Ref.]	Р	v	Remarks
1	Frankel, J., Rich, F.J.,	2.5	5007	Longitudinal wave velocity; polycrystalline
	and Homan, C.G., 1976	3.0	5088	NaCl; longitudinal wave velocity measured at
	[16]	3.5	5165	static pressures from 2.5-27.0 GPa at 300 K;
		4.0	5238	Bridgeman Anvil device used for velocity
		4.5	5307	measurements.
		5.0	5380	
		5.5	5450	
		6.0	5585	
		7.0	5648	
		7.5	5710	
		8.0	5769	
		9.0	5877	
		10.0	5986	
		11.0	6092	
		12.0	6193	
		13.0	6290	
		15.0	6478	
		17.0	6647	
		19.0	6785	
		21.0	6915	
		23.0	7056	
		25.0	7304	
			0670	
2	Frankel, J., et al.,	2.5	2679	Shear wave velocity; sample specifications and
	1910 [10]	3.0	2090	testing conditions are the same as above.
		5.5	2710	
		4.5	2722	
		5.0	2750	
		5.5	2768	
		6.0	2785	
		6.5	2804	
		7.0	2820	
		7.5	2835	
		8.0	2849	
		9.0	2867	
		10.0	2894	
		11.0	2923	
		12.0	2950	
		13.0	2976	
		17.0	3033	
		19.0	3083	
		21 0	3088	
		23.0	3123	
		25.0	3154	
		27:0	3169	
3	Voronov, F.F. and	0	4551	Longitudinal wave velocity; ultrasonic method
	Grigor'ev, S.B., 1975	1	4785	used on polycrystalline NaCl samples under
	[2]	2	4989	quasi-hydrostatic conditions; measurements
		3	5166	made at 298 K.
		4	5317	
		5	5445	

TABLE 3.8. PRESSURE DEPENDENCE OF LONGITUDINAL AND SHEAR WAVE VELOCITIES OF ROCK SALT [Confining Pressure, P, GPa; Velocity, v, m s<sup>-1</sup>]

Data Set	Author(s), Year [Ref.]	Р	v	Remarks
3	Voronov, F.F. and	6	5551	
cone.)	[2]	8	5708	
4	Voronov, F.F. and Grigor'ev, S.B., 1975 [2]	0 1 2 3 4 5 6 7 8	2606 2665 2709 2743 2767 2786 2802 2818 2837	Shear wave velocity; conditions same as above.
5	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	$\begin{array}{c} 0.000\\ 0.010\\ 0.020\\ 0.050\\ 0.075\\ 0.100\\ 0.150\\ 0.200\\ 0.250\\ 0.300\\ 0.350\\ 0.400 \end{array}$	4078 4310 4371 4419 4453 4463 4463 4463 4509 4538 4509 4538 4530 4549	Longitudinal wave velocity; ultrasonic veloci- ties calculated on 4 small samples (19 mm diameter x 25 mm length) and 2 slightly larger samples; transducers were polycrystalline ceramic Pb(Zn,Ti)O <sub>3</sub> polarized for transverse shear with dominant frequency of 1 MHz.
6	Heard, H.C., et al., 1975 [7]	0.000 0.020 0.050 0.100 0.150 0.200 0.250 0.300 0.350 0.400	2419 2509 2591 2629 2636 2659 2657 2666 2668 2676 2685	Shear wave velocity; test conditions similar to above.



FIGURE 3.8. Variation of longitudinal wave velocity and shear wave velocity with high confining pressures (curve numbers correspond to data set numbers in matching table).



FIGURE 3.9. Variation of longitudinal wave velocity and shear wave velocity with lower confining pressures (curve numbers correspond to data set numbers in matching table).

function of temperature, confining pressure, differential stress and time. Assuming that creep of salt takes place by a steady state mode there are factors such as axial stress, grain size, temperature and confining pressure which affect its behavior.

Le Comte [22] investigated the above four factors and drew the following conclusions. In the case of the axial stress an increase in the stress produces an increase in creep rate. An increase in grain size on the other hand decreases that creep rate. Confining pressure tends to decrease the creep rate, whereas, an increase in pressure increases the creep rate several fold. Of these factors the temperature effect is by far the most significant and exerts the greatest influence.

Due to the controversy surrounding the term "strength" when applied to rock salt, it has been decided to drop this term and rather to designate data in a general way as "stress-strain" or as "creep" data. It is then left to the user as to which of the two groups best satisfies his needs.

#### 3.4.1. Stress-Strain Data

In the case of stress, the primary quantities are the principal stresses  $\sigma_1$ ,  $\sigma_3$ , the differential stress ( $\sigma_1-\sigma_3$ ), and the shear stress,  $\tau$ . On occasions a relationship between differential stress and the minor principal stress ( $\sigma_3$ ) is also used.

Initially, in almost every case, the relationship at either low confining stress or strain displays behavior with an elastic component. Beyond a certain stress ( $\sigma_3$ ) or strain, however, the salt shows more of a plastic character. The former behavior may be regarded as elastic, whereas the latter is plastic in nature.

In the case of some relationships between shear stress and strain, the elastic-plastic transition is not pronounced and has arbitrarily been taken to occur at about 0.2% axial strain. The above transition is observed at 298 K; however, this transition changes and may even almost disappear depending on the prevailing temperature.

Dreyer's [12] data on shear and normal stress and their variation with test conditions are tabulated in tables 3.9 and 3.10 and are shown in figures 3.10 and 3.11, respectively. In general, the relationship suggests that the influence of strain hardening is small and, as expected, the shear stress bearing capacity is a minimum under uniaxial loading and increases as the confining pressure increases.

The effect of temperature and confining pressure on the deformation of halite single crystals has been studied by Gera [5] and can be seen in Figure 3.12 with the corresponding values in Table 3.11. From the figure it is observed that as temperature increases, creep also increases, and that the effect of confining pressure is secondary. This latter observation is clear from the small difference between the 100 MPa and 200 MPa curves.

TABLE 3.9.	RELATIONSH	IP BETWEEN	SHEAR S	TRESS AND	STRAIN FOR
	ROCK SALT	UNDER VARY	ING TEST	CONDITION	NS

[Shear Stress,  $\tau$ , GPa: Strain,  $\epsilon$ , %]

Data Set	Author(s), Year [Ref.]	τ	З	Remarks
1	Dreyer, W., 1972 [12]	2.206 3.625 4.650 5.243 5.639 5.887 6.037 6.119 6.239 6.320 6.362	0.15 0.33 0.52 0.74 0.95 1.13 1.35 1.57 1.74 1.95 2.16	Cubical samples of halite with 10.6 cm edge length; grain size distribution homogeneous; uniaxially loaded - $\sigma_2 = \sigma_3$ , $\sigma_3 = 0$ ; room tem- perature.
2	Dreyer, W., 1972 [12]	3.309 4.649 5.399 5.795 6.034 6.312 6.472 6.671 6.791 6.872 6.953	0.22 0.45 0.64 0.85 1.06 1.25 1.46 1.67 1.84 2.05 2.25	Sample similar to above; multiaxially loaded; $\sigma_2 \neq \sigma_3$ , $\sigma_2 = 4.447$ GPa, $\sigma_3 = 2.223$ GPa; room temperature.
3	Dreyer, W., 1972 [12]	2.678 5.081 5.989 6.384 6.583 6.744 6.903 7.024 7.144 7.186 7.306 7.309	$\begin{array}{c} 0.13\\ 0.34\\ 0.55\\ 0.74\\ 0.93\\ 1.18\\ 1.37\\ 1.56\\ 1.76\\ 1.98\\ 2.16\\ 2.39 \end{array}$	Sample similar to above; $\sigma_2 = \sigma_3$ , $\sigma_3 = 4.447$ GPa; room temperature.
4	Dreyer, W., 1972 [12]	2.204 3.228 5.611 6.500 6.974 7.252 7.412 7.572 7.653 7.734 7.855 7.975 8.057 8.177	$\begin{array}{c} 0.07\\ 0.10\\ 0.34\\ 0.51\\ 0.72\\ 0.95\\ 1.14\\ 1.35\\ 1.56\\ 1.75\\ 1.98\\ 2.17\\ 2.39\\ 2.58 \end{array}$	Sample similar to above; $\sigma_2 = \sigma_3$ , $\sigma_3 = 13.341$ GPa; room temperature.



FIGURE 3.10. Shear stress-strain behavior of rock salt for different test conditions (curve numbers correspond to data set numbers in matching table).

TABLE 3.10. STRESS-STRAIN RELATIONSHI	P FOR ROCK SAL	T UNDER VARYING TEST	CONDITIONS
---------------------------------------	----------------	----------------------	------------

[Stress,  $\sigma_1$ , GPa; Strain,  $\epsilon$  , %]

Data Set	Author(s), Year [Ref.]	σ1	ε	Remarks
1	Dreyer, W., 1972 [12]	3.234 7.142 9.164 10.511 11.185 11.724 11.994 12.129 12.263 12.533 12.802	0.06 0.28 0.49 0.68 0.90 1.10 1.32 1.51 1.73 1.92 2.11	Cubical sample of halite with 10.6 cm edge length; uniaxially loaded, $\sigma_2 = \sigma_3$ , $\sigma_3 = 0$ ; room temperature.
2	Dreyer, W., 1972 [12]	3.234 8.760 11.455 13.072 13.341 14.015 14.419 14.959 15.363 15.632 15.767 16.037 16.037	$\begin{array}{c} 0.03 \\ 0.19 \\ 0.39 \\ 0.58 \\ 0.71 \\ 0.90 \\ 1.10 \\ 1.32 \\ 1.52 \\ 1.73 \\ 1.95 \\ 2.14 \\ 2.33 \end{array}$	Sample similar to above; σ <sub>2</sub> ≠σ <sub>3</sub> , σ <sub>2</sub> =4.447 GPa, σ <sub>3</sub> =2.223 GPa; room temperature.
3	Dreyer, W., 1972 [12]	9.703 14.419 16.576 17.115 17.249 17.657 17.923 18.193 18.597 18.732 18.866 19.136	0.08 0.28 0.49 0.69 0.88 1.08 1.32 1.51 1.71 1.92 2.12 2.33	Sample similar to above; σ <sub>2</sub> =σ <sub>3</sub> , σ <sub>3</sub> =4.447 GPa; room temperature.
4	Dreyer, W., 1972 [12]	19.54 24.39 26.144 27.087 27.626 28.030 28.300 28.569 28.839 29.108 29.243 29.648 29.917	0.08 0.27 0.47 0.68 0.88 1.08 1.29 1.49 1.71 1.90 2.11 2.29 2.51	Sample similar to above; $\sigma_2=\sigma_3$ , $\sigma_3=13.341$ GPa; room temperature.



FIGURE 3.11. Normal stress-strain behavior of rock salt for different test conditions (curve numbers correspond to data set numbers in matching table).

TABLE 3.11.	RELATIONSHIP BETWEEN	DIFFERENTIAL	STRESS AND STRAIN FOR	SINGLE HALITE CRYSTALS
	AT VARYING CONFINING	PRESSURE AND	TEMPERATURE	

[Differential Stress  $(\sigma_1 - \sigma_3)$ , MPa; Strain,  $\varepsilon$ , %]

Data Set	Author(s), Year [Ref.]	$(\sigma_1 - \sigma_3)$	З	Remarks
1	Gera, F., 1972 [5]	0.42	0.11	Halite single crystals; deformed dry in com-
		9.30	0.23	pression at 200 MPa; temperature 297 K; data
		20 21	4 12	obtained from smooth curves.
		27.75	7.68	
		34.86	11.03	
		41.97	14.70	
		49.08	18.26	
		54.09	21.28	
		58.27 59.94	23.44 24.63	
2	Comp E 1072 [5]	0.95	0.00	Consistent similar to show a deferred day in
2	Gera, F., 1972 [5]	9.29	0.00	compression at 100 MPa: temperature 297 V:
		15.18	2.28	data obtained from smooth curves
		19.36	4.23	alla obtained ifon theoten curves.
		23.97	6.49	
		28.57	8.76	
		33.17	11.24	
		39.01	14.80	
		44.86	18.15	
		52 36	20.63	
		54.86	23.76	
3	Gera, F., 1972 [5]	1.27	0.11	Specimen similar to above: deformed dry in
		10.11	1.74	compression at 2000 MPa; temperature 423 K;
		13.02	4.11	data obtained from smooth curves.
		16.33	7.34	
		20.46	11.76	
		24.18	12.86	
		28.69	21.99	
		30.76	24.26	
4	Gera, F., 1972 [5]	4.22	0.33	Sample similar to above; deformed dry in com-
		10.11	1.95	pression at 100 MPa; temperature 423 K; data
		14.25	5.73	obtained from smooth curves.
		16.31	8.31	
		21 25	14 67	
		22.87	17.47	
		24.09	19.84	
		25.32	21.56	
		26.55	23.50	
5	Gera, F., 1972 [5]	1.27	0.11	Sample similar to above; deformed dry in com-
		8.02	0.98	pression at 200 MPa; temperature 573 K; data
		9.24	2.81	obtained from smooth curves.
		8.29	7 55	
		8.67	9.38	
		9.49	10.67	
		10.73	11.96	
		11.12	13.47	
		11.02	15.62	
		11.02	18.10	
		10.96	20.36	
_		10.07	22.40	



FIGURE 3.12. Differential stress-strain relationship at several temperatures and different confining pressures (curve numbers correspond to data set numbers in matching table).

Another relationship of interest is that of differential stress versus confining pressure which is shown in figure 3.13. The corresponding data are taken from ref. [7] and reported in table 3.12. It can be observed that after a maximum differential stress of about 50 MPa has been achieved, there is a decrease in differential stress ( $\sigma_1$ - $\sigma_3$ ) as  $\sigma_3$  increases. This behavior has been attributed by Heard et al. [7] to pore collapse in the rock salt and continues until confining pressure has reached a value of about 230 MPa after which differential stress increases with confining pressure.

Axial and circumferential strain of rock salt samples as a function of stress difference during triaxial loading and unloading are presented in figure 3.14 with the corresponding values in table 3.13. The data have been taken from ref. [7] and indicate that for cylindrical samples with an L/D ratio = 2, and loads>50 MPa, there is a marked change in the slope of both stress-strain curves. This implies two different modes of behavior beyond this 50 MPa demarcation, i.e., elastic-plastic transition.

Typical differential stress-strain curves for annealed halite aggregates are illustrated in figures 3.15 to 3.19 and tables 3.14–3.18 for a broad range of strain rates at 273 K to 400 K (Heard [21]). It is noteworthy that strain hardening is decreased by decreasing strain rate or increasing temperature. Steady-state flow is closely approximated during most of the deformation at  $10^{-8}$  s<sup>-1</sup> and 373 K. The onset of steady-state flow occurs at somewhat higher rates at intermediate temperature, and at 673 K, strain hardening appears dominant only at the highest rates investigated.

Figures 3.20 and 3.21 and tables 3.19-3.20 show stress-strain results as a function of temperature at two strain rates,  $10^{-5}$  and  $10^{-7}$  s<sup>-1</sup> at a confining pressure of 200 MPa. In both of these cases, strain hardening disappears as the intermediate temperatures are reached.

A comparison of the behavior of annealed and unannealed rock salt samples which are work hardened to some degree can be observed in figure 3.22 and table 3.21 which represent data from Gera [5]. The annealed sample shows lower shear stress resistance as evidenced by the greater amount of strain it undergoes for the same load compared to the unannealed sample. This lower resistance of the annealed sample is thought to be caused by recrystallization that occurs during annealing allowing the rock salt to revert to its former state (i.e., work hardening effect is destroyed).

TABLE 3.12.	VARIATION OF DIFFERENTIA	L STRESS WITH	CONFINING	PRESSURE	FOR
	UNIAXIAL STRAIN LOADING	OF ROCK SALT			

[Confining	Pressure,	σ,,	MPa;	Differential	Stress,	$(\sigma_1 - \sigma_3)$	), MP;	a]
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Data Set	Author(s), Year [Ref.]	σ₃	$(\sigma_1 - \sigma_3)$	Remarks
1	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	4.90 6.12 11.23 11.17 12.41 16.22	18.39 23.23 26.14 30.65 34.20 38.08	Dry, fine grained, polycrystalline NaCl with 1% porosity; uniaxial strain loading ( $\sigma_2=\sigma_3=$ 0); maximum confining pressure 100 MPa; temperature 296 K.
		26.44 46.99 59.83 71.39 80.37	42.93 45.52 48.12 50.10 51.68	
		111.26 126.70 135.72 155.03 160.21	51.06 51.07 50.12 49.49 47.23	
		197.52 227.16 243.87 274.74 296.57	47.23 47.91 44.39 45.69 46.69 49.93	
		322.31 378.85 425.15 663.06 681.06	49.95 55.48 57.11 67.98 68.96	
		697.77 699.12 641.62 600.92	70.27 65.43 35.38 -0.136	



FIGURE 3.13. Relationship of differential stress to confining pressure of rock salt under uniaxial strain loading (curve numbers correspond to data set numbers in matching table).

## TABLE 3.13. AXIAL ( $\epsilon_1$ ) AND CIRCUMFERENTIAL ( $\epsilon_3$ ) STRAINS AS A FUNCTION OF STRESS DIFFERENCE ON UNIAXIAL STRESS LOADING AND UNLOADING

[Differential S	Stress, (o	$(1 - \sigma_3),$	MPa;	Strain,	ε]	
-----------------	------------	-------------------	------	---------	----	--

Data Set	Author(s), Year [Ref.]	$(\sigma_1 - \sigma_3)$	ε	Remarks
1	Heard, H.C., Abey, A.E., Bonner, B.P., and Duba, A., 1975 [7]	3.899.9326.7043.7355.5159.3366.4174.4380.7566.2941.0513.01	$\begin{array}{c} 0.000\\ 0.000\\ -0.001\\ -0.002\\ -0.004\\ -0.006\\ -0.010\\ -0.023\\ -0.039\\ -0.048\\ -0.045\\ -0.045 \end{array}$	Axial strain ( $\varepsilon_1$ ); dry, fine grained, poly- crystalline NaCl with 1% porosity; uniaxial stress loading and unloading; $\sigma_3$ =100 MPa.
2	Heard, H.C., et al., 1975 [7]	3.89 9.67 26.44 55.32 66.37 71.08 78.06 82.02 65.82 12.48	0.000 0.000 0.001 0.004 0.007 0.012 0.019 0.020 0.020	Circumferential strain (E3); sample and test conditions same as above.



FIGURE 3.14. Axial  $(\epsilon_1)$  and circumferential  $(\epsilon_3)$  strain as a function of differential stress (curve numbers correspond to data set numbers in matching table).

TABLE 3.14.DIFFERENTIAL STRESS-STRAIN CURVE FOR POLYCRYSTALLINE HALITE<br/>EXTENDED AT 200 MPa, 373 K, AND  $\dot{\varepsilon} = 1.5 \times 10^{-3}$  TO<br/> $1.5 \times 10^{-8}$  s<sup>-1</sup>

[Strain, E	:, %;	Differential	Stress, (	$\sigma_1 - \sigma_3$	) MPa]
------------	-------	--------------	-----------	-----------------------	--------

Data Set	Author(s), Year [Ref.]	ε	$\sigma_1 - \sigma_3$	Remarks
			· _, , , , , , , , , , , , , , , , , , ,	
1	Heard, H.C., 1972	0.000	4.988	$\dot{\varepsilon} = 1.5 \times 10^{-3} \text{ s}^{-1}$
-	[21]	0.087	9.977	
	[]	0.218	14.966	
		0.480	17.728	
		0.655	19.955	
		1.004	22.449	
		1.441	25.033	
		1.878	27.171	
		2.576	29.309	
		3.712	31.804	
		4.978	33.674	
		6.943	35.902	
		8.603	37.327	
		9.869	38.307	
		11.354	39.287	
2	Heard, H.C., 1972	0.655	12.294	$\dot{\epsilon} = 1.5 \times 10^{-4} \text{ s}^{-1}$
	[21]	1.004	14.877	
		1.616	18.262	
		2.358	20.935	
		3.537	23.875	
		5.371	26.726	
		7.031	28.418	
		8.777	30.111	
		10.131	31.180	
		11.616	32.249	
3	Heard, H.C., 1972	0.262	10.155	$\dot{\varepsilon} = 1.5 \times 10^{-5} \text{ s}^{-1}$
	[21]	0.742	15.055	
		1.354	18.351	
		2.052	20.222	
		2.314	20.935	
		3.362	22.539	
		5.066	24.409	
		6.376	25.389	
		7.904	26.369	
		9.127	26.993	
		10.611	27.616	
		11.528	27.884	

Data	Author(s), Year	ε	01-03	Remarks
Set	[Ref.]		······	
4	Heard, H.C., 1972	0.087	2,405	$\dot{c} = 1.5 \times 10^{-6} \text{ s}^{-1}$
•	[21]	0.175	4,988	0 1.0 A 10 -
	[21]	0.262	6 770	
		0.437	9,977	
		0.611	11,492	
		1.004	13,363	
		1.703	15.055	
		2.402	16 302	
		3.712	17,995	
		5.066	19.420	
		6,201	20.311	
		7,991	21,469	
		9,389	22.093	
		10,699	22.717	
		11,310	22.806	
		111510	22.000	
5	Heard, H.C., 1972	0.568	10.957	$\dot{\varepsilon} = 1.5 \times 10^{-7} \text{ s}^{-1}$
	[21]	1.310	12.472	
	[22]	2.271	13.897	
		3.450	15.233	
		4.585	16.124	
		6.201	17.104	
		7.467	17.728	
		8.908	18.262	
		10.000	18.619	
		10.699	18.708	
		0 ( ) 7	0 175	. 1 . 10-8 -1
6	Heard, H.C., 1972	0.437	9.175	$\varepsilon = 1.5 \times 10^{\circ} \text{ s}^{\circ}$
	[21]	0.568	9.621	
		0.742	9.977	
		1.354	10.423	
		2.183	10.779	
		3.302	11 (02	
		4.803	11 501	
		0.394	11.501	
		7.904	11 501	
		9.127	11 501	
		10.202	11.001	

TABLE 3.14. DIFFERENTIAL STRESS-STRAIN CURVE FOR POLYCRYSTALLINE HALITE EXTENDED AT 200 MPa, 373 K, AND  $\hat{\varepsilon}$  = 1.5 x 10<sup>-3</sup> TO 1.5 x 10<sup>-8</sup> s<sup>-1</sup> (Continued)



FIGURE 3.15. Differential stress-strain curves for polycrystalline halite at 373 K.

#### TABLE 3.15. DIFFERENTIAL STRESS-STRAIN RELATIONSHIP FOR POLYCRYSTALLINE HALITE AT 200 MPa, 473 K, AND $\dot{\epsilon} = 1.8 \times 10^{-2}$ TO 1.2 x 10<sup>-8</sup> s<sup>-1</sup>

Data Set	Author(s), [Ref.]	Year	ε	σ1-σ3	Remarks
1	Heard, H.C.,	1972	0.050	4.955	$\dot{\epsilon} = 1.8 \times 10^{-2} \text{ s}^{-1}$
	121]		0.145	9.999	
			0.200	12.299	
			1.034	17.516	
			1.785	19,990	
			2.842	22.020	
			3.811	23.254	
			4.823	24.310	
			5.880	25.366	
			7.904	26.949	
			9.883	28.000	
			11.686	28.610	
2	Heard, H.C.,	1972	0.635	14.598	$\dot{\varepsilon} = 1.5 \times 10^{-3} \text{ s}^{-1}$
	[21]		1.032	16.100	
			1.385	16.806	
			1.869	17.335	
			3.849	19.006	
			5.917	20.145	
			7.984	21.196	
			9.919	22.070	
			11.107	22.507	
3	Heard, H.C.,	1972	0.323	11.591	$\dot{\varepsilon} = 1.5 \times 10^{-4} \text{ s}^{-1}$
	[21]		0.764	12.916	
			1.161	13.533	
			1.821	14.149	
			3.889	15.731	
			5.913	16.959	
			7.892	17.745	
			9.914	18.265	
			11.233	18.524	
4	Heard, H.C.,	1972	0.051	5.044	$\dot{\varepsilon} = 1.2 \times 10^{-4} \text{ s}^{-1}$
	[21]		0.141	6.901	
			0.495	9.023	
			0.760	9.907	
			1.290	11.232	
			1.906	12.290	
			2.787	13.525	
			3.88/	15 292	
			4.98/	15 720	
			7 02/	16 594	
			9 913	17,292	
			11,232	17.727	

[Strain,  $\varepsilon$ , %; Differential Stress,  $(\sigma_1-\sigma_3)$  MPa]

Dete	Author(a)	Voar			
Set	[Ref.]	leat	ε	$\sigma_1 - \sigma_3$	Remarks
	[[[[[]]]]]				
5	Heard, H.C.,	1972	0.405	7.254	$\dot{\varepsilon} = 1.2 \times 10^{-5} \text{ s}^{-1}$
	[21]		1.374	8.842	
			1.859	9.547	
			3.047	10.691	
			3.883	11.395	
			5.951	12.534	
			7.929	13.143	
			9,908	13.663	
			10.919	13.747	
6	Heard, H.C.,	1972	0.140	6.194	$\dot{\epsilon} = 1.2 \times 10^{-6} \text{ s}^{-1}$
-			0.624	6.722	0 110 1 10 5
	[2].]		1,900	7,335	
			3,923	7,943	
			5,945	8.375	
			7,924	8,895	
			9,946	9,150	
			11,397	9,142	
			11.337	J.142	
7	Heard, H.C.,	1972	0.093	3,893	$\dot{\epsilon} = 1.2 \times 10^{-7} \text{ s}^{-1}$
·	[21]		0.357	4,245	C 112 A 10 5
	[21]		1,281	4.683	
			1 897	4 945	
			2.952	5 117	
			3 875	5 289	
			5 985	5 5/3	
			7 963	5 532	
			9 985	5 521	
			11 3/8	5 514	
			11.940	5.514	
8	Heard, H.C.,	1972	0.138	4.424	$\dot{\varepsilon} = 1.2 \times 10^{-7} \text{ s}^{-1}$
	[21]		1.106	5.038	
			1.897	5.388	
			3.084	5.647	
			3.920	5.642	
			5.414	5.723	
			5.414	5.546	
			5.500	3.864	
			5.543	3.687	
			5.587	3.510	
			5.939	3.508	
			6.554	3.416	
9	Heard, H.C.,	1972	0.048	3.008	$\dot{\varepsilon} = 1.2 \times 10^{-8} \text{ s}^{-1}$
	[21]		0.136	3.273	
			1.191	3.268	

TABLE 3.15.DIFFERENTIAL STRESS-STRAIN RELATIONSHIP FOR POLYCRYSTALLINE<br/>HALITE AT 200 MPa, 473 K, AND  $\dot{\epsilon} = 1.8 \times 10^{-2}$  TO<br/> $1.2 \times 10^{-8} \text{ s}^{-1}$  (Continued)



FIGURE 3.16. Differential stress-strain curves for polycrystalline halite at 473 K.

# TABLE 3.16. DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE EXTENDED AT 200 MPa, 521 K, AND $\dot{\epsilon} = 1.8 \times 10^{-1}$ TO 1.2 x $10^{-7}$ s<sup>-1</sup>

[Strain,  $\varepsilon$ , %; Differential Stress,  $(\sigma_1 - \sigma_3)$  MPa]

Data Set	Author(s), Year [Ref.]	ε	$\sigma_1 - \sigma_3$	Remarks
1	Heard, H.C., 1972 [21]	1.631 1.733 2.643 3.702 5.714 7.623 9.630 10.282	15.457 15.761 17.633 19.300 21.571 23.285 24.745 25.147	$\dot{\varepsilon} = 1.8 \times 10^{-1} \text{ s}^{-1}$
2	Heard, H.C., 1972 [21]	0.063 0.126 0.239 0.353 0.716 1.025 1.329 1.785 2.693 3.748 5.705 7.661 9.716 11.470	2.433 4.969 7.503 9.988 12.572 14.244 15.053 16.116 17.632 18.539 19.949 21.104 22.057 22.859	$\dot{\epsilon} = 1.9 \times 10^{-2} s^{-1}$
3	Heard, H.C., 1972 [21]	0.063 0.076 0.189 0.303 0.563 0.766 1.220 1.824 3.783 5.788 7.743 9.747 11.149	$\begin{array}{c} 2.438\\ 4.979\\ 7.468\\ 10.008\\ 12.039\\ 12.546\\ 13.306\\ 14.116\\ 15.731\\ 16.838\\ 17.641\\ 18.443\\ 18.893\end{array}$	$\dot{\epsilon} = 1.5 \times 10^{-3} s^{-1}$
4	Heard, H.C., 1972 [21]	0.063 0.126 0.489 0.947 1.804 2.909	2.433 4.969 7.502 8.920 10.284 11.191	$\dot{\epsilon} = 1.2 \times 10^{-4} \text{ s}^{-1}$

Data Set	Author(s), [Ref.]	Year	ε	σ1-σ3	Remarks
4 (cont.)	Heard, H.C., [21]	1972	3.812 5.816 7.819 9.822	11.795 12.595 13.193 13.588	
5	Heard, H.C., [21]	1972	0.283 1.887 3.941 5.844 7.846 9.848	6.235 7.089 7.838 8.386 8.730 9.023	$\dot{\varepsilon} = 1.2 \times 10^{-5} \text{ s}^{-1}$
6	Heard, H.C., [21]	1972	10.998 0.321 1.876 3.929 5.930 7.931 9.931	9.169 4.004 4.858 5.506 5.748 5.890 5.890	$\dot{\varepsilon} = 1.2 \times 10^{-6} \text{ s}^{-1}$
7	Heard, H.C., [21]	1972	0.167 0.718 1.870 4.021 5.972 7.923 9.973	3.295 3.495 3.742 4.035 4.126 4.267 4.307	$\dot{\varepsilon} = 1.2 \times 10^{-7} \text{ s}^{-1}$
			11.023	4.250	

TABLE 3.16.	DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE
	EXTENDED AT 200 MPa, 521 K, AND $\dot{\varepsilon}$ = 1.8 x 10 <sup>-1</sup> TO
	$1.2 \times 10^{-7} s^{-1}$ (Continued)


FIGURE 3.17. Differential stress-strain curves for polycrystalline halite at 521 K.

# TABLE 3.17. DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE AT 200 MPa, 573 K AND $\dot{\epsilon}$ = 1.8 x 10<sup>-1</sup> TO 1.2 x 10<sup>-8</sup> s<sup>-1</sup>

Data Set	Author(s), [Ref.]	Year	ε	$\sigma_1 - \sigma_3$	Remarks
1	Heard, H.C.	1972	0.957	7,556	$\dot{\epsilon} = 1.6 \times 10^{-1} \text{ s}^{-1}$
~	[21]		1,304	8,933	- 100 11 10 13
	1211		2.043	10,933	
			2,870	12.533	
			4.043	14.044	
			5.174	15.066	
			6.087	15.600	
			8.043	16.711	
			9.957	17.466	
			11.913	18.044	
2	Heard, H.C.	1972	0.043	0.044	$\dot{\varepsilon} = 1.8 \times 10^{-2} \text{ s}^{-1}$
-	[21]	_,,_	0.217	2.533	
	·,		0.391	5.066	
			0.435	5.866	
			0.696	6.533	
			1.304	7.422	
			2.043	8.266	
			4.000	10.133	
			6.043	11.733	
			8.043	13.066	
			9.957	14.133	
			12.043	14.933	
3	Heard H.C.	1972	0.087	0.044	$\dot{\varepsilon} = 1.2 \times 10^{-3} \text{ s}^{-1}$
5	[01]	2012	0.217	2.488	
	[21]		0.304	3.466	
			0,565	4.533	
			1.043	5.777	
			2.043	7.022	
			3.609	8.088	
			4.000	8.444	
			6.000	9.644	
			8.043	10.533	
			9.957	11.066	
			11.304	11.155	
4	Heard. H.C	1972	0.348	2.311	$\dot{\varepsilon} = 1.5 \times 10^{-4}  \mathrm{s}^{-1}$
	[21]		2.043	4.266	
			4.000	5.644	
			6.000	6.444	
			8.000	6.577	
			9.957	7.288	
			11.043	7.377	

[Strain,  $\varepsilon$ , %; Differential Stress, ( $\sigma_1$ - $\sigma_3$ ) MPa]

Data	Author(c) Year			
Set	[Ref.]	ε	$\sigma_1 - \sigma_3$	Remarks
5	Heard, H.C., 1972	0.304	2.044	$\dot{\varepsilon} = 1.2 \times 10^{-5} \text{ s}^{-1}$
	[21]	0.739	2.577	
		1.000	2.711	
		2.043	3.155	
		4.000	3.866	
		6.000	4.355	
		8.000	4.755	
		9.957	4.888	
		11.087	4.844	
6	Heard HC 1972	0 391	1 911	$\dot{c} = 1.2 \times 10^{-6} c^{-1}$
U	[21]	0.652	2,177	C 1.2 A 10 B
	[21]	0.826	2,222	
		2.043	2.444	
		4,000	2,666	
		6,000	2.844	
		8,043	2,800	
		10,000	2.844	
		11.435	2.844	
7	No. 1072	0.20/	1 (00	• - 1 2 - 10 <sup>-7</sup> <sup>-1</sup>
/	Heard, H.C., 1972	0.304	1.000	$\xi = 1.2 \times 10^{\circ} \text{ s}^{\circ}$
	[21]	0.652	1.955	
		0.913	2.044	
		1.21/	2.044	
		2.043	2.000	
		4.000	2.133	
		0.000	2.044	
		0.043	2.000	
		11 / 25	2.044	
		11.435	2.044	
8	Heard, H.C., 1972	0.261	1.422	$\dot{\varepsilon} = 1.2 \times 10^{-8} \text{ s}^{-1}$
	[21]	1.174	1.555	
	1211	2.000	1.600	
		3.913	1.600	

TABLE 3.17.	DIFFERENTIAL	STRESS-STRAIN	CURVES FOR	POLYCRYSTALLINE	HALITE AT
	200 MPa, 573	K AND $\varepsilon = 1.8$	x 10 <sup>-1</sup> TO	$1.2 \times 10^{-8} \text{ s}^{-1}$	Continued)



FIGURE 3.18. Differential stress-strain curves for polycrystalline halite at 573 K.

TABLE 3.18.	DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE
	EXTENDED AT 200 MPa, 673 K, AND $\dot{\epsilon} = 1.9 \times 10^{-1}$ TO
	$1.2 \times 10^{-7} c^{-1}$

Data Set	Author(s), [Ref.]	Year	£	01-03	Remarks
1	Heard H C	1972	0 137	2 894	$\dot{E} = 1.9 \times 10^{-1} e^{-1}$
Ŧ	[21]	1)/2	1,175	3,549	0 - 1.9 X 10 B
	[21]		1,996	3.897	
			3,940	4,462	
			5,970	4,851	
			7,999	5.065	
			9,985	5.191	
			11.237	5.275	
2	Heard, H.C.,	1972	0.135	1.929	$\dot{\epsilon} = 1.4 \times 10^{-2} \text{ s}^{-1}$
	[21]		0.221	1.973	
			1.993	2.669	
			3.980	3.146	
			5.966	3.448	
			7.952	3.530	
			10.024	3.524	
			11.060	3.521	
3	Heard, H.C.,	1972	0.134	1.578	$\dot{\varepsilon} = 1.2 \times 10^{-3} \text{ s}^{-1}$
	[21]		0.350	1.753	
			0.523	1.884	
			1.991	2.012	
			3.977	2.138	
			5.963	2.176	
			8.035	2.170	
			10.020	2.208	
			11.316	2.248	
4	Heard, H.C.,	1972	0.263	1.402	$\dot{\varepsilon} = 1.2 \times 10^{-4} \text{ s}^{-1}$
	[21]		1.429	1.5/4	
			1.990	1.5/3	
			4.019	1.011	
			2.901 J.901	1 600	
			10 010	1 504	
			10.407	1.637	
5	Heard H C	1972	0 573	4 340	$\dot{c} = 1.2 \times 10^{-5} c^{-1}$
2	[21]	1)/2	0.791	4.997	2 - 1.2 X 10 S
	[21]		1.616	6.793	
			2,093	7,581	
			3.305	9.025	
			4.300	9.900	
			5.857	10.992	
			8.019	12.258	
			9.359	12.868	
			10.526	13.347	

[Strain,  $\varepsilon$ , %; Differential Stress, ( $\sigma_1 - \sigma_3$ ) MPa]

Data Set	Author(s), [Ref.]	Year	£	$\sigma_1 - \sigma_3$	Remarks
6	Heard, H.C.,	1972	0.093	2.499	$\dot{\varepsilon} = 1.2 \times 10^{-6} \text{ s}^{-1}$
	[21]		0.182	3.376	
			0.270	4.078	
			0.618	5.042	
			1.052	5.918	
			1.615	6.706	
			1.962	7.143	
			3.000	7.974	
			3.952	8.629	
			5.940	9.764	
			7.971	10.547	
			9.958	10.980	
			11.253	11.021	
7	Heard, H.C.,	1972	0.049	1.973	$\dot{\varepsilon} = 1.2 \times 10^{-7} \text{ s}^{-1}$
	[21]		0.095	3.069	
			0.572	4.165	
			1.957	5.433	
			3.989	6.392	
			5.933	6.957	
			8.006	7.433	
			10.035	7.647	
			11.633	7.774	

TABLE 3.18. DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE EXTENDED AT 200 MPa, 673 K, AND  $\dot{\epsilon} = 1.9 \times 10^{-1}$  TO 1.2 x  $10^{-7}$  s<sup>-1</sup> (Continued)



FIGURE 3.19. Differential stress-strain curves for polycrystalline halite at 673 K.

# TABLE 3.19. DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE EXTENDED AT 200 MPa. TEMPERATURE FROM 300 TO 673 K AND $\dot{\epsilon} = 1.2-1.5 \times 10^{-5} \text{ s}^{-1}$

Data Set	Author(s), [Ref.]	Year	ε	σ <sub>1</sub> -σ <sub>3</sub>	Remarks
1	Heard H C	1972	0 183	11 731	Temperature = $300 \text{ K}$
T	[21]	1772	0.189	15,130	iemperature 500 k.
	[21]		0.252	20.173	
			0.583	25,105	
			0.802	27.296	
			1 236	30 253	
			1 831	33 099	
			2 694	36 272	
			3 771	39 115	
			4 846	41 080	
			5 750	41.000	
			2.123	42.000	
			7 7/6	44.025	
			9 97/	40.114	
			0.670	40.421	
			9.079	47.401	
			10.209	41.035	
2	Heard, H.C.,	1972	0.170	4.932	Temperature = 373 K.
	[21]		0.341	10.085	
			0.725	15.125	
			1.266	17.862	
			1.859	19.941	
			2.934	21,906	
			3.848	23.215	
			5.833	25,063	
			7,818	26,482	
			9.802	27.663	
			11.464	28.308	
3	Heard, H.C.,	1972	0.495	6.904	Temperature = 473 K.
	[21]		1.248	8.542	
			1.947	9.524	
			3.021	10.831	
			3.932	11.482	
			5.863	12.563	
			7.846	13.205	
			9.830	13.737	
			10.848	13.949	
4	Heard, H.C.,	1972	0.332	5.808	Temperature = 521 K.
	[21]		0.333	6.028	
			0.440	6.246	
			1.996	7.111	
			3 926	7,973	

[Strain,  $\varepsilon$ , %; Differential Stress,  $(\sigma_1 - \sigma_3)$  MPa]

Data Set	Author(s), [Ref.]	Year	£	σ <sub>1</sub> -σ <sub>3</sub>	Remarks
4 (cont.)	Heard, H.C., [21]	1972	5.909 7.892 9.875 11.160	8.505 8.928 9.132 9.231	
5	Heard, H.C., [21]	1972	0.326 1.988 3.972 5.901 7.938 9.867 10.671	2.190 3.273 3.915 4.448 4.871 5.075 5.178	Temperature = 573 K
6	Heard, H.C., [21]	1972	0.325 1.934 3.970 5.899 7.989 9.918 11.471	2.080 2.616 3.148 3.462 3.664 3.759 3.637	Temperature = 673 K.

TABLE 3.19.	DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALIT	E
	EXTENDED AT 200 MPa. TEMPERATURE FROM 300 TO 673 K AND	
	$\dot{\varepsilon} = 1.2 - 1.5 \times 10^{-5} \text{ s}^{-1}$ (Continued)	



FIGURE 3.20. Differential stress-strain curves for polycrystalline halite at temperatures from 300 to 673 K.

### TABLE 3.20. DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE EXTENDED AT 200 MPa, 300 TO 673 K, AND $\hat{\varepsilon} = 1.2-1.5 \times 10^{-7} \text{s}^{-1}$

Data Author(s), Year ε Remarks 01-03 Set [Ref.] 1 Heard, H.C., 1972 0.225 4.987 Temperature = 300 K. 0.493 10.064 [21] 0.674 15.141 0.986 20.128 1.516 25.203 27.695 1.955 2.438 29.385 30.540 3.181 3.924 31.337 5.933 32.841 7.898 33.811 9.862 34.246 11.040 34.418 2 Heard, H.C., 1972 0.581 10.509 Temperature = 373 K. [2]] 0.756 11.399 1.456 12.909 1.981 13.530 3.947 15.658 5.956 17.073 18.131 7.965 18.744 9.929 18.826 11.195 3 Heard, H.C., 1972 0.311 4.007 Temperature = 473 K. 0.748 4.450 [21] 1.184 4.715 1.970 4.978 5.412 4.021 5.985 5.669 7.993 5.659 5.648 10.000 5.642. 11.178 4 Heard, H.C., 1972 0.310 3.294 Temperature = 521 K. [21] 0.397 3.472 3.820 1.969 4.020 4.076 6.027 4.333 7.991 4.233 9.998 4.312 10.958 4.306

[Strain,  $\varepsilon$ , %; Differential Stress,  $(\sigma_1 - \sigma_3)$  MPa]

Author(s), [Ref.]	Year	ε	σ1-σ3	Remarks
Heard, H.C., [21]	1972	0.220 0.483 1.966 4.017 6.025 7.989 9.996 11.130	1.780 1.957 2.127 2.205 2.195 2.362 2.352 2.435	Temperature = 573 K.
Heard, H.C., [21]	1972	0.307 2.009 4.017 6.024 7.988 9.951 10.693	1.423 1.682 1.671 1.749 1.739 1.817 1.813	Temperature = 673 K.
	Author(s), [Ref.] Heard, H.C., [21] Heard, H.C., [21]	Author(s), Year [Ref.] Heard, H.C., 1972 [21] Heard, H.C., 1972 [21]	Author(s), Year [Ref.] $\varepsilon$ Heard, H.C., 19720.220[21]0.4831.9664.0176.0257.9899.99611.130Heard, H.C., 19720.307[21]2.0094.0176.0247.9889.95110.693	Author(s), Year [Ref.] $\varepsilon$ $\sigma_1 - \sigma_3$ Heard, H.C., 19720.2201.780[21]0.4831.9571.9662.1274.0172.2056.0252.1957.9892.3629.9962.35211.1302.435Heard, H.C., 19720.3071.423[21]2.0091.6824.0171.6716.0241.7497.9881.7399.9511.81710.6931.813

TABLE 3.20.	DIFFERENTIAL STRESS-STRAIN CURVES FOR POLYCRYSTALLINE HALITE
	EXTENDED AT 200 MPa, 300 TO 673 K, AND $\dot{\epsilon} = 1.2 - 1.5 \times 10^{-7} \text{ s}^{-1}$
	(Continued)



FIGURE 3.21. Differential stress-strain curves for polycrystalline halite at temperatures from 300 to 673 K.

Data Set	Author(s), Year [Ref.]	σ1	ε	Remarks
1	Gera, F., 1972 [5]	0.15	0.00	Lower Stassfurt halite; unannealed; sample
		1.29	0.02	taken from a mine.
		1.9	0.02	
		3.42	0.04	
		3.80	0.04	
		4.48	0.04	
		5.32	0.05	
		5.93	0.06	
		0.92 7.60	0.07	
		8.36	0.09	
		8.97	0.10	
		9.65	0.10	
		10.57	0.11	
		11.63	0.13	
		12.85	0.14	
		14.14	0.10	
		14.75	0.19	
		15.28	0.22	
		15.97	0.26	
		16.42	0.29	
		17.26	0.33	
		17.57	0.39	
		17.95	0.41	
		18.26	0.45	
		18.71	0.48	
		19.02	0.52	
		19.32	0.552	
		19.71	0.596	
2	Gera, F., 1972 [5]	0.00	0.00	After annealing; sample similar to above.
		0.61	0.02	
		1.45	0.05	
		2.21	0.08	
		3.35	0.13	
		3.88	0.15	
		4.57	0.19	
		5.18	0.21	
		5.71	0.25	
		6.70	0.29	
		7.16	0.36	
		7.47	0.39	
		7.85	0.43	
		8.15	0.47	
		8.46	0.49	
		8.69	0.52	
		9.22	0.58	
		9.38	0.61	
		9.68	0.63	
		9.91	0.67	
		10.22	0.69	
		10.37	0.72	
		10.00	0.76	
		10.15		

TABLE 3.21. EFFECT OF ANNEALING AT 873 K ON STRESS-STRAIN RELATIONSHIP OF ROCK SALT [Stress,  $\sigma_1$ , MPa; Strain,  $\epsilon$ , %]



FIGURE 3.22. Effect of annealing on a stress-strain relationship (curve numbers correspond to data set numbers in matching table).

#### 3.4.2. Creep Data

Creep can be defined as slow deformation over a long period of time at essentially constant load. At room temperature and low stresses, rock salt will exhibit considerably less creep deformation than at high temperatures and pressures. In general, salt shows marked plastic character, and even at relatively low temperatures it will display a recognizable component of creep. Creep data are generally presented as some type of time relationship.

Thompson [25] investigated creep as a function of differential stress on four rock salt specimens from Hockly, Texas. The tests were conducted at 306 K and a confining pressure of 11.37 MPa. Various load stresses and strain rates were adopted. These data are tabulated in table 3.22 and displayed in figure 3.23. Typical curves showing primary and steady-state creep were presented by Burke [19]. This information was obtained using a dead load compression unit and artificial salt samples and is illustrated in figure 3.24 and table 3.23. Tensile tests using various  $\sigma_1$  and  $\sigma_3$  values were carried out by Nair and Deere [23]. Data obtained from these triaxial extension tests are displayed in table 3.24 and figure 3.25.

Two variations on basic creep relationships are given by Odé [34] in which he shows nonuniform creep of NaCl at different load stresses and the behavior of halite single crystals compressed at different constant loads. Data related to these two aspects are given in table 3.25 and figure 3.26 and table 3.26 and figure 3.27, respectively.

The effect of confining pressure and temperature on the creep of rock salt has been investigated by several researchers. LeComte [22] investigated the effects of temperature to 573 K and confining pressure to 100 MPa. The results of this work are presented in table 3.27

#### TABLE 3.22. CREEP CURVES FOR HALITE

[Time, t, min; Strain,  $\varepsilon$ , %]

Data Set	Author(s), Year [Ref.]	t	ε	Remarks
1	Thompson, E.G., 1965	315,562	0.226	$\sigma = 16.54 \text{ MPa}$
_	[25]	906.262	0.357	$\dot{\epsilon} = 90 \times 10^{-8} \text{ min}^{-1}$ .
	1-0,	1268,959	0.411	Temperature = $306$ K
		1788.877	0.473	and confining pres-
		2466.337	0.540	sure = $11.37$ MPa.
		2960.531	0.596	
		3324.826	0.637	
		3952.755	0.677	
		4317.368	0.715	
		4761.392	0.750	
		5362.318	0.796	
		5831.427	0.842	
		6224.642	0.861	
		6746.797	0.904	
		7346.444	0.961	
		7764.744	0.990	
		8208.768	1.026	
		8702.323	1.087	
2	Thompson, E.G., 1965	585.268	0.176	σ = 13.78 MPa
	[25]	1395.184	0.238	$\dot{\epsilon} = 4.7 \times 10^{-8} \text{ min}^{-1}$
		1811.885	0.281	Temperature = $306 \text{ K}$
		2783.497	0.314	and confining pres-
		3517.198	0.352	sure = 11.37 MPa.
		4305.226	0.377	
		5642.729	0.437	
		6587.657	0.4/3	
		8138.625	0.512	
		9032.425	0.535	
		10267.990	0.565	
3	Thompson, E.G., 1965	495.792	0.043	$\sigma = 9.65 \text{ MPa}$
	[25]	1389.592	0.065	$\dot{\epsilon} = 53 \times 10^{-9} \text{ min}^{-1}$ .
		2153.491	0.071	Temperature = 306 K
		2864.664	0.078	and confining pres-
		3575.518	0.086	sure = 11.37 MPa.
		4287.649	0.085	
		5763.362	0.092	
		6553.625	0.098	
		8609.012	0.108	
		11586.479	0.125	
		13114.600	0.135	
		14431.812	0.145	



FIGURE 3.23. Creep curves for halite at various load stresses and strain rates.

### TABLE 3.23. TYPICAL CREEP CURVES FOR POLYCRYSTALLINE NaCl SHOWING PRIMARY AND STEADY STATE CREEP AT TEMPERATURE = 721 K AND GRAINIZE $\sim$ 370 $\mu m$

Data	Author(s),	Year		-	n- 1
Set	[Ref.]		t	E	Remarks
1	Burke P M	1968	3 120	5 1 2 7	$\sigma = 4.34 \text{ MP}_{2}$
T	[19]	1908	7 430	6 272	$c = 2.3 \times 10^{-5} c^{-1}$
	[ 1 ]		11 653	6 994	E - 2.J X 10 3
			15 875	7 716	
			17 319	8 120	
			21 476	8 540	
			24.976	8 052	
			27.077	0.955	
			20 885	9.303	
			22.005	10 155	
			35 456	10.105	
			38 957	11 014	
			164.00	11.014	
2	Burke, P.M.,	1968	1.582	1.068	$\sigma = 3.03 \text{ MPa}$
	[19]		3.070	1.688	$\dot{\epsilon} = 2.6 \times 10^{-6} \text{ s}^{-1}$
			7.227	2.100	
			12.084	2.614	
			17.612	3.094	
			26.560	3.710	
			35.465	4.119	
			45.726	4.527	
			69.618	5.238	
			96.201	5.844	
			113.923	6.249	
			144.569	6.818	
			184.702	7.348	
			224.858	7.981	
			248.706	8.485	
			319.470	9.516	
			328.310	9.614	
3	Burke. P.M.	1968	5.455	0.135	$\sigma = 2.17 \text{ MPa}$
-	[19]		19.706	0.162	$\dot{\epsilon} = 6.8 \times 10^{-7} \text{ s}^{-1}$
			41.476	0.460	
			76.125	0.717	
			109.396	0.871	
			129.094	0.999	
			165.078	1.151	
			179.329	1.178	
			210.572	1.368	
			249.269	1.519	
			306.308	1.798	
			351.124	2.015	

[Time, t, min; Strain, ε, %]



FIGURE 3.24. Typical creep curves for polycrystalline NaCl.

Data	Author(s), Year	t	ε	Remarks
1	Nair, K. and Deere,	0.250E+00	0.180E+00	$\sigma_{3} = 20.7 \text{ MPa}$
	D.U., 1970 [23]	0.502E+00	0.215E+00	$\sigma_{1} = 3.4 \text{ MPa.}$
		0.125E+01	0.272E+00	•
		0.275E+01	0.344E+00	
		0.464E+01	0.455E+00	
		0.220E+02	0.698E+00	
		0.482E+02	0.845E+00	
		0.114E+03	0.113E+01	
		0.369E+03	0.171E+01	
		0.479E+03	0.199E+01	
		0.991E+03	0.278E+01	
2	Nair, K. and Deere,	0.509E+00	0.256E+00	σ, = 17.9 MPa
	D.U., 1970 [23]	0.994E+00	0.297E+00	$\sigma_{1}^{3} = 0.7 \text{ MPa.}$
	·	0.212E+01	0.393E+00	1
		0.204E+02	0.845E+00	
		0.489E+02	0.115E+01	
		0.982E+02	0.154E+01	
		0.292E+03	0.244E+01	
		0.719E+03	0.362E+01	
3	Nair, K. and Deere,	0.192E+00	0.248E+00	$\sigma_a = 23.6 \text{ MPa}$
	D.U., 1970 [23]	0.334E+00	0.292E+00	$\sigma_1 = 2.1 \text{ MPa.}$
		0.447E+00	0.310E+00	1
		0.135E+01	0.422E+00	
		0.275E+01	0.559E+00	
		0.620E+01	0.697E+00	
		0.126E+02	0.908E+00	
		0.448E+02	0.143E+01	
		0.996E+02	0.223E+01	
		0.189E+03	0.357E+01	
4	Nair, K. and Deere,	0.985E-01	0.224E+00	σ <sub>3</sub> = 24.8 MPa
	D.U., 1970 [23]	0.993E+00	0.558E+00	$\sigma_1 = 3.4 \text{ MPa.}$
		0.183E+01	0.676E+00	
		0.931E+01	0.133E+01	
		0.198E+02	0.195E+01	
		0.122E+03	0.478E+01	
5	Nair, K. and Deere,	0.999E-01	0.238E+00	$\sigma_3 = 22 \text{ MPa}$
	D.U., 1970 [23]	0.509E+00	0.461E+00	$\sigma_1 = 0.7 \text{ MPa.}$
		0.101E+01	0.685E+00	
		0.197E+01	0.893E+00	
		0.620E+01	0.145E+01	
		0.207E+02	0.254E+01	

### TABLE 3.24. CREEP STRAIN-TIME CURVES FOR SALT (TENSILE TEST) [Time, t, hr; Strain, ε, %]

Data	Author(s), Year	t	ε	Remarks
6	Nair, K. and Deere,	0.164E+00	0.397E+00	$\sigma_3 = 25.5 \text{ MPa}$
	D.U., 1970 [23]	0.198E+00 0.253E+00 0.107E+01 0.205E+01	0.434E+00 0.488E+00 0.892E+00 0.111E+01	σ <sub>1</sub> = 2.1 MPa.
		0.498E+01 0.144E+02 0.219E+02 0.269E+02 0.495E+02	0.161E+01 0.250E+01 0.294E+01 0.312E+01 0.470E+01	
7	Nair, K. and Deere, D.U., 1970 [23]	0.301E+00 0.680E+00 0.165E+01 0.498E+01 0.865E+01 0.198E+02	0.541E+00 0.748E+00 0.113E+01 0.186E+01 0.243E+01 0.340E+01	σ <sub>3</sub> = 26.5 MPa σ <sub>1</sub> = 0.7 MPa.
8	Nair, K. and Deere, D.U., 1970 [23]	0.131E+00 0.200E+00 0.513E+00 0.100E+01 0.818E+01 0.670E+02 0.387E+03	0.394E+00 0.437E+00 0.612E+00 0.730E+00 0.144E+01 0.295E+01 0.720E+01	$\sigma_3 = 22 \text{ MPa}$ $\sigma_1 = 1.4 \text{ MPa}$ .
9	Nair, K. and Deere, D.U., 1970 [23]	0.121E+01 0.200E+01 0.499E+01 0.494E+02 0.196E+03 0.376E+03	0.129E+01 0.145E+01 0.186E+01 0.346E+01 0.492E+01 0.596E+01	$\sigma_{3} = 24.1 \text{ MPa}$ $\sigma_{1} = 3.4 \text{ MPa}.$
10	Nair, K. and Deere, D.U., 1970 [23]	0.101E+01 0.308E+00 0.512E+00 0.103E+01 0.191E+01 0.309E+01 0.505E+01	0.726E+00 0.121E+01 0.156E+01 0.203E+01 0.268E+01 0.333E+01 0.440E+01	σ <sub>3</sub> = 31.7 MPa σ <sub>1</sub> = 3.4 MPa.
11	Nair, K. and Deere. D.U., 1970 [23]	0.101E+00 0.148E+01 0.136E+02 0.193E+02	0.399E+00 0.587E+00 0.115E+01 0.134E+01	σ <sub>3</sub> = 17.2 MPa σ <sub>1</sub> = 3.4 MPa.
12	Nair, K. and Deere, D.U., 1970 [23]	0.625E+01 0.980E+01 0.218E+02 0.520E+02 0.141E+03 0.545E+03	0.120E+00 0.135E+00 0.155E+00 0.187E+00 0.221E+00 0.319E+00	$\sigma_1 = 17.2 \text{ MPa}$ $\sigma_3 = 6.9 \text{ MPa}.$

TABLE 3.24. CREEP STRAIN-TIME CURVES FOR SALT (TENSILE TEST) (Continued)



FIGURE 3.25. Tensile creep-strain curves for salt (curve numbers correspond to data set numbers in matching table).

### TABLE 3.25. NONUNIFORM CREEP OF NaCl WITH VARYING LOADS

[Time, t, min; Strain,  $\varepsilon$ , %]

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Data Set	Author(s), Year [Ref.]	t	ε	Remarks
1	Odo 11 1068 [2/1	0 2445400	0.7355-02	$\sigma = hh 5 MDa 1act$
T	000, H., 1900 [24]	0.244E+00	0.733E-02	0 - 44.5 Mra 10ad
		0.430E+00	0.325E-01	SLIESS.
		0.140F+01	0.578E-01	
		0.199F+01	0.570L=01	
		0.252E+01	0.687 = 01	
		0.290E+01	0.698 - 01	
		0.342F+01	0.708F-01	
		0.393E+01	0.724E-01	
		0.432E+01	0.745E-01	
		0.474E+01	0.766E-01	
		0.545E+01	0.864F-01	
		0.583E+01	0.958E-01	
		0.625E+01	0.101E+00	
		0.702E+01	0.104E+00	
		0.736E+01	0.107E+00	
		0.808E+01	0.109E+00	
		0.908E+01	0.111E+00	
		0.997E+01	0.112E+00	
		0.197E+02	0.116E+00	
		0.249E+02	0.117E+00	
		0.408E+02	0.120E+00	
		0.503E+02	0.121E+00	
		0.622E+02	0.123E+00	
		0.120E+03	0.125E+00	
		0.232E+03	0.126E+00	
2	Ode, H., 1968 [24]	0.244E+00	0.166E-02	$\sigma$ = 2.45 MPa load
		0.331E+00	0.946E-02	stress.
		0.492E+00	0.178E-01	
		0.651E+00	0.240E-01	
		0.786E+00	0.267E-01	
		0.993E+00	0.303E-01	
		0.144E+01	0.381E-01	
		0.191E+01	0.438E-01	
		0.285E+01	0.465E-01	
		0.395E+01	0.491E-01	
		0.575E+01	0.517E-01	
		0.964E+01	0.539E-01	
		0.158E+02	0.570E-01	
		0.247E+02	0.597E-01	
		0.454E+02	0.629E-01	
		0.601E+02	0.650E-01	
		0.891E+02	0.930E-01	•
		0.890E+02	0.966E-01	
		0.976E+02	0.101E+00	
		0.112E+03	0.106E+00	
		0.118E+03	0.108E+00	

Data Set	Author(s), Y [Ref.]	ear	t	ε	Remarks
2 (cont.)	Ode, H., 1968	[24]	0.145E+03 0.175E+03 0.216E+03 0.293E+03 0.407E+03	0.112E+00 0.115E+00 0.117E+00 0.121E+00 0.124E+00	
3	Ode, H., 1968	[24]	0.493E+00 0.653E+00 0.826E+00 0.996E+00 0.132E+01 0.148E+01 0.201E+01 0.232E+01 0.266E+01 0.329E+01 0.361E+01 0.397E+01 0.605E+01 0.696E+01 0.696E+01 0.801E+01 0.801E+01 0.101E+02 0.117E+02 0.141E+02 0.209E+02 0.241E+02 0.327E+02 0.499E+02 0.29E+02 0.134E+03 0.181E+03 0.246E+03 0.509E+03	0.795E-02 0.121E-01 0.142E-01 0.163E-01 0.200E-01 0.221E-01 0.236E-01 0.252E-01 0.273E-01 0.304E-01 0.315E-01 0.341E-01 0.367E-01 0.388E-01 0.398E-01 0.430E-01 0.445E-01 0.466E-01 0.482E-01 0.555E-01 0.571E-01 0.592E-01 0.618E-01 0.686E-01 0.702E-01 0.719E-01 0.719E-01	σ = 2.94 MPa load stress.
4	Ode, H., 1968	[24]	0.999E+00 0.123E+01 0.142E+01 0.171E+01 0.197E+01 0.243E+01 0.308E+01 0.389E+01 0.480E+01 0.593E+01	0.389E-02 0.702E-02 0.911E-02 0.112E-01 0.123E-01 0.138E-01 0.170E-01 0.185E-01 0.201E-01 0.217E-01	$\sigma$ = 3.43 MPa load stress.

.

Data Set	Author(s), Y [Ref.]	ear	t	3	Remarks
4 (cont.)	Ode, H., 1968	[24]	0.805E+01 0.994E+01 0.138E+02 0.159E+02 0.201E+02 0.242E+02 0.344E+02 0.524E+02 0.711E+02 0.899E+02 0.101E+03 0.186E+03 0.246E+03 0.297E+03 0.487E+03	$\begin{array}{c} 0.228E-01\\ 0.254E-01\\ 0.301E-01\\ 0.322E-01\\ 0.363E-01\\ 0.390E-01\\ 0.447E-01\\ 0.484E-01\\ 0.510E-01\\ 0.552E-01\\ 0.552E-01\\ 0.625E-01\\ 0.636E-01\\ 0.636E-01\\ 0.642E-01\\ \end{array}$	



FIGURE 3.26. Nonuniform creep of NaCl.

### TABLE 3.26. CREEP CURVES FOR HALITE SINGLE CRYSTALS AT DIFFERENT CONSTANT LOADS

[Time, t, min; Strain,  $\varepsilon$ , %]

Data Set	Author(s), Year [Ref.]	t	ε	Remarks
1	Ode, H., 1968 [24]	83.952 146.852 204.529 403.971 603.509 808.323 1002.679	0.498 0.997 1.416 2.492 3.385 4.251 4.987	σ = 25 MPa.
2	Ode, H., 1968 [24]	120.767 204.787 404.433 604.161 803.929 1003.725 1203.561 1403.384 1597.971 1797.834 2002.947	0.551 0.919 1.602 2.128 2.576 2.971 3.288 3.631 3.921 4.185 4.476	σ = 23 MPa.
3	Ode, H., 1968 [24]	36.788 73.385 110.105 204.678 404.433 604.242 804.092 998.693 1203.847 1398.474 1598.378 1793.020 1998.200	0.105 0.577 0.813 1.128 1.602 1.971 2.262 2.526 2.738 2.950 3.136 3.321 3.481	σ = 17 MPa.
4	Ode, H., 1968 [24]	78.838 199.796 399.686 604.854 804.758 1004.703 1199.371 1399.316 1604.524 1799.206 1999.151	0.210 0.395 0.607 0.793 0.979 1.086 1.220 1.327 1.434 1.541 1.649	σ = 22 MPa.

Data Set	Author(s), Year [Ref.]	t	ε	Remarks
5	Ode. H., 1968 [24]	10.445	0.157	$\sigma = 70 \text{ MPa}$ .
-	,,	89.297	0.341	
		126.098	0.420	
		205.032	0.448	
		404.963	0.581	
		604.935	0.636	
		810.143	0.743	
		1004.866	0.772	
		1204.824	0.853	
		1399.547	0.882	
		1599.533	0.911	
		1799.519	0.939	
		1999.518	0.942	
6	Ode, H., 1968 [24]	10.526	0.000	$\sigma$ = 10.5 MPa.
		205.235	0.055	
		405.207	0.110	
		605.180	0.165	
		805.179	0.167	
		1005.138	0.249	
		1205.110	0.303	
		1405.082	0.358	
		1599.791	0.413	
		1794.514	0.442	
		1999.749	0.497	

#### TABLE 3.26. CREEP CURVES FOR HALITE SINGLE CRYSTALS AT DIFFERENT CONSTANT LOADS (Continued)



TIME , t , minutes

FIGURE 3.27. Creep curves for halite single crystals.

and figure 3.28. Similar work on the effects of confining pressure only was conducted by Thompson [25]. Differential stress was kept constant and a range of confining pressures was used. The evidence is that the effect of confining pressure is minimal. Data related to Thompson's work are supplied in table 3.28 and figure 3.29. Baar [17] gives field data indicating the acceleration of creep caused by heating of a salt mine pillar to peak temperatures of about 423 K. The data presented in table 3.29 and figure 3.30 yield four data sets, each set related to connected rooms in the salt mine in which the experiment was performed. From the information presented, it can be seen that creep is a thermally activated process since if it were not, the creep rate at any temperature would depend on stress difference only. LeComte also investigated the effect of axial stress on creep and the combined effects of grain size and axial stress on creep of rock salt. These results can be found in table 3.30 and figure 3.31, and table 3.31 and figure 3.32, respectively.

Steady-state creep rate as some function of stress has been studied by Burke and is also reported by Odé. Burke [29] presents a relationship between steady-state creep rate and stress for coarse-grained salt (1000-3000  $\mu$ m). These values are given in table 3.32 and figure 3.33. The same relationship for polycrystalline NaCl and single crystal NaCl was also investigated by Burke at 1013 K (see table 3.33 and figure 3.34). Steady-state creep rate of NaCl at several stresses as a function of temperature are reported by Odé [34] and is illustrated in figure 3.35 and table 3.34.

Figure 3.36 shows the time-strain data at various confining pressures and temperatures and table 3.35 tabulates the corresponding values. These values were obtained by Dreyer [12] in 1972 from creep tests on artificial rock salt samples. The lower three curves indicate that confining pressure has only a small influence on time dependent strain at room temperature. The upper curves show that the effect of confining pressure is greater at higher temperatures. In general, temperature has a marked effect on the deformational behavior of rock salt.

Dreyer [12] has also studied the creep behavior of untempered and tempered rock salt as a function of time and the relevant data are presented in figure 3.37 and table 3.36. Although these two rock salt samples have a slightly different composition (see measurement methods), it is considered that they are representative of the trend in creep behavior of tempered and untempered rock salt.

Generally, tempered samples show a much more prolonged "creep life" than do untempered samples. This is because untempered samples reach this maximum creep strain in a short time whereas tempered samples take longer to reach their maximum. In addition, tempered rock salt exhibits a much higher maximum creep strain (5 to 6 times greater). It is believed that the behavior of the tempered salt is due to recrystallization during tempering.

#### 3.5. Hardness

The hardness of rock salt depends on atmospheric humidity, previous plastic deformation, impurities in the crystals, and quench temperatures. Large discrepancies in hardness values of NaCl are found at small loads. The various factors which influence the hardness number at small loads include microrelief of surface, roughness of indentor, elastic recovery in indent, vibration, loading rate, etc.

Strelkov and Shpunt [15] have shown that the published data on hardness may be represented by curves 1-3 of figure 3.38 which may be obtained on a single specimen of NaCl by varying the atmospheric humidity B and the previous plastic deformation  $\epsilon$ . Curve 1 is for an unstressed ( $\epsilon \sim 0$ ) specimen in dry air (B| $\leq$  30%) while curve 3 is for the same specimen in moist air. Curve 3 is for a deformed specimen ( $\epsilon \geq 0.3-0.4\%$ ) in dry atmosphere.

The values of hardness at low loads indicated by these curves and tabulated in table 3.37 have not been corrected for the factors mentioned above. The absolute values of hardness can be obtained only if all factors have been considered, which is difficult to accomplish. However, as the above curves represent an average of a large data set, they can be considered to represent the recommended values of microhardness.

According to Strelkov and Shpunt [15] 1=3transition involves a delay (relative to the change in B) of 15-20 minutes. Curve 2 differs from 1 for  $\epsilon \ge 0.3-0.4\%$ . The 2=3 transition is analogous to 1=3. A.  $2 \rightarrow 1$  transition occurs on annealing even highly deformed materials ( $\epsilon \ge 2-3\%$ ). The maximum humidity at which NaCl can be tested for microhardness is 75%; for values higher than this water is deposited on the crystals.

For values of load p > 20 g and indentation depth  $h > 6-7\mu$ , the microhardness is steady and independent of load, humidity, and previous plastic deformation. The values of steady microhardness have been found to fall in the range of 19-23 kg/mm<sup>2</sup> due to differences in impurity content.

Kishsh and Sharkezi [14] have studied the microhardness of NaCl crystals containing cation and anion impurities in relation to temperature and rate of quenching. Their data are presented in figure 3.39 with the corresponding values in table 3.38. The figure shows

#### TABLE 3.27. EFFECT OF TEMPERATURE AND CONFINING PRESSURE ON THE CREEP OF ROCK SALT

[Time, t, hr; Strain, ε, %]

Data Set	Author(s), [Ref.]	Year		t	ε	Remarks
1	LeComte, P.,	1965	[22]	2.328 6.003 9.693	1.199 1.719 2.141	Confining pressure = 100 MPa; Temperature = 471 K:
				19.558 24.520	3.085 3.346	Axial stress = 6.9 MPa.
				33.191 43.116	3.900	
				52.426	4.879	
				67.948 79.749	5.597 6.120	
				90.924 94.650	6.643 6.806	
2	LeComte, P.,	1965	[22]	1.759 5.416	0.810 1.460	Confining pressure = 0.1 MPa;
				11.540 21.428	2.336 3.118	Temperature = 377 K; Axial stress = 6.9
				32.589	3.737	MPa.
				49.352	3.933 4.521	
				59.296 68.629	4.914 5.209	
				83.564 96.637	5.668	
3	LeComte, P.,	1965	[22]	0.485	0.972	Confining pressure =
				4.856 14.846	1.006	100 MPa; Temperature = $377$ K:
				27.318	1.274	Axial stress = 6.9
				36.679	1.375	MPa.
				72.256	1.712	
				84.733 98.459	2.046	
				120.944 134.060	2.152 2.222	
4	LeComte, P.,	1965	[22]	10.592	0.231	Confining pressure =
				35.578	0.338	0.1 MPa; Temperature = $202$ K.
				72.433	0.410	Axial stress = 6.9
				86.178	0.519	MPa.
				108.677	0.523	
				131.167	0.601	
				153.042	0.610 0.650	

Data Set	Author(s), [Ref.]	Year	t	E	Remarks
5	LeComte, P.,	1965	[22] 8.097 15.592 23.712 49.327 69.327 99.321 142.440 169.314	0.197 0.233 0.268 0.343 0.351 0.395 0.444 0.454	Confining pressure = 100 MPa; Temperature = 302 K; Axial stress = 6.9 MPa.
6	LeComte, P.,	1965	[22] 4.338 30.578 58.697 78.692 94.321 119.316 126.811 151.185 179.935	0.261 0.336 0.379 0.419 0.393 0.435 0.470 0.479 0.490	Confining pressure = 20 MPa; Temperature = 302 K; Axial stress = 6.9 MPa.

#### TABLE 3.27. EFFECT OF TEMPERATURE AND CONFINING PRESSURE ON THE CREEP OF ROCK SALT (Continued)



FIGURE 3.28. Effect of temperature and confining pressure on creep of rock salt.

### TABLE 3.28. EFFECT OF CONFINING PRESSURE ON THE STEADY STATE CREEP RATE OF HALITE

[Time, t, min; Strain, ε, %]

Data Set	Author(s), Year [Ref.]	t	ε	Remarks
1	Thompson, E.G., 1965 [25]	442.493 784.022 1441.997 1942.167 2311.024 2916.783 3443.446 4391.568 5103.045 5708.932 6420.281 7105.457 7922.395 8581.334 9872.526 10821.354 11348.339 12191.706 12956.042 13483.091 14379.317	0.236 0.287 0.335 0.367 0.378 0.405 0.431 0.474 0.490 0.512 0.533 0.547 0.563 0.571 0.600 0.614 0.627 0.641 0.652 0.662 0.671	Confining pressure = 13.78 MPa.
2	Thompson, E.G., 1965 [25]	417.092 785.178 1442.832 2074.700 2785.406 3575.529 4260.448 4918.874 5656.651 6472.562 7210.276 8554.391 9318.791 9924.871	0.196 0.239 0.300 0.338 0.386 0.421 0.445 0.445 0.474 0.493 0.552 0.573 0.595 0.603 0.616	Confining pressure = 10.33 MPa.
3	Thompson, E.G., 1965 [25]	361.792 677.533 1125.100 1783.654 2152.575 2705.925 3311.876 4049.655 4734.895 5393.577 6078.753 6605.866 7528.137 8924.918	0.303 0.330 0.356 0.380 0.388 0.402 0.421 0.421 0.439 0.450 0.469 0.482 0.491 0.512 0.536	Confining pressure = 3.44 MPa.

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Data Set	Author(s), Year [Ref.]	t	£	Remarks
4	Thompson, E.G., 1965 [25]	466.868 1124.008 1544.889 1965.834 2465.619 3361.010 3887.481 4941.192 5441.554 6126.602 7074.916 8287.013 8945.695 9683.666 10395.079 11106.619 12529.509 13056.494	0.319 0.401 0.441 0.479 0.527 0.570 0.604 0.642 0.666 0.685 0.719 0.749 0.749 0.768 0.779 0.797 0.811 0.846 0.859	Confining pressure = O MPa.

TABLE 3.28. EFFECT OF CONFINING PRESSURE ON THE STEADY STATE CREEP RATE OF HALITE (Continued)



FIGURE 3.29. Effect of confining pressure on steady state flow of halite.

### TABLE 3.29. ACCELERATED CREEP CAUSED BY HEATING A SALT MINE PILLAR TO PEAK TEMPERATURE OF $\pm 423$ K

[Time, t, days; Vertical Deformation,  $\Delta L$ , cms]

Data Set	Author(s), Year [Ref.]	t	Δl
	Page C & 1077 [17	1 472 105	0.001
T	Baar, C.A., 19// [1/	J 472.10J	0.091
		407.272	0.240
		506 150	0.308
		511 190	0.50
		517.493	0.449
		523.789	0.490
		531,351	0.523
		537.654	0.548
		545.216	0.581
		554.044	0.607
		561.613	0.624
		571.707	0.640
		583.051	0.690
		593.141	0.716
		603.232	0.741
		614.585	0.764
		624.680	0.782
		639.824	0.800
		652.434	0.840
		681.464	0.866
		701.652	0.899
		718.056	0.924
		730.668	0.957
		744.550	0.975
		759.699	0.983
		774.847	0.993
		787.459	1.026
		798.816	1.043
		808.903	1.0//
		813.947	1.092
		823.983	1.249
		826.481	1.318
		834.013	1.424
		844.087	1.491
		049.11U 856 652	1.559
		046 017	1.040
		871 760	1 726
		884 365	1 800
		891 923	1 8/1
		899 485	1.874
		923.438	1,966
		930,993	2,016
		941.087	2.032
		952,430	2.082

Data	Auth	nor(s), Year		t	Δτ
Set		[Ref.]			
1	Baar	C A 1977	[17]	968 831	2 115
(cont)	Daar,	U.A., 1777	[1/]	981 447	2.113
(conc.)				990 272	2.174
				990.272	2.174
				1005 /00	2 200
				1012 082	2.209
				1012.902	2.211
				1023.070	2.232
				1030.210	2.215
2	Baar,	C.A., 1977	[17]	463.384	0.000
				472.147	0.182
				485.941	0.414
				499.758	0.589
				507.303	0.662
				511.091	0.665
				516.108	0.746
				523.667	0.789
				529,963	0.830
				537.518	0.881
				545.073	0.929
				553.898	0.962
				562.723	0,998
				571.544	1.038
				582,891	1.079
				594 244	1,104
				606 853	1.148
				640 903	1 247
				653 519	1 272
				667 394	1 305
				680 010	1 331
				702 717	1 381
				71/ 071	1 /07
				731 734	1 4407
				744 350	1 /65
				756 962	1 /08
				773 376	1 /98
				787 255	1 524
				799 871	1 5/9
				808 680	1 600
				811 197	1.666
				823 711	1 915
				827 440	<b>7</b> 030
				836 737	2.039
				020.222	2.1/1
				040.202	2.290
				040.739	2.413
				866 282	2.400
				000.302	2.04/

# TABLE 3.29. ACCELERATED CREEP CAUSED BY HEATING A SALT MINE PILLAR TO PEAK TEMPERATURE OF $\pm 423$ K (Continued)

TABLE 3.29.	ACCELERATED CREEP CAUSE	) BY	HEATING A SALT	MINE PILLAR	ГО
	PEAK TEMPERATURE OF ±42	3 K	(Continued)		

Data Set	Author(s), Year [Ref.]	t	∆l
3	Baar, C.A., 1977 [17	] 604.794	0.010
		611.097	0.035
		624.972	0.068
		642.635	0.101
		655.241	0.152
		666.591	0.185
		681.736	0.203
		703.183	0.243
		718.325	0.269
		732.200	0.302
		747.341	0.327
		758.695	0.353
		776.364	0.370
		785.196	0.386
		802.859	0.421
		809.152	0.469
		812.916	0.528
		822.938	0.718
		829.214	0.810
		836.749	0.911
		843.025	1.003
		850.573	1.069
		856.859	1.135
		865.667	1.209
		873.209	1.292
		883.289	1.343
		894.625	1.409
		902.177	1.468
		912.255	1.526
		926.120	1.585
		942.500	1.668
		955.105	1.717
		967.715	1.760
		981.576	1.826
		995.448	1.866
		1004.273	1.902
		1013.104	1.917
		1025.717	1.950
		1040.848	2.001
4	Baar, C.A., 1977 [17	613.639	0.000
	,,, (2.	624.989	0.027
		627.508	0.043
		642.652	0.061
		655.265	0.094
		667.898	0.078
		680.504	0.127
		700.692	0.160
		718.352	0.203

TABLE 3.29.	ACCELERATED CREEP CAUSED BY HEATING A SALT MINE PILLAR TO
	PEAK TEMPERATURE OF ±423 K (Continued)

Data Set	Auth	nor(s), Yea [Ref.]	ir	t	Δl
	Poor	C A 107	7 [17]	722 224	0 221
(Cont)	baar,	U.A., 197	, [T\]	732.234	0.221
(CONC.)				744.000	0.243
				759.991	0.269
				773.877	0.279
				785.230	0.304
				801.634	0.330
				809.196	0.363
				814.206	0.462
				822.959	0.670
				829.231	0.769
				836.763	0.876
				843.042	0.960
				850.590	1.026
				858.139	1.094
				865.677	1.186
				873.229	1.244
				884.538	1.376
				893.346	1.450
				902.157	1.518
				912.234	1.577
				926.092	1.651
				931.129	1.684
				942.476	1.727
				953.822	1.767
				966.418	1.841
				980.286	1.892
				994.151	1.950
				1002.976	1.983
				1014.329	2.009
				1024.417	2.042
				1039.551	2.085


FIGURE 3.30. Accelerated creep caused by heating a salt mine pillar.

# TABLE 3.30. EFFECT OF AXIAL STRESS ON THE CREEP OF ROCK SALT [Time, t, hr; Strain, $\varepsilon$ , %]

Data Set	Author(s), [Ref.]	Year		t	ε	Remarks
1	LeComte, P.,	1965	[22]	2.548	0.643	Confining pressure =
				/./55	0.933	100 MPa;
				15.585	1.206	Temperature = $302$ K;
				20.033	1.490	Axial stress = 13.8
				20.040	1 7 2 7	MPa.
				48 247	1 00%	
				40.247 57 /01	2 130	
				73 095	2.139	
				97 949	2.301	
				124 117	2.705	
				143.746	3 186	
				158 139	3 347	
				168.608	3.443	
				194.786	3,653	
				240.595	4.023	
				265.465	4.217	
				292.956	4.394	
				311.282	4.523	
				336.158	4.652	
				362.343	4.797	
				371.506	4.862	
2	LeComte, P.,	1965	[22]	6.438	0.997	Confining pressure =
				27.368	1.271	100 MPa;
				37.836	1.383	Temperature = 377.5 K
				60.077	1.641	Axial stress = $6.9$
				/1.853	1.//0	MPa.
				83.629	1.899	
				108.490	2.108	
				1/1 217	2.301	
				155.618	2.462	
3	LeComte, P.,	1965	[22]	5.150	0.804	Confining pressure =
				13.008	0.820	100 MPa;
				24.797	0.836	Temperature = 377.5 K;
				32.655	0.853	Axial stress = $34.5$
				48.376	0.853	MPa.
				73.265	0.869	
				96.842	0.902	
				123.043	0.902	
				145.313	0.903	
				171.511	0.935	
				195.090	0.952	
				216.050	0.952	
				238.321	0.953	
				263.208	0.985	

Data Set	Author(s), [Ref.]	Year	t	E	Remarks
2	TeCente D	1065	202 227	1 002	
	Lecomie, P.,	1902	273.337	1.002	
(cont.)	[22]		226 567	1 010	
			264 074	1.019	
			201 502	1.051	
			391.383	1.068	
4	LeComte, P.,	1965	6.467	0.740	Confining pressure =
	[22]		16.944	0.772	100 MPa;
	4 5		28.734	0.772	Temperature = 377 K;
			49.693	0.789	Axial stress = $34.5$
			81.132	0.805	MPa.
			116.500	0.838	
			150.557	0.871	
			168.898	0.871	
			187.238	0.871	
5	LeComte, P.,	1965	10,451	0.257	Confining pressure =
_	[22]		24.855	0.322	100 MPa:
			36,643	0.338	Temperature = $302$ K:
			49.740	0.371	Axial stress = $6.9$
			60,219	0.387	MPa.
			79.866	0.419	
			104.749	0.484	
			127.014	0.533	
			142.735	0.533	
			151.902	0,565	
			170.242	0.566	
			180.719	0.598	



FIGURE 3.31. Effect of axial stress on creep.

# TABLE 3.31.EFFECT OF GRAIN SIZE AND AXIAL STRESS<br/>ON THE CREEP OF ROCK SALT

[Time, t, hr; Strain,  $\varepsilon$ , %]

Data Set	Author(s), [Ref.]	Year		t	ε	Remarks
1	LeComte. P.	1965	[22]	3,560	0.941	Confining pressure =
-	2000 200, 200,	1,00	[ ]	8,382	1.000	100 MPa:
				11.603	1.026	Temperature = $377.5$ K
				13.212	1.043	
				26.063	1.212	
				29.263	1.279	
				33.285	1.321	
				36.498	1.363	
				39.715	1.397	
				49.358	1.515	
				51.771	1.541	
				58.209	1.600	
				61.418	1.650	
				73.478	1.786	
				77.504	1.819	
				86.356	1.904	
				110.515	2.099	
				122.597	2.192	
				128.231	2.242	
				135.4/8	2.302	
				143.526	2.378	
				156.425	2.454	
2	LeComte, P.,	1965	[22]	2.885	0.681	Confining pressure =
				3.676	0.714	100 MPa;
				6.081	0.757	Temperature = 377.5 K
				6.872	0.790	
				10.081	0.841	
				14.089	0.908	
				16.498	0.942	
				26.967	1.027	
				32.605	1.069	
				38.249	1.103	
				51.152	1.171	
				55.178	1.205	
				65.681	1.222	
				74.563	1.248	
				82.645	1.257	
				98.800	1.291	
				106.882	1.300	
				122.232	1.326	
				134.35/	1.335	
				146.4/3	1.361	
				169.102	1.388	
				105 7(/	1.430	
				195./64	1.431	

TABLE 3.31.

EFFECT OF GRAIN SIZE AND AXIAL STRESS ON THE CREEP OF ROCK SALT (Continued)

Data Set	Author(s), [Ref.]	Year	t	ε	Remarks
2 (cont.)	LeComte, P.,	1965 [22]	217.588 246.681 265.279 288.716 311.357 333.986 359.053	1.449 1.484 1.485 1.512 1.513 1.540 1.541	
3	LeComte, P.,	1965 [22]	2.167 3.750 4.537 5.328 7.728 11.750 22.223 26.253 36.735 43.991 51.251 59.303 64.946 76.253 77.862 89.174 98.847 102.077	0.504 0.572 0.614 0.647 0.698 0.740 0.816 0.842 0.901 0.944 0.978 1.045 1.079 1.105 1.122 1.139 1.199 1.207	Confining pressure = 100 MPa; Temperature = 377.5 K; Axial stress = 6.9 MPa.



FIGURE 3.32. Combined effects of axial stress and grain size on creep rate.

#### TABLE 3.32. EFFECT OF STRESS AND TEMPERATURE ON THE STEADY STATE CREEP RATE OF COARSE GRAIN SODIUM CHLORIDE

Data Set	Author(s), [Ref.]	Year	σ	log(έ	Remarks
1	Burke, P.M., [19]	1968	4.327 8.612	-0.611E+01 -0.475E+01	Temperature = 638 K.
2	Burke, P.M., [19]	1968	3.066 5.932	-0.561E+01 -0.351E+01	Temperature = 722 K.
3	Burke, P.M., [19]	1968	2.122 4.237	-0.530E+01 -0.356E+01	Temperature = 513 K.
4	Burke, P.M., [19]	1968	0.9439 1.860	-0.530E+01 -0.424E+01	Temperature = 876 K.
5	Burke, P.M., [19]	1968	0.276 0.406 0.477 0.550 0.806 0.930 0.896	-0.539E+01 -0.494E+01 -0.519E+01 -0.457E+01 -0.411E+01 -0.356E+01 -0.336E+01	Temperature = 1015 K

[Stress,  $\sigma$ , MPa; Log Steady State Creep Rate, log  $\varepsilon$  s<sup>-1</sup>]



FIGURE 3.33. Effect of stress and temperature on the steady state creep rate of coarse grained NaCl (curve numbers correspond to data set numbers in matching table).

# TABLE 3.33.STEADY-STATE CREEP RATE OF SINGLE CRYSTAL AND POLYCRYSTALLINE<br/>SODIUM CHLORIDE AS A FUNCTION OF STRESS AT 1013 K

[Stress,  $\sigma$ , MPa; Creep Rate,  $\dot{\epsilon}$ , s<sup>-1</sup>

Data Set	Author(s), [Ref.]	Year	σ	Ê
1	Burke, P.M., [19]	1968	0.688 0.999	0.662E-03 0.209E-02
2	Burke, P.M., [19]	1968	0.499 2.391	0.928E-05 0.526E-02
3	Burke, P.M., [19]	1968	0.606 1.02	0.313E-04 0.232E-03
4	Burke, P.M., [19]	1968	0.599 0.656 0.717 0.799 0.841	0.396E-05 0.482E-05 0.515E-05 0.607E-05 0.627E-05
5	Burke, P.M., [19]	1968	0.046 0.104 1.033	0.198E-07 0.363E-03 0.326E-03
6	Burke, P.M., [19]	1968	0.104 0.296	0.363E-03 0.306E-05



FIGURE 3.34. Steady state creep rate single crystal and polycrystalline NaCl as a function of stress at 1013 K (curve numbers correspond to data set numbers in matching table).

# TABLE 3.34. STEADY STATE CREEP RATE OF NaC1 VERSUS TEMPERATURE AT VARIOUS STRESSES

Data Set	Author(s), Year [Ref.]	Т	ė	Remarks
1	Ode, H., 1968 [24]	900	0.163E-03	$\sigma$ = 0.59 MPa load
		917 999	0.754E-03 0.142E-01	stress.
		1004	0.183E-01	
2	Ode, H., 1968 [24]	907	0.178E-03	$\sigma$ = 0.78 MPa load
		937 1014	0.637E-03	stress.
		1014	0.133E-01	
3	Ode, H., 1968 [24]	937	0.194E-03	$\sigma$ = 0.98 MPa load
		943	0.344E-03	stress.
		984	0.113E-02	
		1024	0.608E-02	
		1032	0.873E-02	
		1029	0.970E-02	

[Temperature, T, K; Creep Rate, ¿, min<sup>-1</sup>]



FIGURE 3.35. Relationship of steady state creep rate of NaCl with temperature at various stresses (curve numbers correspond to data set numbers in matching table).

1				
	Dreyer, W., 1972 [12]	1.83 8.84	13.34 24.93	Artificial rock sample; confining pressure O MPa; temperature 377.65 K.
		19.74	33.38	
		29.37	38.67	
		66.67	53.84	
		84.70	58.79	
		90.93	62.33	
2	Dreyer, W., 1972 [12]	9.48	24.93	Artificial rock sample; confining pressure
		21.65	36.19	1088 MPa; temperature 471.35 K.
		40.28	46.06	
		67.93	58.40	
		90.43	68.28	
3	Dreyer, W., 1972 [12]	6.36	11.59	Artificial rock sample; confining pressure
		25.70	13.74	1088 MPa; temperature 377.65 K.
		54.06	16.62	
		83.72	19.49	
		121.12	22.39	
4	Dreyer, W., 1972 [12]	27.71	3.57	Artificial rock salt sample; confining pres-
		53.51	4.69	sure O MPa; temperature 302.15 K.
		81.90	5.45	
		105.12	5.86	
		123.82	6.25	
		150.27	7.00	
5	Dreyer, W., 1972 [12]	6.42	3.52	Artificial rock salt sample; confining pres-
		23.85	2.51	sure 212 MPa; temperature 302.15 K.
		36.10	2.89	·
		56.75	2.59	
		78.69	2,99	
		118.68	4.14	
		141.91	3.84	
		183.19	4.95	
		103713	1.01	
6	Dreyer, W., 1972 [12]	6.42	3.52	Artificial rock salt sample; confining pres-
		23.21	2.51	sure 1088 MPa; temperature 302.15 K.
		36.11	2.89	
		56.75	2.94	
		/8.69	2.99	
		100.62	3.74	
		125.13	.3.80	
		167 07	4.21 3.20	
		175.46	3.57	
		183.20	3.58	

TABLE 3.35.	TIME-STRAIN	DATA	OF	HALITIC	ROCK	SALT	AT	VARIOUS	CONFINING	PRESSURES	AND	TEMPERATURES
				[Time.	t. h	rs: Si	ra	in. ε. %]				



FIGURE 3.36. Time-strain relationship for halitic rock salt (curve numbers correspond to data numbers in matching table ).

Data Set	Author(s), Year [Ref.]	t	£	Remarks
1	Dreyer, W., 1972 [12]	0.25 0.50 0.75 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 28 56 84 112 140	86 102 112 119 144 161 173 182 188 193 198 203 208 213 208 213 217 221 224 228 235 238 264 307 324 335 342	Square prisms (4 x 4 x 10 cm) of white rock salt containing alternating layers of fine and coarse grained material separated by thin argillaceous bands of anhydrite; untempered; constant stress of 106 MPa; temperature 291 K.
2	Dreyer, W., 1972 [12]	103 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 22 24 26 28	348 359 363 366 368 369 369 369 370 370 370 370 370 370 370 370	Tempered; sample and testing conditions same as above.

TABLE 3.36.	TIME-STRAIN RELATIONSHIP	OF	TEMPERED	AND	UNTEMPERED	ROCK	SALT	AT	106	MPa	AND	298	К
	Time	e. 1	t. days: S	Strat	in. ε. %]								



FIGURE 3.37 Time-strain relationship for tempered and untempered rock salt (curve numbers correspond to data set numbers in matching table).

TABLE 3.37. RELATIONSHIP OF MICROHARDNESS TO INDENTATION DEPTH OF ROCK SALT [Indentation Depth, h, µm; Microhardness, H, kg mm<sup>-2</sup>; Load, P, g]

1       Strelkov, P.G., Shpunt, A.A., and Nabutovskaya, 0.A., 1967 [15]       1.31       10.25       NaCl specimen; plastic ded dry air with atmospheric         0.A., 1967 [15]       2.06       18.89       3.16       20.50         4.54       20.51       6.26       20.54         9.70       20.33       13.70       20.35         19.70       20.15       1.85       21.84         2       Strelkov, P.G., et al., 1967 [15]       1.44       20.02       Deformed specimen of NaCl plastic deformation (ɛ) ≥         3       Strelkov, P.G., et al., 1967 [15]       0.58       43.42       NaCl; plastic deformation	$ \begin{array}{r} 1.31\\ 1.65\\ 2.06\\ 3.16\\ 4.54\\ 6.26\\ 9.70\\ 13.70 \end{array} $	10.25 17.07 18.89 20.50 20.51 20.54	NaCl specimen; plastic deformation (ɛ)≈0; dry air with atmospheric humidity (B) ≤ 30%.
A.A., and Nabutovskaya, 0.A., 1967 [15]       1.65       17.07       dry air with atmospheric         0.A., 1967 [15]       2.06       18.89       3.16       20.50         4.54       20.51       6.26       20.54       9.70       20.33         13.70       20.35       19.70       20.15       Deformed specimen of NaCl         2       Strelkov, P.G., et al., 1967 [15]       1.44       20.02       Deformed specimen of NaCl         3       Strelkov, P.G., et al., 1967 [15]       0.58       43.42       NaCl; plastic deformation	$ \begin{array}{r} 1.65\\ 2.06\\ 3.16\\ 4.54\\ 6.26\\ 9.70\\ 13.70\end{array} $	17.07 18.89 20.50 20.51 20.54	dry air with atmospheric humidity (B) $\leq 30\%$ .
<ul> <li>0.A., 1967 [15]</li> <li>2.06 18.89</li> <li>3.16 20.50</li> <li>4.54 20.51</li> <li>6.26 20.54</li> <li>9.70 20.33</li> <li>13.70 20.35</li> <li>19.70 20.15</li> <li>2 Strelkov, P.G., et al., 1.44 20.02 Deformed specimen of NaCl plastic deformation (c) ≥</li> <li>2 Strelkov, P.G., et al., 0.58 43.42 NaCl; plastic deformation 1967 [15]</li> <li>3 Strelkov, P.G., et al., 0.73 37.28</li> </ul>	2.06 3.16 4.54 6.26 9.70	18.89 20.50 20.51 20.54	
3.16       20.50         4.54       20.51         6.26       20.54         9.70       20.33         13.70       20.35         19.70       20.15         2       Strelkov, P.G., et al.,       1.44       20.02       Deformed specimen of NaCl         1967       [15]       1.85       21.84       plastic deformation (ε) ≥         3       Strelkov, P.G., et al.,       0.58       43.42       NaCl; plastic deformation         1967       [15]       0.73       37.28       1.85       1.85	3.16 4.54 6.26 9.70	20.50 20.51 20.54	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.54 6.26 9.70 13.70	20.51	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	6.26 9.70 13.70	20.54	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.70 13.70	20.00	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	13 70	20.33	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	T.) • / O	20.35	
2       Strelkov, P.G., et al., 1967 [15]       1.44 2.85 2.84 2.88 2.77 4.54       20.02 2.84 2.88 2.77 4.54       Deformed specimen of NaCl plastic deformation (ε) ≥         3       Strelkov, P.G., et al., 1967 [15]       0.58 0.73 0.73 0.73       43.42 37.28       NaCl; plastic deformation	19.70	20.15	
1967 [15]       1.85       21.84       plastic deformation (ε) ≥         2.88       22.77       4.54       20.51         3       Strelkov, P.G., et al., 1967 [15]       0.58       43.42       NaCl; plastic deformation (ε)	1.44	20.02	Deformed specimen of NaC1; dry atmosphere;
2.88 22.77 4.54 20.51 3 Strelkov, P.G., et al., 0.58 43.42 NaCl; plastic deformation 1967 [15] 0.73 37.28	1.85	21.84	plastic deformation ( $\varepsilon$ ) $\ge 0.3-0.4\%$ .
4.54         20.51           3 Strelkov, P.G., et al.,         0.58         43.42         NaCl; plastic deformation           1967 [15]         0.73         37.28	2.88	22.77	
3         Strelkov, P.G., et al.,         0.58         43.42         NaCl; plastic deformation           1967 [15]         0.73         37.28	4.54	20.51	
1967 [15] 0.73 37.28	0.58	43.42	NaCl; plastic deformation ( $\varepsilon$ ) $\approx$ 0; moist air
	0.73	37.28	
1.22 30.47	1.22	30.47	
1.63 29.11	1.63	29.11	
2.05 27.75	2.05	27.75	
2.46 26.85	2.46	26.85	
2.74 26.17	2.74	26.17	
3.57 23.91	3.57	23.91	
3.85 23.23	3.85	23.23	
4.12 22.78	4.12	22.78	
6.26 20.54	6.26	20.54	



FIGURE 3.38. Relationship of microhardness to indentation depth of rock salt (curve numbers correspond to data set numbers in matching table).

the change in microhardness H of NaCl samples of nominal purity (Ca<sup>2+</sup>  $10^{-3}$ - $10^{-2}$  mole %) in relation to the quench temperature T. The curve exhibits maxima and minima attributable to the presence of impurities in the crystals. At temperatures greater than 873 K (600°C) the microhardness increases without any deviations. On reducing the quenching rate, the microhardness of the samples diminishes and so does the difference between maximum and minimum values.

Figure 3.40 shows the quench temperature dependence of microhardness of NaCl crystals containing impurities. These data are also from reference [14] and tabulated in table 3.39. For the purest material no maxima and minima appear, even for very high cooling rates as indicated by curve 1. It can be seen from this figure that for a quench temperature of over 873 K (600° C), the microhardness gradually increases, independently of the impurity content, and approaches a constant value on quenching from about the melting point of the crystal.

## **3.6.** Surface Effects

### 3.6.1. Joffé Effect

The Joffé effect is the only surface effect considered here. The Joffé effect is attributed to microfractures in the surface of the crystals. If surface microfractures are removed either by etching or the chemical polishing process, the ductility of a crystal is increased significantly. Cleaved crystals are known to fracture after about 2% elongation, while the maximum elongation for polished crystals was 20%. Crystals that were tested in solvent show even higher ductility.

The behavior of single halite crystals is strongly influenced by the surface preparation of the crystal itself prior to loading and consequent deformation. It is thought that microfractures on the surface of crystals cause brittleness. If these microfractures are removed by either polishing or etching, the ductility of the crystal increases significantly.

Data Set	Author(s), Year [Ref.]	Т	Н	Remarks
1	Kishsh, I. and Sharkezi,	306.0	21.58	2 x 2 x 6 mm NaCl crystals preliminarily
	1., 1971 [14]	379.5	22.02	annealed at 923 K and then cooled at 2 deg/
		429.7	22.59	h; both slow and fast quenching used; Zeiss
		483.9	22.59	Model 32 used for microhardness determina-
		530.1	23.52	tion with an indentor load of 4 g; 30-40
		584.2	24.45	impressions used for hardness estimation.
		630.9	22.96	
		681.4	21.97	
		735.5	22.68	
		785.6	23.89	
		839.8	23.76	
		890.2	23.33	
		940.3	24.19	
		990.4	25.68	
		1040.6	26.11	

TABLE 3.38. QUENCH TEMPERATURE DEPENDENCE OF MICROHARDNESS OF ROCK SALT

[Quench Temperature, T, K; Microhardness, H, kg mm<sup>-2</sup>]



FIGURE 3.39. Dependence of microhardness on quench temperature of rock salt (curve numbers correspond to data set numbers in matching table).

Data Set	Author(s), Year [Ref.]	T	Н	Remarks
	Kishsh. I. and Sharkezi.	298.2	21.75	Sample and testing conditions same as those
-	I., 1971 [14]	374.6	21.80	of Table 3.17; impurity introduced but total
		441.6	21.91	impurity is under $10^{-7}$ mole %.
		527.4	21.97	
		578.4	22.02	
		629.3	22.07	
		6/0.0 721 1	22.13	
		776 9	22.23	
		833.0	22.68	
		934.3	23.28	
		984.9	23.89	
		1035.6	24.50	
2	Kishsh, I. and Sharkezi,	303.1	22.20	Sample same as above; $Ca^{2+} 10^{-5}$ mole %.
	I., 1971 [14]	374.3	22.30	
		4/1.0	22,56	
		526.9	22.70	
		629 0	22.07	
		675.0	22.27	
		725.6	22.97	
		776.1	23.73	
		832.3	23.53	
		883.3	23.43	
		934.0	23.83	
		984.7 1035.5	24.24 24.59	
2		202.0	00.65	2 1 0 <sup>2+</sup> 10 <sup>-3</sup> 10 <sup>-2</sup> 1 <sup>w</sup>
3	Kishsh, I. and Sharkezi,	302.8	22.65	Sample same as above; Ca <sup>-</sup> 10 <sup>-</sup> -10 <sup>-</sup> mole %.
	1., 19/1 [14]	480 5	22.90	
		531.0	24.36	
		576.8	24.82	
		628.3	23.72	
		669.8	22.47	
		730.4	23.37	
		781.0	24.03	
		832.1	23.88	
		883.2	23.63	
		933.9	24.03	
		1035.4	24.39	
4	Kishsh. I. and Sharkezi.	302.7	22.85	Sample same as above: $As^+ 10^{-1}$ mole % + $Ca^{+2}$
·	I 1971 [14]	378.9	23.26	$10^{-3}$ mole %.
		480.3	24.16	
		530.9	24.81	
		576.5	25.32	
		628.0	24.37	
		679.8	22.77	
		725.0	23.97	
		/05.4	22.33	
		882 9	24.03	
		933.7	24.44	
		989.6	24.74	
		1035.3	24.89	

# TABLE 3.39. QUENCH TEMPERATURE DEPENDENCE OF MICROHARDNESS OF ROCK SALT CRYSTALS CONTAINING IMPURITIES

[Quench Temperature, T, K; Microhardness, H, kg mm<sup>-2</sup>]



FIGURE 3.40. Dependence of microhardness on quench temperature of impure rock salt crystals (curve numbers correspond to data set numbers in matching table).

Stokes, Johnston, and Li [3] have studied the Joffé effect on NaCl crystals. Their data are tabulated in table 3.40 and shown in figure 3.41. A plot of the resolved shear stress versus percent strain is given for differently prepared single NaCl crystals. Curves for the following conditions are presented:

1. Fresh cleaved crystal.

2. Polished crystal deliberately "painted" and showing a stain.

3. Polished crystal showing a stain and exposed to humid atmosphere.

4. Unstained polished crystal after one day in dry air.

5. The same as curve 4.

6. Unstained polished crystal after eight days in dry air.

7. Unstained polished crystals after three months in dry air.

An interesting feature of the data in figure 3.41 is that storage time seems to play no part in the ductility of polished crystals. For details concerning the test, see the section on the measurement methods.

## 3.7. Effect of Nuclear Irradiation on Mechanical Properties of Rock Salt

Ionizing radiation leads to a significant variation of the stress-strain properties of rock salt. The effect of radiation varies with temperature, the time of radiation, the radiation dose, as well as with the type of salt considered and the dimensions of the specimen.

### 3.7.1. Effect on Stress-Strain Behavior

Bradshaw et al. [13] performed uniaxial compression testing on bedded salt and dome salt to evaluate the effects of radiation on stress-strain behavior, maximum compressive stress, and yield stress. The tests were first run at 293 K and then at 473 K using radiation doses of 0, 10<sup>6</sup>, 10<sup>7</sup>, 10<sup>8</sup>, and 5×10<sup>8</sup> R, respectively. Three samples each of dome salt of two cases: (1) bedded salt with force applied perpendicular to bedding planes, and (2) bedded salt with force applied parallel to bedding planes, were considered. Their values are presented in Tables 3.41 and 3.42 and have been plotted in figures 3.42 and 3.43, respectively. Figure 3.42 shows the stress-strain curves for different exposure doses and the force applied perpendicular to bedding planes at 293 K. Figure 3.43 shows the relationship between radiation dose and maximum compressive stress and yield stress at 293 K. These investigations indicate the following trends:

1. The maximum compressive stress of rock salt exposed to  $5 \times 10^8$  R is less than that of unirradiated salt for both bedded and dome salt.

2. At exposures of  $5 \times 10^8$  R and 473 K, there is little difference between the stress capacities of bedded and dome salt.

3. The yield stress of dome salt is higher than the yield stress of bedded salt for radiation doses  $< 3 \times 10^7$  R.

Studies by Demidova and Gol'denberg [10] have shown that generally the yield limit of NaCl crystal irradiated at room temperature increases with irradiation

Data Set	Author(s), Year [Ref.]	τ	З	Remarks
1	Stokes, R.J., Johnston,	0.23	0.43	Cleaved NaCl crystals; all tests (Data Sets
	T.L., and Li, C.H., 1959	0.55	0.47	1-7) done on a conventional hard tensile
	[3]	0.75	0.51	machine at what is assumed to be room tem-
		0.87	0.51	perature.
		0.94	0.66	
		1 04	1 15	
		1.08	1.48	
		1.18	1.87	
		1.22	2.14	
		1.26	2.47	
2	Stokes, R.J., et al.,	0.29	3.97	Polished NaCl crystals deliberately "painted"
	1959 [3]	0.65	3.89	and showing a stain.
		0.85	3.98	
		1.04	3.9/	
		1 25	4.13	
		1.36	4.62	
3	Stokes, R.J., et al.,	0.22	4.80	Polished NaCl crystals showing a stain and
	1959 [3]	0.58	4.77	exposed to a humid atmosphere.
		0.73	4.99	
		0.83	5.20	
		0.86	5.48	
		0.96	5.86	
		1.04	6.24	
4	Stokes, R.J., et al.,	0.19	7.89	Unstained polished crystals of NaCl after
	1959 [3]	0.43	7.82	l day in dry air.
		0.77	7.86	
		0.88	7.91	
		0.97	7.90	
		1.03	8.17	
		1.13	8.61	
		1 3/	9.05	
		1.50	10.08	
		1.71	10.68	
		1.92	11.22	
		2.16	11.81	
		2.47	12.34	
		2.70	12.77	
		3.07	13.30	
		3.50	14.00	
		3.97	14.91	
		4.40	17 01	
		5.30	18.26	
		5.70	19.50	
		6.1	21.08	
		6.42	22.50	
		6.71	23.86	
		7.00	25.28	
		7.29	26.87	
		7.51	28.40	
		/./	29.78	

TABLE 3.40. STRESS-STRAIN RELATIONSHIP OF ROCK SALT CRYSTAL HAVING DIFFERENT SURFACE CONDITIONS [Resolved Shear Stress,  $\tau$ , MPa; Strain,  $\varepsilon$ , %]

.

Data Set	Author(s), Year [Ref.]	τ	ε	Remarks
5	Stokes, R.J., Johnston,	0.2	9.60	Unstained polished NaCl crystals after 1 day
	T.L., and Li, C.H., 1959	0.52	9.70	in dry air.
	[3]	0.78	9.00	
		1 02	9.07	
		1.08	10.16	
		1.12	10.49	
		1.20	10.87	
		1.33	11.36	
		1.55	12.07	
		1.81	12.82	
		2.18	13.80	
		2.50	14.77	
		2.88	15.80	
		3.23	17 02	
		3.82	18 90	
		4.13	20.01	
		4.5	21.34	
		4.9	22.64	
6	Stokes, R.J., et al.,	0.18	13.09	Unstained polished NaCl crystals after 8
	1959 [3]	0.46	13.07	days in dry air.
		0.67	13.22	
		0.77	13.33	
		0.86	13.65	
		1.03	14.03	
		1.30	14.57	
		1.05	15.10	
		2 33	16 94	
		2.67	17.97	
		3.08	19.16	
		3.42	20.36	
		3.77	21.55	
		4.10	22.75	
		4.35	23.89	
		4.54	24.88	
7	Stokes, R.J., et al.,	0.10	17.90	Unstained polished NaCl crystals after 3
	1959 [3]	0.38	17.88	months in dry air.
		0.72	17.86	
		0.98	19.00	
		1 14	18 17	
		1 23	18 38	
		1.37	18.71	
		1.48	18,92	
		1.67	19.63	
		2.04	20.60	
		2.36	21.41	
		2.72	22.33	
		3.08	23.14	
		3.45	23.95	
		3.75	24.43	
		4.11	25.33	
		4.38	25.94	

# TABLE 3.40. STRESS-STRAIN RELATIONSHIP OF ROCK SALT CRYSTAL HAVING DIFFERENT SURFACE CONDITIONS (continued)



FIGURE 3.41. Stress-strain relationship of salt crystals having different surface conditions.

Data Set	Author(s), Year [Ref.]	σ1	ε	Remarks
1	Bradshaw, R.L., Limpson, F.M., Boegly, W.J., Jr., Kubobta, H., Parker, F.L., and Struxness, E.G., 1968 [13]	10.6 13.8 15.7 19.0 21.5 23.6 25.2 26.1 26.7 27.1 27.2 27.3 27.3	$\begin{array}{c} 0.006\\ 0.009\\ 0.011\\ 0.016\\ 0.021\\ 0.026\\ 0.031\\ 0.036\\ 0.041\\ 0.046\\ 0.051\\ 0.056\\ 0.061\\ \end{array}$	2" x 2" cubes of bedded salt; force applied perpendicular to planes of stratification at room temperature; unirradiated.
2	Bradshaw, R.L., et al., 1968 [13]	5.0 9.3 12.4 14.3 17.4 20.0 21.9 23.5 24.7 25.5 25.8 25.8 25.9 25.6 25.6	0.002 0.006 0.009 0.010 0.021 0.026 0.031 0.036 0.041 0.046 0.051 0.056 0.061	Sample similar to above; irradiated to 10 <sup>6</sup> R.
3	Bradshaw, R.L., et al., 1968 [13]	4.9 11.3 15.0 16.9 20.5 23.1 25.0 26.5 27.5 28.0 28.0 28.0 28.0 28.0 27.9	0.002 0.006 0.009 0.011 0.021 0.026 0.031 0.036 0.041 0.046 0.051 0.056 0.061	Sample similar to above; irradiated to 10 <sup>7</sup> R.
4	Bradshaw, R.L., et al., 1968 [13]	5.3 $11.5$ $15.4$ $17.3$ $20.9$ $23.3$ $25.3$ $26.3$ $27.1$ $27.3$ $26.6$ $25.7$ $25.1$ $24.8$	0.002 0.005 0.009 0.011 0.021 0.027 0.031 0.036 0.041 0.046 0.051 0.056 0.061	Sample similar to above; irradiated to 10 <sup>8</sup> R.
5	Bradshaw, R.L., Limpson, F.M., Boegly, W.J., Jr., Kubota, H., Parker, F.L., and Struxness, E.G., 1968 [13]	5.27 10.95 15.20 17.57 21.20 22.8 23.8 24.3 23.8 22.7 21.1 19.5 18.5	$\begin{array}{c} 0.002\\ 0.006\\ 0.009\\ 0.011\\ 0.016\\ 0.021\\ 0.026\\ 0.031\\ 0.036\\ 0.041\\ 0.046\\ 0.051\\ 0.055 \end{array}$	Sample similar to above; irradiated to 5 x 10 <sup>8</sup> R.

## TABLE 3.41. RADIATION EFFECTS ON STRESS-STRAIN RELATIONSHIP OF ROCK SALT

[Compressive Stress,  $\sigma_1$ , MPa; Strain,  $\epsilon$ , in/in]



FIGURE 3.42. Effect of radiation on the stress-strain behavior of rock salt (curve numbers correspond to data set numbers in matching table).

#### TABLE 3.42. MAXIMUM COMPRESSIVE AND YIELD STRESS OF ROCK SALT FROM HUTCHINSON, KANSAS, AND GRAND SALINE, TEXAS

All results have been rounded off to the nearest .69 MPa and standard deviation to the nearest .34 MPa.

Type of Salt	Exposure Dose (R)	Maximum Compressive Stress MPa	Yield Stress MPa
	At 293	K	
Bedded Parallel	0 10 <sup>6</sup> 10 <sup>7</sup> 10 <sup>8</sup> 5 x 10 <sup>8</sup>	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$
Bedded Perpendicular	0 10 <sup>6</sup> 10 <sup>7</sup> 10 <sup>8</sup> 5 x 10 <sup>8</sup>	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c} 15.86 \ \pm \ 2.07 \\ 12.41 \ \pm \ 1.72 \\ 15.86 \ \pm \ 3.45 \\ 16.55 \ \pm \ 3.45 \\ 16.55 \ \pm \ 2.07 \end{array}$
Dome	0 10 <sup>6</sup> 10 <sup>7</sup> 10 <sup>8</sup> 5 x 10 <sup>8</sup>	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{r} 19.99 \pm 1.03 \\ 19.99 \pm 1.03 \\ 20.68 \pm 0.69 \\ 18.62 \pm 0.69 \\ 17.93 \pm 1.39 \end{array}$
	At 473	K	
Bedded Parallel	0 5 x 10 <sup>8</sup>	26.89 ± 1.38 23.44 ± 2.76	11.03 ± 1.39 13.10 ± 1.72
Bedded Perpendicular	0 5 x 10 <sup>8</sup>	24.82 ± 0.69 22.75 ± 2.76	11.03 ± 0.69 14.48 ± 1.03
Dome	$ \begin{smallmatrix} 0 \\ 5 \times 10^8 \\ \end{smallmatrix} $	24.82 ± 3.45 21.37 ± 2.07	13.10 ± 1.03 15.86 ± 1.03

(After Bradshaw [13], 1968)

Bedded Parallel: bedded salt, force applied parallel to the planes of stratification.

Bedded Perpendicular: bedded salt, force applied perpendicular to the plane of stratification.



FIGURE 3.43. Relationship between maximum compressive stress and radiation dose.

dose; at low doses the temperature hardening mechanism controls while at higher doses a temperature insensitive mechanism prevails. They also observed that even before two hours of irradiation had occurred, the strain was elastic while the failure was brittle. Only at rupture a small local plastic strain was evident. Whisker crystals irradiated for two or more hours revealed macroscopic plastic flow only if they had first been subject to plastic strain. A substantial difference in the extent of the variation in the ultimate strength of crystals of different diameters was shown as the radiation dose was varied [8]. The ultimate tensile stress capacity of NaCl whisker crystals, measuring 18  $\mu$ m in diameter, was observed to increase first and then decrease, passing through a maximum at an irradiation time of about eight hours as shown in figure 3.44 with the corresponding values in table 3.43. Specimens measuring 86 µm in diameter under the same conditions exhibited a gradual increase in the degree of hardening with dose.

Figure 3.45 is also taken from Demidova and Gol'denberg [10] and shows that another effect of radiation is the change in the nature of crystal whisker fracture. The corresponding values are tabulated in table 3.44. Prior to exposures the specimens fail in a plastic mode whereas the exposed specimens fracture primarily in a brittle mode.

#### 3.7.2. Effect on Young's Modulus

The relationship between radiation dose and Young's modulus as investigated by Bradshaw et al. [13] is given in table 3.45 and plotted in figure 3.46. There is a general increase in modulus of elasticity with increase in radiation dose but this trend is irregular and inconsistent.

#### 3.7.3. Effect on Creep

In addition to the static tests, the creep rate resulting from the application of a constant force of 17.237 MPa for 100 minutes was measured by Bradshaw et al. [13]. Figure 3.47 shows the creep curves for bedded salt with the corresponding values given in Table 3.46. The irradiated salt which received  $5 \times 10^8$  R was stronger as shown by less creep.

#### 3.7.4. Effect on Hardness

The hardness of NaCl crystals increases on irradiation. Small irradiation doses, however, produce very little hardening compared to coloration. Demidova and Gol'denberg [10] observed that: (1) two hours of exposure to x-rays result in hardening of crystal whiskers, and (2) the degree of hardening increases as the diameter diminishes.

	[Irradiation	Time, t	, hrs;	Tensile Stress, o <sub>t</sub> , MPa]
Data Set	Author(s), Year [Ref.]	t	σt	Remarks
1	Demidova, N.N. and Gol'denberg, S.U., 1975 [8]	-0.08 1.91 3.81 7.78 11.87 15.96	2.89 5.61 10.06 16.94 10.84 3.88	NaCl whisker crystals measuring 10-100 $\mu m$ in diameter cultivated from solution using the Amelinck method; specimens irradiated at room temperature; this data obtained for a specimen with a diameter of 18 $\mu m$ .
2	Demidova, N.N. and Gol'denberg, S.U., 1975, [8]	0.09 2.07 3.95 8.07 15.96	1.20 2.29 2.99 4.24 5.46	This data obtained for a specimen with a diameter of 86 m.





FIGURE 3.44. Dependence of ultimate stress capacity of NaCl crystal whiskers on irradiation time (curve numbers correspond to data set numbers in matching table).

Data Set	Author(s), Year [Ref.]	σ <sub>t</sub>	E	Remarks
1	Demidova, N.N. and Gol'denberg, S.U., 1975 [8]	$\begin{array}{c} 15.11\\ 17.17\\ 16.75\\ 18.80\\ 17.98\\ 16.75\\ 19.20\\ 17.97\\ 16.75\\ 17.96\\ 19.20\\ 20.0\\ 20.0\\ 20.0\\ 20.0\\ 20.0\\ 20.0\\ 21.23\\ 21.22\\ 22.04\\ 23.26\\ 21.22\\ 22.04\\ 23.26\\ 21.22\\ 22.04\\ 23.26\\ 21.22\\ 22.45\\ 20.4\\ 23.75\\ 23.80\\ 24.63\\ 25.48\\ 26.31\\ 26.73\\ 26.73\\ 26.73\\ 26.73\\ 26.73\\ 26.73\\ 26.73\\ 26.73\\ 26.73\\ 26.73\\ 27.15\\ 27.99\\ 28.92\\ \end{array}$	$\begin{array}{c} 1.74\\ 1.75\\ 5.08\\ 5.92\\ 6.75\\ 9.24\\ 11.76\\ 13.42\\ 15.08\\ 16.75\\ 19.26\\ 20.93\\ 23.43\\ 25.09\\ 27.60\\ 30.10\\ 30.94\\ 33.44\\ 35.10\\ 30.94\\ 33.44\\ 35.10\\ 36.77\\ 38.43\\ 40.11\\ 42.62\\ 48.07\\ 51.70\\ 53.52\\ 55.36\\ 58.97\\ 60.79\\ 64.42\\ 266.24\\ 69.66\\ 54.62\\ 66.24\\ 69.66\\ 69.66\\ 66.24\\ 69.66\\ $	Unexposed; NaCl crystal whiskers grown by Amelinck method from solution and tested on a tensile machine; specimen diameter 13.7 μ.
2	Demidova, N.N. and Gol'denberg, S.U., 1974 [10]	29.63 29.67 30.09 31.34 31.77 32.60 32.61 5.24 12.57 19.89 29.30 38.71 44.99 55.45 61.73 72.73 79.51 87.87	0.11 0.23 0.33 0.46 0.57 0.69 0.79 0.89 1.01 1.12 1.22	Exposed; NaCl crystal whiskers grown by Amelinck method from solution and irradiated directly on a tensile ma- chine with unfiltered x-radiation for 2 hours; diameter of crystal whisker used 26 µ.

TABLE 3.44. EFFECT OF RADIATION ON TENSILE STRESS-STRAIN BEHAVIOR OF NaCl CRYSTAL WHISKER [Tensile Stress,  $\sigma_t$ , MPa; Strain,  $\varepsilon$ , %]



FIGURE 3.45. Effect of radiation on tensile stress-strain behavior of a NaCl crystal whisker (curve numbers correspond to data set numbers in matching table).

# TABLE 3.45. YOUNC'S MODULUS OF ROCK SALT FROM HUTCHINSON, KANSAS, AND GRAND SALINE, TEXAS

All results have been rounded off to the nearest .69 MPa and the standard deviation to the nearest .34 MPa.

Type of Salt	Exposure Dose, D (R)	Modulus of Elasticity, Es GPa
	<u>At 293 K</u>	
Bedded Parallel	0 10 <sup>6</sup> 10 <sup>7</sup> 10 <sup>8</sup> 5 x 10 <sup>8</sup>	$\begin{array}{r} 2.41 \pm 0.41 \\ 2.21 \pm 0.41 \\ 2.41 \pm 0.14 \\ 2.48 \pm 0.62 \end{array}$
Bedded Perpendicular	0 10 <sup>6</sup> 10 <sup>7</sup> 10 <sup>8</sup> 5 x 10 <sup>8</sup>	$\begin{array}{r} 2.48 \pm 0.80 \\ 2.41 \pm 0.69 \\ 2.62 \pm 0.26 \\ 2.62 \pm 0.41 \\ 2.55 \pm 0.76 \end{array}$
Dome	$ \begin{array}{r} 0 \\ 10^{6} \\ 10^{7} \\ 10^{8} \\ 5 \times 10^{8} \end{array} $	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$
Bedded Parallel	<u>At 473 K</u>	$0.62 \pm 0.07$
	$5 \times 10^{8}$	$0.83 \pm 0.14$
Bedded Perpendicular	0 5 x 10 <sup>8</sup>	0.90 ± 0.07 0.90 ± 0.07
Dome	0 5 x 10 <sup>8</sup>	0.96 ± 0.07 1.10 ± 0.07

(After Bradshaw [13], et al.)



FIGURE 3.46. Variation of Young's Modulus of rock salt with radiation dosage.

Data Set	Author(s), Year [Ref.]	t	ε	Remarks
1	Bradshaw, R.L., Limpson.	0.9	9.00	Bedded salt with force applied perpendicular
-	F.M., Boegly, W.J., Jr.,	1.4	10.50	to planes of stratification; constant load
	Kubobta, H., Parker, F.L.,	2.9	10.88	of 17.237 MPa.
	and Struxness, E.G.,	6.4	11.26	
	1968 [13]	10.3	11.57	
		15.5	11.53	
		26.6	11.92	
		40.8	11.95	
		60.6	11.98	
		80.1	12.29	
		100.2	12.31	
2	Bradshaw, R.L., et al.,	0.9	6.25	Similar conditions as Data Set 1: irradi-
	1968 [13]	1.4	10.25	ated to 5 x $10^8$ R.
		1.9	11.38	
		4.6	14.63	
		8.3	15.14	
		12.5	15.65	
		21.7	15.91	
		30.8	16.31	
		50.6	16.47	
		70.4	16.75	
		90.2	17.04	

# TABLE 3.46. EFFECT OF IRRADIATION ON CREEP PROPERTIES OF ROCK SALT [Time, t, min; Strain, $\varepsilon$ , (in/in) x 10<sup>3</sup>]



FIGURE 3.47. Effect of radiation on the creep of rock salt (curve numbers correspond to data set numbers in matching table).

Figure 3.48 from Inabe and Takeuchi [9] shows the relationship between Vickers hardness and x-ray dosage for specimens annealed and reheated up to 600°C and then cooled. The corresponding values are tabulated in table 3.47.

## 3.7.5. Evaluation of Data

At this stage the published data do not permit the generation of recommended values of the mechanical properties of rock salt. The available data are contradictory and even though measurements seem to have been carefully conducted, the nature of the material under consideration makes it difficult to characterize it adequately.

TABLE 3.47. VICKER'S MICROHARDNESS OF NaCl CRYSTALS AS A FUNCTION OF X-RAY DOSE

[X-Ray Dose, 10<sup>5</sup> R; Change in Vicker's Microhardness,  $\Delta H_v$ , kg mm<sup>-2</sup>]

abe. K. and Takeuchi.	0.09	0.21	NaCl crystals grown in air by Kyropoulos
. 1973 [9]	0.30	0.45	technique from a melt reagent grade material.
,	1.05	0.81	Specimens annealed in air at 923 K for 80
	2.05	1.08	hours and slowly cooled at 293 K/hr.
	3.06	1.00	
nabe, K. and Takeuchi,	0.09	0.10	NaCl crystals grown as indicated above; how-
, 1973 [9]	0.31	0.20	ever they were reheated to 873 K and allowed
	1.03	0.49	to cool on an asbestos plate.
	2.01	0.55	•
	3.00	0.50	
	abe, K. and Takeuchi, , 1973 [9] nabe, K. and Takeuchi, , 1973 [9]	abe, K. and Takeuchi,       0.09         , 1973 [9]       0.30         1.05       2.05         3.06         mabe, K. and Takeuchi,       0.09         , 1973 [9]       0.31         1.03       2.01         3.00       3.00	abe, K. and Takeuchi,       0.09       0.21         , 1973 [9]       0.30       0.45         1.05       0.81       2.05       1.08         3.06       1.00       0.09       0.10         nabe, K. and Takeuchi,       0.09       0.10       0.31       0.20         1.03       0.49       2.01       0.55       3.00       0.50



3.48. Effect of radiation on the microhardness of rock salt (curve numbers correspond to data set numbers in matching table.)

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#### Symbols and Units

Symbol	Name	Unit
P	Pressure	MPa, GPa
ρ	Density	kg m <sup>-3</sup>
$ ho_0/ ho$	Compression	dimensionless
Ε	Young's modulus	GPa
G	Shear modulus	GPa
Ks	Bulk modulus	GPa
μ	Poisson's ratio	dimensionless
ν	Velocity	m s <sup>-1</sup>
τ	Shear stress	GPa
e	Strain, also true strain	%, in/in
ε	Creep, also strain rate	$t^{-1}$
σ	Compressive stress	MPa, GPa
$(\sigma_1 - \sigma_3)$	Differential stress	MPa, GPa
t	Time	min, h, s
Η	Hardness	kg mm <sup>-2</sup>
Т	Temperature	ĸ
$\sigma_{t}$	Tensile stress	MPa
$\Delta L$	Change in length	cm

#### **Conversion Factors**

Pressure		
To convert from	to	Multiply by
MPa	lb in <sup>-2</sup> (usi)	$1.45138 \times 10^{2}$
MPa	kbar	$1 \times 10^{-2}$
GPa	lb in <sup>-2</sup> (psi)	$1.45138 \times 10^{5}$
GPa	kbar	10
	bar	$10 \times 10^{3}$
Density		
To convert from	to	Multiply by
kg · m <sup>-3</sup>	lb•ft⁻³	0.06243
kg ⋅ m <sup>-3</sup>	g •' cm <sup>−3</sup>	$1 \times 10^{-3}$
Temperature		
To convert from	to	Subtract
K	°C	273.15

# **Chapter 4**

# Thermophysical Properties J. M. Yang\*

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## 4.1. Introduction

In this chapter the thermophysical properties (thermal conductivity, thermal diffusivity, and thermal linear expansion) of rock salt are discussed. Recommended values which were generated from the analysis and synthesis of the available experimental data are presented. In spite of the fact that the study of molten salts has increased notably in the past thirty years, experimental data on molten rock salt are still very scanty. As a consequence, no recommended values were generated for thermal conductivity above the melting point. Recommended values of the thermal diffusivity were derived by correlating the recommended values of thermal conductivity, specific heat, and thermal expansion. In those cases where the reported values are not adequately substantiated by experimental data or where the material cannot be uniquely characterized, the term "typical" values is used. No attempt was made to estimate the thermal diffusivity beyond the melting point.

The data sets upon which the recommended values are based are shown in the various figures for the respective properties. Additional data sources are given as references.

## 4.2. Review of Measurement Methods for Thermophysical Properties

Many different methods and variations for measuring the thermophysical properties of solids have been developed, especially in the past fifty years. In this section, only the methods that are frequently used for measuring rock salts will be described and discussed.

It is noted that the only commonly used method for measuring thermal diffusivity, the flash method, is often employed (together with independently-obtained specific heat values) to obtain thermal conductivity values. This method will be discussed in section 4.2.1. entitled "Measurement Methods for Thermal Conductivity".

### 4.2.1. Measurement Methods for Thermal Conductivity

#### 4.2.1.1. Absolute, Longitudinal Steady-State Heat Flow Method

In the absolute, longitudinal heat flow method, the experimental arrangement is so designed that the flow of heat is nearly entirely in the axial direction of a rod (or disk) specimen. The radial heat loss or gain of the specimen can either be prevented or minimized and evaluated. Under steady-state condition and assuming no radial heat loss or gain, the thermal conductivity is determined by the following expression which is from the one-dimensional Fourier-Biot heat-conduction equation

$$k = -\frac{q\Delta x}{A\Delta T} \tag{4.1}$$

where k is the average thermal conductivity corresponding to the average temperature  $\frac{1}{2}(T_1+T_2)$ ,  $\Delta T = T_2-T_1$ , q is the rate of heat flow, A is the cross-sectional area of the specimen, and  $\Delta x$  is the distance between points of temperature measurements for  $T_1$  and  $T_2$ .

In this method, the specimen used is in the form of a relatively long rod or disk (for poor conductors) so as to produce an appreciable temperature drop along the specimen for precise measurement. A source of heat at a constant temperature is supplied at one end of the rod (or one side of the disk). Heat flows axially through the rod (or disk) to the other end (or side) where a heat sink at a lower constant temperature is located. The radial heat loss or gain of the rod (or disk) should be negligible. In order to calculate the thermal conductivity from equation (4.1), it is necessary to measure the rate of heat flow into and/or out of the rod (or disk), the crosssectional area, the temperature of at least two points along the rod (or of two sides of the disk), and the distance between these points (or the thickness of the disk). This method has been used for most measurements below room temperature. General reviews of the lowtemperature measurements and experimental techniques have been presented by White [83,84]. For details of some of the useful low-temperature apparatus the reader may consult references [85-96].

While this method is inherently capable of high precision and accuracy, experience has shown that uncertainties of approximately one percent are attained at room temperature and lower. This figure rises to three percent at high temperatures.

### 4.2.1.2. Comparative, Longitudinal Steady-State Heat Flow Method

In this method a reference sample (or samples) of known thermal conductivity is placed in series with the unknown specimen with hopefully the same rate of heat flow through both the reference sample and the specimen. Under such ideal conditions, the thermal conductivity of the specimen is given by

$$k = k_{\rm r} \frac{A_{\rm r} \left(\Delta T / \Delta x\right)}{A \left(\Delta T / \Delta x\right)} r$$
(4.2)

where the subscript r designates the reference sample.

This method may be divided into two distinct groups: the "long-specimen" type [97–99] for measuring the thermal conductivity of good conductors, and the "short-specimen" type [36,101–104] for measuring poor conductors.

Comparative methods have the advantages of simple apparatus, easier specimen fabrication, and easier operation. Their disadvantages include additional measurement errors due to the required additional measurement of temperatures and thermocouple separations, difficulty in matched guarding against radial heat loss (or gain), and lower accuracy due to the additional uncertainty in the conductivity of the reference sample, the conductivity mismatch between specimen and reference sample, and due to the interfacial thermal contact resistance. These have been carefully analyzed by Laubitz [105] and Flynn [106]. The accuracy of the method is limited by the uncertainties in the reference material used. Normally this may be as high as two or three percent.

#### 4.2.1.3. Absolute, Radial Steady-State Heat Flow Method

This method uses a specimen in the form of a right circular cylinder with a coaxial central hole, which contains either a heater or a heat sink, depending on whether the dered heat flow direction is to be radially outward or inward. In the earlier experiments and also in many later designs [107-110], end guards are not employed. The effect of heat losses from the ends of the specimen is minimized by using a long specimen and monitoring the heater power within only a small section of the specimen away from the ends.

The guarded cylindrical method employing end guards at both ends of the specimen to prevent axial heat losses was developed by Powell [111] and first reported in 1939 for measurements on Armco iron at high temperatures. In this method the specimen is composed of stacked disks with a coaxial central hole containing either a heater or a heat sink. Temperatures are measured either by thermocouples or by an optical pyrometer.

The thermal conductivity is calculated from the expression

$$k = \frac{q \ln(r_2/r_1)}{2\pi l (T_1 - T_2)}$$
(4.3)

where l is the length of the central heater and  $T_1$  and  $T_2$  are temperatures measured at radii  $r_1$  and  $r_2$ , respectively.

For details of some of the useful apparatus employing the guarded cylindrical method, the reader may consult references [111-117]. The uncertainties in this method are normally those encountered in the absolute radial method.

#### 4.2.1.4. Flash Method

The flash method is a variant of the absolute, longitudinal transient heat flow method using a small thin disk specimen. In this method, a flash of thermal energy is supplied to one of the surfaces of the disk specimen within a time interval that is short compared with the time required for the resulting transient flow of heat to propagate through the specimen. This method was developed by Parker, Jenkins, Butler, and Abbott [118] and reported in 1961.

In use, a heat source such as flash tube or laser supplies a flash of energy to the front face of a thin disk specimen and the temperature as a function of time at the rear face is automatically recorded. The thermal diffusivity is obtained from the thickness of the specimen, l, and a specific time,  $t_{\frac{1}{2}}$ , at which the back face temperature reaches half its maximum value by the expression

$$\alpha = 1.37 \ l^2 / \pi^2 t_{1/2} \tag{4.4}$$

The thermal conductivity of the specimen is then calculated by the relation

$$k = \rho \alpha c_p \tag{4.5}$$

where k is the thermal conductivity,  $\rho$  is the density, and  $c_p$  is the specific heat at constant pressure.

Subsequent improvements on this method have been made [119,110] by the application of corrections for the finite pulse-time effect and the radiation-loss effect. Current capabilities exhibit an uncertainty of the order of five to ten percent depending on sample transparency and temperature level.

### 4.2.2. Measurement Methods for Thermal Expansion

#### 4.2.2.1. Push-Rod Dilatometers

The push-rod dilatometer method for measuring thermal expansion is experimentally simple, reliable, and easy to automate [121]. With this method, the expansion of the specimen is transferred out of the heated zone to an extensometer by means of rods (or tubes) of some stable material. The expansion of the specimen is given by

$$\frac{\Delta L}{L_0} = c_0 \quad \frac{(\Delta L)_a}{L_0} + c_1 \tag{4.6}$$

where  $(\Delta L)_a$  is the apparent change in length as calculated from the difference between the extensioneter readings at two different temperatures, and  $c_0$  and  $c_1$  are calibration constants for the system. If the reference rod is made the same length as the push rod and a second specimen placed on the base plate, the dilatometer will measure the difference between the specimens [122]. The difference, or differential expansion is given by

$$\frac{(\Delta L)_2}{L_0} - \frac{(\Delta L)_1}{L_0} = c_0 \quad \frac{(\Delta L)_a}{L_0} + c_1. \tag{4.7}$$

When used this way the dilatometer can have a very high sensitivity. This technique is also very useful for quality control measurements and for studying phase transitions.

One of the most common sources of error in using dilatometers is the measurement of temperature. All too often the temperature that is measured is not the temperature of the specimen. If a thermocouple is used, care must be taken to ensure that its junction and specimen are the same temperature; they can be at different temperatures even if in contact with each other. Another common source of error, especially for flexible materials or materials near their softening temperatures, is deformation under the load of the push rod. Special techniques such as increasing sample diameter, reducing push rod pressure, and using horizontal mounts must be used for these soft materials.

The uncertainty of this method depends on the quality of the push rod used and precision of construction. Results of two or three percent uncertainty may be achieved routinely.

#### 4.2.2.2. Interferometers

These methods are based on the interference of monochromic light reflected from two surfaces [123] that are separated by a specimen or by the combination of a specimen and a reference material. The general condition for interference is

$$2nL\cos\theta = N\lambda_{\nu} \tag{4.8}$$

where *n* is the index of refraction of the atmosphere between the surfaces, *L* the distance between the two surfaces,  $\theta$  the angle between the direction of the incident rays and the direction normal to the surfaces, *N* the order of interference, and  $\lambda_{\nu}$  the wavelength of the light in vacuum. Monochromatic light sources that may be used include cadmium, helium, mercury, and sodium low-pressure discharge lamp [124] and a stabilized He-Ne laser [125].

If slightly inclined surfaces are illuminated with collimated light and viewed at normal incidence ( $\theta$ =0 for all rays), fringes of equal inclination are observed. When the surfaces are flat the fringes will be straight; otherwise they are determined by the contour of the surfaces. This type of interference is used in the Fizeau interferenceter

[126]. If plane-parallel surfaces are illuminated with an extended source ( $\theta$  will vary), fringes of equal inclination are observed. This type of interference (concentric rings) is used in the Fabry-Perot interferometer [127].

When an interferometer is used to measure thermal expansion, the expansion of the specimen is given by

$$\frac{\Delta L}{L} = \frac{\lambda_{\nu} \quad \Delta N}{2nL \cos\theta} - \frac{\Delta n}{n}$$
(4.9)

where  $\Delta N$  is the number of the fringes that pass a fiducial mark and  $\Delta n$  is the change of refractive index. A useful approximation for the refractive index is

$$n = 1 + (n_r - 1) \frac{T_r P}{P_r T}$$
(4.10)

where  $n_r$  is the index at the reference temperature  $T_r$  and the reference pressure  $P_r$ . In vacuum or in sufficiently low-pressure atmosphere

$$\frac{\Delta L}{L} = \frac{\lambda_{\nu} \quad \Delta N}{2L \quad \cos\theta} \tag{4.11}$$

In a Fizeau interferometer (straight fringes) the fractional part of  $\Delta N$  is easily determined from measurements of the position of the fiducial mark between two fringes. In a Fabry-Perot interferometer (circular fringes) the fractional part, v is given by

$$\nu = 1 - p + \frac{nLd_{p}^{2}}{f^{2}\lambda_{\nu}}$$
(4.12)

where  $d_p$  is the diameter of the *p*th fringe (counted from the center of the concentric pattern) and *f* is the focal length of the lens that forms the pattern. If measurements are made on the second and fourth fringes, the fractional part is

$$\nu = \frac{3d_2^2 - d_4^2}{d_4^2 - d_2^2} \tag{4.13}$$

The number of fringes that move past a reference point during the expansion of a specimen can be counted by eye or automatically by photographic [128] or photoelectric [129] techniques. Another way of determining  $\Delta N$  is by finding the value of N at each temperature. This can be done by using at least three different wavelengths [124]. From eq (4.8) it can be seen that

$$(N_1+\nu_1)\lambda_1 = (N_2+\nu_2)\lambda_2 = (N_3+\nu_3)\lambda_3$$
 (4.14)

where  $N_1$ ,  $N_2$ , and  $N_3$  are the fringe integers and  $\nu_1$ ,  $\nu_2$ , and  $\nu_3$  are the fringe fractions for each of the three wavelengths. In the method of exact fractions a value is
guessed for  $N_1$  (~ $2nL/\lambda_1$ ) and using the measured value of  $\nu_1$  the values of  $(N_2+\nu_2)$  and  $(N_3+\nu_3)$  are calculated. This procedure is repeated with different values of  $N_1$  until the calculated values of  $\nu_2$  and  $\nu_3$  agree with their measured values. If N is known, then

$$\frac{\Delta L}{L} = \frac{\Delta N}{N} - \frac{\Delta n}{n} \cdot \tag{4.15}$$

The Fizeau interferometer can be used to measure either the absolute or relative expansion of a specimen. In the relative method a pedestal of one material fills most of space within a ring or cylinder of a second material. The pedestal is preferably made of a reference material. While the ring supports the optical flat, the interference is formed by reflections from the optical flat and the top surface of the pedestal. Since the reflecting surfaces are close together this method has three advantages: (1) the fringes are bright and well defined; (2) the change of the refractive index of the gas within the small space does not affect the measurements; and (3) longer specimens can be used with a corresponding increase in sensitivity. The thermal expansion is given by

$$\left[\frac{\Delta L}{L}\right]_{s} = \frac{\lambda_{\nu}\Delta N}{2nL_{s}} + \frac{L_{r}}{L_{s}}\left[\frac{\Delta L}{L}\right]_{r} + \frac{L_{s}-L_{r}}{L_{s}}\frac{\Delta n}{n} (4.16)$$

where the subscripts s and r refer to the specimen and reference materials. When  $L_r \sim L_s$  the last term can be ignored.

#### 4.2.2.3. X-Ray Methods

These methods are based on the diffraction of a collimated beam of monochromatic x-rays that is scattered by atoms in a crystal lattice. The Bragg law

$$\lambda = 2d(hkl)\sin\theta \qquad (4.17)$$

gives the condition for constructive reflection of the incident radiation. Here d is the separation of the lattice planes, h, k, and l are the Miller indices for the planes, and  $\theta$  is the angle measured between the direction of the incident or reflected beam and the planes. Except for a small correction due to refraction, the measurement of expansion is independent of wavelength such that

$$\frac{\Delta d(hkl)}{d(hkl)} = -\cos\theta\Delta \theta = \frac{\sin\theta_1 - \sin\theta_2}{\sin\theta_2} (4.18)$$

where  $\theta_1$  and  $\theta_2$  are the angles of incidence of the beam with the crystal plane at temperatures  $T_1$  and  $T_2$ , respectively.

The thermal expansion of crystalline materials can be accurately measured with x-ray cameras and diffractometers under conditions that preclude the use of any other method, as when the specimens are very small, weak, and/or irregular in shape. These methods are also unique in that they can easily be used to determine the principal coefficients of thermal expansion of anisotropic crystals and permit direct observation of phase changes. There is a further advantage in that measurements with x-rays do not include effects that are observed in measurements on bulk specimens. The problems associated with heating the specimen and accurately measuring its temperature in both x-ray cameras and diffractometers are discussed in several articles [131-133].

Unique x-ray techniques exist for special situations. In particular, the use of the Bond technique for single crystals [134] has resulted in a sensitivity of  $10^{-7}$  in measurements of  $\Delta a/a$  [135]. In this technique the specimen is rotated between equivalent diffracting orientations on either side of the incident beam. The value of  $\theta$  thus obtained is unaffected by any specimen eccentricity, absorption, and zero errors, and errors due to specimen tilt and beam axial divergence are minimized.

The inherent accuracy of this technique is extremely high for well characterized and stable materials.

#### 4.3. Thermal Conductivity

The thermal conductivity of different samples of rock salt can be different by four orders of magnitude, depending on the temperature region. This variation is dependent upon the degree of lattice imperfection, the various treatments before the measurement, and the kind and the amount of impurities present in the sample.

Figure 4.1 shows several types of thermal conductive behavior of rock salts with different treatments. Group 1 represents the thermal conductivity of high-purity rock salt [1-8,16]. Based on the data in this group, recommended values for pure rock salt were generated for temperatures above 100 K and are tabulated in table 4.1. Those tabulated values below 100 K are merely typical values. The recommended values are considered accurate to within ±5%. Rock salts which were annealed at different temperatures are represented by group 2 [9,10]. The thermal conductivity of samples with different amounts of Na [2] and NaOH [7,8] are shown in group 3 and group 4, respectively. Data for rock salts which were melted, treated with Cl<sub>2</sub>, and recrystallized are also shown, group 5 [7]. Finally, data for rock salts with unknown impurities are represented by group 6 [5,11].

It should be noted that at temperatures below 100 K, the thermal conductivity of rock salt is inversely proportional to the quantity of the added impurity. However, at temperatures higher than 100 K, the thermal conductivity seems to be insensitive to the impurity content.



Figure 4.1. Thermal Conductivity of Rock Salt.

remperatore,			,
Т	k	T	k
0.4	0.95	25	191
0.5	1.78	30	130
0.6	3.13	40	75.0
0.7	4.97	50	54.0
0.8	7.40	75	34.9
0.9	10.0	100	24.3
1	14.0	150	15.0
2	99.3	200	10.9
3	270	250	8.24
4	443	293	6.65
5	595	300	6.57
6	735	400	4.80
7	820	500	3.67
8	880	600	2.98
9	870	700	2.47
10	836	800	2.08
15	502	900	1.85
20	306	1000	1.67

TABLE 4.1. RECOMMENDED VALUES OF THE THERMAL CONDUCTIVITY OF ROCK SALT\*

\*Those below 100 K are typical values.

There are a number of additional references where the thermal conductivity of rock salt, either pure or impure, is reported [12–15, 17–43, 45, 136–140, 148–152].

## 4.4. Thermal Diffusivity

There are very few experimental data available for the thermal diffusivity of rock salt. Consequently, the thermal diffusivity values are derived from the recommended values of the thermal conductivity, the specific heat, and the density computed from the recommended thermal expansion values.

The equation used to calculate the thermal diffusivity can be expressed as

$$\alpha = \frac{k}{c_p \rho} \tag{4.19}$$

where  $\alpha$  is the thermal diffusivity, k is the thermal conductivity,  $c_p$  is the specific heat at constant pressure, and  $\rho$  is the density. The density at temperature T can be calculated from the equation [44]

$$\rho = \rho_0 \left( 1 + 3 \ \frac{\Delta L}{L_0} \right)^{-1} \tag{4.20}$$

where  $\rho_0$  (=2.16 g/cm<sup>3</sup>) is the density of rock salt at room temperature (293 K), and  $\Delta L = L-L_0$ , L and  $L_0$ being the lengths at temperature T and at room temperature, respectively.

The thermal diffusivity values so calculated are plotted in figure 4.2 and tabulated in table 4.2. The values in the temperature region above 100 K can be considered with the uncertainty of  $\pm 5\%$ . Some experimental data for the thermal diffusivity of high-purity rock salt [33,43] are also exhibited in the figure for comparison. It can be seen that the recommended values agree with the experimental data quite well. Other references on the thermal diffusivity of rock salt are [46,47].

#### 4.5. Thermal Linear Expansion

The quantity reported here for the thermal linear expansion of rock salt is the percent expansion, which is defined as  $\Delta L/L_0(\%)$ , where  $\Delta L = L-L_0$ , and L and  $L_0$  are the lengths at temperature T and at room temperature (293 K), respectively. In figure 4.3 the recommended values of the thermal linear expansion and the selected experimental data sets which were used to generate the recommended values are shown. These recommended values are considered with the uncertainty of  $\pm 5\%$ . The recommended values are also tabulated in table 4.3, and can be represented approximately by the following equations:

$$\Delta L/L_0 = -1.064 + 3.025 \times 10^{-3}T + 1.471 \times 10^{-6}T^2 - 8.559 \times 10^{-11}T^3 (293 \le T \le 600 \text{ K})$$
(4.21)

$$\Delta L/L_0 = -1.161 + 4.030 \times 10^{-3}T \tag{4.22}$$

$$- 4.554 \times 10^{-7} T^2 + 1.285 \times 10^{-9} T^3$$
(4.22)  
(600  $T < 1074$  K)

and

$$\Delta L/L_0 = -8.5462 + 0.012169 T \quad (1074 \text{ K} \le T) \quad (4.23)$$

f romport		ar presente,	/, 10 m 0
	<u>Solid</u>	So	lid
Т	α	Т	α
10	301	293	0.0353
15	136	300	0.0349
20	36.7	400	0.0249
25	15.9	500	0.0186
50	0.952	600	0.0149
75	0.356	700	0.0123
100	0.192	800	0.0103
150	0.0955	900	0.00915
200	0.0628	1000	0.00827
250	0.0459		

TABLE 4.2. RECOMMENDED VALUES OF THE THERMAL DIFFUSIVITY OF ROCK SALT\* [Temperature, T,K; Thermal Diffusivity, 10<sup>-4</sup>m<sup>2</sup>s<sup>-1</sup>]

\*Those below 100 K are typical values.

Theoretical calculation of the thermal expansion of rock salt in the temperature range 0-300 K was conducted by White [69] using the Grüneisen relation; his results agreed with the experimental data.

Strictly speaking, the concept of thermal linear expansion does not apply to liquids and/or materials in the molten state. However, for ease of presentation and ease of comparison with room temperature dimensions, the quantity  $\Delta L/L_0$ , instead of the volumetric expansion, is presented also for the molten state. (For practical purposes, the volumetric expansion,  $\Delta V/V_0$ , can be equated to  $3 \Delta L/L_0$ ). These values are calculated from volumetric thermal expansion data which were obtained from density measurements.

The theoretical calculation of the thermal expansion of molten rock salt was carried by Vilcu et al. [57,58] and Lu [56] using Significant-Structure theory of liquid. Their results agreed well with the experimental data.

Additional experimental data on the thermal linear expansion are given in references [28,41,48–50, 61–82,100,141–147].

## 4.6. Effect of Nuclear Irradiation on Thermophysical Properties

Experimental data on the thermophysical properties of rock salt which has been irradiated are lacking. Only three data sets on the thermal conductivity were reported [10], and no information on the thermal linear expansion and the thermal diffusivity could be found in the literature. Therefore, no recommended values for these thermophysical properties are generated. However, the available thermal conductivity data are plotted in figure 4.4 and tabulated in table 4.4. The recommended and typical curves for high-purity rock salt without nuclear irradiation (from section 4.2) are reproduced in figure 4.4 for comparison. All three sets are for specimens (Optovac sodium chloride) with approximate OH<sup>-1</sup> concentration of 3 ppm and  $\gamma_{r}$  irradiated, with  $3.8 \times 10^{16}$ F centers/cm<sup>3</sup> (curve 1), 5.6  $\times 10^{17}$ F centers/cm<sup>3</sup> (curve 2), and 7.6  $\times 10^{17}$ F centers/cm<sup>3</sup> (curve 3). It is seen from figure 4.4 that irradiation drastically reduced the thermal conductivity of rock salt at cryogenic temperatures. No data are available at or above room temperature.





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[Temperature,	T,K; Thermal	Linear Expansi	on, ∆L/L <sub>0</sub> ,%]
Т	∆l/l <sub>0</sub>	Т	$\Delta L/L_0$
5	-0.772	600	1.371
10	-0.772	700	1.878
15	-0.772	800	2.430
20	-0.771	900	3.034
25	-0.771	1000	3.699
50	-0.759	1074	4.528
75	-0.722	1100	4.840
100	-0.666	1200	6.057
150	-0.521	1300	7.274
200	-0.352	1400	8.490
250	-0.168	1500	9.707
293	0.000	1600	10.924
400	0.448	1700	12.141
500	0.896	1750	12,750

TABLE 4.3. RECOMMENDED VALUES OF THE THERMAL LINEAR EXPANSION OF ROCK SALT



Figure 4.3. Thermal Linear Expansion of Rock Salt.

53.3.1



Figure 4.4. Thermal Conductivity of Irradiated Rock Salt.

# TABLE 4.4. EXPERIMENTAL DATA ON THE THERMAL CONDUCTIVITY OF ROCK SALT AFTER NUCLEAR IRRADIATION

[Temperature, T,K; Thermal Conductivity, k, Wm<sup>-1</sup>K<sup>-1</sup>]

Curv	ve 1	Curv	7e 2	Cur	ve 3
$(3.8 \times 10^{16} \text{F})$	centers/cm <sup>3</sup> )	$(5.6 \times 10^{17} \text{ F})$	centers/cm <sup>3</sup> )	$(7.6 \times 10^{17} \text{F})$	centers/cm <sup>3</sup> )
Т	k	T	k	Т	k
1.26	5.19	1.33	2.43	1.26	2.10
1.26*	5.89	1.47*	2.81	1.35*	2.70
1.35*	6.33	1.53*	3.13	1.44*	3.17
1.35*	7.18	1.58*	3.88	1.63*	4.24
1.55*	9.95	1.70	4.74	1.84*	5.65
1.55	11.30	1.95*	6.33	2.05	7.02
1.75*	14.00	2.13*	7.87	2.40*	10.40
1.82*	15.90	2.41	10.70	2.57*	11.00
1.92*	18.40	2.68*	13.10	2.91*	11.60
2.02*	20.50	3.04*	15.70	3.41	14.70
2.09*	23.70	3.38*	18.40	3.41*	18.00
2.29	26.40	3.69*	20.90	3.79*	16.70
2.41*	30.00	4.18*	24.60	4.13*	16.40
2.73*	33.40	4.64	27.40	3.72*	20.70
2.73*	38.00	5.16*	31.70	4.28*	18.30
3.03*	44.70	5.44*	35.40	4.51*	20.00
3.37*	48.90	6.05*	40.90	5.01*	23.10
3.56	55.50	6.73*	46.40	5.57	26.20
3.95*	64.20	7.35	51.70	6.08*	30.90
4.24*	72.80	7.75*	57.60	6.87*	37.00
4.55*	78.30	8.47*	62.00	7.77*	45.10
5.06*	90.50	8.77*	66.60	8.94	54.00
5.53*	103.00	9.09*	71.60	9.76*	63.60
6.15*	115.00	9.75*	77.00	11.60*	81.90
6.84	130.00	11.00	92.30	12.90*	92.90
7.74*	148.00	12.50*	103.00	14.40	105.00
8.02*	165.00	13.90*	115.00	15.90*	113.00
9.07*	180.00	15.40*	128.00	17.70*	115.00
9.57*	204.00	17.20	133.00	19.30	118.00
10.40	220.00	18.40	133.00	21.50*	111.00
11.60*	241.00	20.10*	130.00	25.60	96.40
12.90	254.00	21.60*	128.00	27.50*	91.40
14.60	254.00	23.20	119.00	32.80	68.50
20.10	212.00	31.40*	87.60		
26.30*	151.00	33.10	77.20		
36.80	77.20	48.90*	46.50		
43.20*	56.80	63.80	36.80		
56.40*	37.50				
61.60	31.90				

\*Not plotted in the figure.

## 4.7. References

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## Symbols and Units

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## **Conversion Factors**

Symbol	Name	Unit	Thermal conductivity		
A	Cross-sectional area of the specimen	m <sup>2</sup>	thermal conductivity		
Α <sub>r</sub>	Cross-sectional area of the reference		To convert from	to	Multiply by
	sample	m²	$W m^{-1} K^{-1}$	Bturn h-1 ft-1 F-1	0 5777908
Co,C1	Calibration constants	dimensionless			0.5111900
c <sub>p</sub>	Specific heat at constant pressure	J kg K <sup>−1</sup>	W m <sup>-1</sup> K <sup>-1</sup>	callT s <sup>-1</sup> cm <sup>-1</sup> C <sup>-1</sup>	2.38846 X 10 <sup>-3</sup>
d	Separation of the lattice planes (eq 4.17)	m	Thermal diffusivity		
$d_p$	Diameter of the <i>p</i> th fringe	m	To convert from	to	Multiply by
¢*	Focal length of the lens	m	m <sup>2</sup> s <sup>-1</sup>	$cm^2 s^{-1}$	104
h,k,l	Miller indices	dimensionless	$m^2 s^{-1}$	$ft^2 s^{-1}$	10 7639
;	Thermal conductivity	W m <sup>-1</sup> K <sup>-1</sup>	$m^2 s^{-1}$	$m^2 h^{-1}$	3600
r	Thermal conductivity of the reference				3000
	sample	W m <sup>-1</sup> K <sup>-1</sup>			
L	Length at temperature T	m			
s	Length of the specimen	m			
L <sub>r</sub>	Length of the reference sample	m			
Lo	Length at room temperature (293 K)	m			
$\Delta L$	$\Delta L = L - L_0$	m			
$\Delta L/L_0$	Thermal linear expansion	%			
	Length of the central heater	m			
V	Order of interference	dimensionless			
$N_1, N_2, N_3$	Fringe integers	dimensionless			
$\Delta N$	Number of fringes that pass a fiducial				
	mark	dimensionless			
ı	Refractive index	dimensionless			
$\Delta n$	Change of refractive index	dimensionless			
D	Pressure	atm (use Pa)			
7	Rate of heat flow	watt			
1,r <sub>2</sub>	Radii	m			
Г	Temperature	K			
$T_{1}, T_{2}$	Temperatures	K			
$\Delta T$	$\Delta T = T_2 - T_1$	K			
V	Volume at temperature T	m <sup>3</sup>			
V <sub>0</sub>	Volume at room temperature (293 K)	m <sup>3</sup>			
$\Delta V$	$\Delta V = V - V_0$	m <sup>3</sup>			
$\Delta V/V_0$	Thermal volumetric expansion	%			
$\Delta x$	Distance difference	m			
Greek					
symbols					
x	Thermal diffusivity	m <sup>2</sup> s <sup>-1</sup>			
9	Angle	degree			
	Wavelength	m			
v	Wavelength of light in vacuum	m			
v	The fractional part in Fabry-Perot				
	interferometer	dimensionless			
$\nu_1, \nu_2, \nu_3$	Fringe integers	dimensionless			
0	Density	ka m-3			
0	D is in the second seco				
$P_0$	Density at room temperature (293 K)	kg m <sup>-3</sup>			

# Chapter 5 Optical Properties H. H. Li\*

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#### 5.1. Introduction

Optical properties of a material are of fundamental importance to the description of interactions between electromagnetic radiation and the material. They relate both the absorptive and dispersive characteristics of the material and have a wide range of applications in science and technology. In this chapter, the available information on the refractive index and absorption coefficient of rock salt are reviewed and discussed. For the refractive index, the available data are adequate for data evaluation and the generation of recommended values. In the case of the absorption coefficient, the situation is different in that this property is influenced by a number of factors, notably the thermal history of the crystal, the irradiation history, the impurity contents, the physical environment, etc. As a consequence, no recommended values could be generated. Only qualitative discussions and a few typical graphical presentations are given.

## 5.2. Measurement Methods for Optical Properties

The response of a nonmagnetic solid with isotropic or cubic symmetry to incident electromagnetic radiation can be generally described in terms of two optical constants, which are related to each other through dispersion relations.

These two optical constants can consist of either (1) the refractive index, n, and the extinction coefficient, k, or (2)  $\epsilon_1$  and  $\epsilon_2$  which are, respectively, the real and imaginary part of the complex dielectric constant  $\epsilon$ . These two pairs of constants are related as follows:

$$\epsilon(\lambda) = \epsilon_1(\lambda) + i\epsilon_2(\lambda) = [n^2(\lambda) - k^2(\lambda)] + 2in(\lambda)k(\lambda)$$
(5.1)

In the transparent wavelength region where the absorption can be neglected, the refractive index of the material can be directly determined in a number of ways. The basic principle of such measurements is rather simple. It makes use of the dispersive nature of the material and the wavefront reconstruction of the electromagnetic radiation after the radiation has passed through the dispersive medium. Depending on the shape of the dispersive element and the environmental medium surrounding it the reconstructed wavefront is detected through angular displacement, interference order advanced, distant moved or the refractive index of embedding medium changed. The following table summarizes these methods.

Shape of Crystal	Quantity to be Observed	Principle
Prism	Deviation angle	Snell's Law
Plane parallel plate	Interference order	Interference order depends on thickness
Scratch on plate	Apparent depth	Optical path increase in the plate
Lens	Focal length	Lens maker formula
Irregular	Refractive index of embedding medium	Contrast disappears when crystal and medium have same refractive index

In general, refractive index obtained by prism method is reported to the fifth or sixth decimal place, interference method gives three to four decimal places, the other methods yield no more than three decimal places. For a comprehensive and concise review of these methods, the reader is referred to the text in refs. [74 and 75].

For a crystal of sufficient thickness so that the reflection from the rear surface can be neglected, the absorption coefficient can be determined by using a simple exponential law:

$$T_{\infty} = (1 - R_{\infty})^2 e^{-\alpha d},$$
 (5.2)

where  $R_{\infty}$  and  $T_{\infty}$  are, respectively, the reflectivity and transmission at normal incidence,  $\alpha$  the absorption coefficient, and *d* the thickness of the sample. However, the sample to be measured is not always thick and the reflection from the rear surface is not always negligible. The observed reflectance and transmission of a transparent plate is the resultant of multiple reflections and transmission at the boundary surfaces. In terms of  $T_{\infty}$  and  $R_{\infty}$ , the observed transmission and reflectivity of a plate sample (not a thin film) can be expressed as:

$$T = \frac{\left[ (1 - R_{\infty})^2 + 4R_{\infty} \sin^2 \psi \right] e^{-\alpha d}}{1 \quad R_{\infty}^2 e^{-2\alpha d}}$$
(5.3)

and

$$R = \frac{R_{\infty}(1 - e^{-\alpha d})}{1 - R_{\infty}^2 e^{-\alpha d}}$$
(5.4)

where

$$\psi = \tan^{-1} \frac{2k}{n^2 + k^2 - 1},$$

$$k = \frac{\lambda \alpha}{4\pi},$$

$$R = \frac{(n - n')^2 + k^2}{(n + n')^2 + k^2},$$

$$n' - \text{refractive index of surrounding medium,}$$

 $n' \simeq 1$  for air or vacuum.

It appears that if we know  $R_{\infty}$  and either *n* or *k*, the remaining one can be calculated by this relation. But this is only limited to the transparent region where direct measurement of n can be made. It is obvious that the key parameters *T* and *R* are usually difficult to measure accurately, because of influencing surface conditions, such as flatness, aging, oxide layers, absorbed gas, etc. However, this method is self contained at a given wavelength.

Precise determination for small absorption coefficients, in the order of  $10^{-3}$  or lower, was considered impossible until the laser source became available. As the bulk absorption becomes smaller than surface losses measuring the former requires amplification of the absorption effect, which, in turn, requires high-level energy input to the sample. The two commonly used methods are the laser calorimeter [76] and the differential technique [77].

In the laser calorimeter, the absorbed energy is measured in the form of heat. It can be shown that the bulk and surface loss, i.e., the total absorption, is related to the absorbed energy, *Ea*, by

$$\alpha L + 2\sigma = \frac{E_a}{E_T} \left[ \frac{2n}{1+n^2} \right]$$
 (5.5)

provided  $\alpha L < 1$ , where L is the sample length through which a laser beam passes, and  $\sigma$  the surface loss.  $E_a$  can be calculated using the specific heat, the mass of the sample and the measured temperature rise. The transmitted energy can be determined using a black body and the temperature rise. In order to separate the bulk and surface absorptions, the total absorption of a series of samples of different thickness, cut from the same piece of material and polished in the same way must be measured. A plot of total absorption versus sample thickness will give a straight line with slope  $\alpha$  and intercept  $2\sigma$ . Although this method yields very accurate results and is used to measure absorptions as low as 10<sup>-5</sup> cm<sup>-1</sup>, it covers only a limited wavelength range. For a wider wavelength range measurement, the differential technique is used.

In the differential technique, a dual-beam spectrometer is used to compare the transmissions of a thick sample  $(T_s \text{ and } d_s)$  and a reference sample  $(T_r \text{ and } d_r)$ . An optical wedge is added to the reference beam and its transverse position is so adjusted as to balance the transmitted intensity of the sample beam. The transmission of the wedge,  $T_w$ , is then measured. The relation of the three measured transmissions is therefore

$$T_{\rm r} \times T_{\rm w} = T_{\rm s} \tag{5.6}$$

hence, by using eq (5.3)

$$T_{\rm w} = e^{-\alpha \Delta d} \quad \left( \frac{1 - R^2 e^{-2\alpha d_{\rm r}}}{1 - R^2 e^{-2\alpha d_{\rm s}}} \right) \tag{5.7}$$

where  $\Delta d = d_s - d_r$ , and

$$R = \left(\frac{n-1}{n+1}\right)^2 \tag{5.8}$$

The accuracy of the method depends strongly on the accuracy of the values for refractive index and transmission. While the former can be determined with high accuracy, the accuracy of the latter parameter depends on the instrument utilized. A  $\pm 1\%$  uncertainty is generally expected. This imposes a limit, the order of  $1 \times 10^{-3}$  cm<sup>-1</sup>, to the lowest value for absorption coefficient to be measured.

Beyond the transparent region in the high absorption region where neither n and k is accessible, one has to rely on the reflection spectrum from which the optical constants can be derived by the Kramers-Kronig analysis [78] or by the multiple-oscillator fit based on the Lorentz theory [79].

The Kramers-Kronig relations are derived from the dispersion relation in that the phase angle  $\theta(\omega)$  of the complex reflectivity  $\overline{R}(\omega)$  is determined based on the observed reflection spectrum:

$$\overline{R}(\omega) = R(\omega) e^{i\theta(\omega)}, \qquad (5.9)$$

$$\theta(\omega) = \frac{\omega}{\pi} P \int_0^\infty \frac{\left[\ln R(\omega') - \ln R(\omega)\right]}{\omega^2 - \omega'^2} d\omega' \quad (5.10)$$

where  $\omega$  is the frequency of radiation and P is the principal value of the Cauchy integral. Based on the amplitude,  $R(\omega)$ , and phase angle of the reflectivity, the refractive index and absorption index can be calculated according to the following

$$n(\omega) = \frac{1 - R(\omega)}{1 + R(\omega) - 2\sqrt{R(\omega)}\cos\theta(\omega)}$$
(5.11)

and

$$k(\omega) = \frac{2\sqrt{R(\omega)} \sin\theta(\omega)}{1 + R(\omega) - 2\sqrt{R(\omega)}\cos\theta(\omega)}$$
(5.12)

In principle, the calculation of  $\theta$  requires a complete reflection spectrum with frequency ranging from zero to infinity. In practice, R is measured only for a limited spectral range. In order to use eq (5.10), extrapolation of  $R(\omega)$  beyond the measured range must be made based on certain approximations. Consequently, errors are introduced in  $\theta$  and hence in n and k. It is clear that the accuracies of optical constants derived from the reflection spectra depend strongly on the accurate determination of reflectivity. Unfortunately, measurements on the latter are inherently inaccurate because of experimental difficulties. Typical errors reported for reflectivity observations are one to ten percent. This will reflect an error of about one to ten percent in the calculated optical constants depending on the stability of the light source and the quality of reference mirror used.

In the Lorentz theory, the refractive index and absorption index are related to the oscillator frequencies,  $\omega_i$ , the oscillator strengths,  $s_i$ , and the damping factors,  $\gamma_{i}^{i}$ , by the expressions:

$$n^{2} - k^{2} = \epsilon_{\infty} + \sum_{i} \frac{S_{i} [1 - (\omega/\omega_{i})^{2}]}{[1 - (\omega/\omega_{i})^{2}]^{2} + \gamma_{i}^{2} (\omega/\omega_{i})^{2}}$$
(5.13)

$$2nk = \sum_{i} \frac{S_{i} \gamma_{i} (\omega/\omega_{i})}{[1 - (\omega/\omega_{i}^{1})]^{2}]^{2} + \gamma_{i}^{2} (\omega/\omega_{i})^{2}} (5.14)$$

where  $\epsilon_{\infty}$  is the optical dielectric constant. The resulting n and k have to satisfy the observed reflectivity by the relation

$$R(\omega) = \left| \begin{array}{c} n(\omega) - 1 + ik(\omega) \\ n(\omega) + 1 + ik(\omega) \end{array} \right|^2$$
(5.15)

It is clear that this approach requires knowledge of the oscillator frequencies which in general is not complete. This leaves no choice but to use only the observed predominant ones. Nevertheless, this method, similar to the Kramers-Kronig analysis, yields good approximations to the properties under consideration.

## 5.3. Refractive Index and Absorption Coefficient

Pure rock salt is uniformly transparent from  $0.2 \,\mu$ m in the ultraviolet to  $12 \,\mu$ m in the infrared. In the region of 15  $\,\mu$ m the absorption increases rapidly. Rock salt in moderately thin pieces may be expected to transmit several percent of the light up to wavelengths as long as  $26.0 \ \mu$ m. However, a plate 1 cm in thickness is completely opaque to radiation of wavelengths greater than 20  $\mu$ m.

Rock salt has long been a favorite material for infrared spectroscopy. It polishes easily and, although hygroscopic, can be protected by evaporated plastic coatings. It shows excellent dispersion over its entire transmission range. It has been difficult, however, to obtain natural rock salt crystals of sufficient size and purity for making optical components. As crystal-growing techniques advanced, synthetic sodium chloride crystals have been grown up to 11.3 kg in weight commercially, making this material readily available for large optical parts and stimulating the design and construction of infrared instruments.

Measurement of the refractive index of sodium chloride dates back to 1871, when Stefan [1] determined the refractive indices of a rock salt prism for solar lines B, D, and F. Since then, a large amount of data in the transparent region have been contributed by a number of investigators, among which are Martens [2], Paschen [3], and Langley [4,5]. They used either the deviation method or interferometry in their experiments. It was not until 1929 that measurements were carried out beyond the transparent region in the infrared. Kellner [6] determined refractive indices of NaCl in the 23-35 µm region, based on information on transmission and reflection of thin specimens. In the vacuum ultraviolet region, Rossler and Walker [7] observed the region from 0.0476 to 0.2480 µm, and Miyata and Tomiki [8,9] studied from 0.10 to  $0.25 \,\mu$  m. Additional measurements on the refractive index were reported in ref. [10-37]. Data on the refractive index are now available from 0.0476 µm up to 300 µm and at 2000 µm.

A collective plot of the available data is shown in figure 5.1., where the reference number for the data source is designated by the number in a circle. In the interest of visual clarity not all the available data are plotted in the figure. Furthermore, most of the UV and IR data were determined from the analysis of the reflection spectra. It was found that refractive index data in the transparent regions for colorless natural rock salt are in close agreement with those for synthetic crystal with discrepancies occurring at the fourth decimal place.

Beyond the transparent regions, in the vacuum ultraviolet and infrared regions, investigations were mainly concerned with the characteristic absorptions. Predominant absorption peaks in the ultraviolet region were measured by Hilsch and Pohl [38], Schneider and O'Bryan [39] and by Ramachandran [40]. Fundamental infrared absorption peaks were reported by Lowndes and Martin [36], and Karheuser [41]. Observation of the



Figure 5.1. Experimental Refractive Index of Rock Salt

refractive index carried out in the millimeter wavelength region was used to determine the static dielectric constant of the material. Dianov and Irisova [33] determined the refractive index at a wavelength of 2 millimeters. The static dielectric constant, using the relation  $\epsilon_0 = n^2$ , is in close agreement with that obtained by other methods. The selected absorption peak values taken from these works are given below:

Ultraviolet absorption peaks occur at:

$0.050 \mu{\rm m},$
$0.100 \ \mu \mathrm{m},$
$0.128 \ \mu m$ ,
$0.158 \mu{ m m}$

Infrared absorption peaks occur at:

40.50 μm	(LO mode),
60.98 µm	(TO mode),
$120.34 \mu{\rm m},$	

And the dielectric constants are:

high frequency dielectric constant  $\epsilon_{\infty} = 2.33$ , static dielectric constant  $\epsilon_0 = 5.99$ .

The temperature coefficient dn/dT is available over a large part of the transparent region of NaCl. Notable are those measured by Micheli [42] (from 0.202 to 0.643  $\mu$ m), Liebreich [43,44] (from 0.656 to 8.85  $\mu$ m), and Kolosovskii and Ustimenko [45] (for 10.6  $\mu$ m). These data are plotted in figure 5.2.

Li [46], in 1976, reduced the then available experimental data on the refractive index and dn/dT to a common temperature of 293 K and after careful critical evaluation and analysis adopted a formula, eq (5.16), for the calculation of dn/dT for the temperature range 293 ± 50 K

$$2n \frac{dn}{dT} = -11.91(n^2 - 1) - 0.50 + \frac{6.118 \lambda^4}{(\lambda^2 - 0.02496)^2} + \frac{199.36 \lambda^4}{(\lambda^2 - 3718.56)^2},$$
 (5.16)

where dn/dT is in units of  $10^{-5}$  K<sup>-1</sup> and  $\lambda$  is in  $\mu$ m.

Similarly a Sellmeier type dispersion equation, (eq 5.17), was used to evaluate refractive index at 293 K in the wavelength region 0.20-30.0  $\mu$ m:

$$n^{2} = 1.00055 + \frac{0.19800 \lambda^{2}}{\lambda^{2} - (0.050)^{2}} + \frac{0.48398 \lambda^{2}}{\lambda^{2} - (0.100)^{2}} + \frac{0.38696 \lambda^{2}}{\lambda^{2} - (0.128)^{2}} + \frac{0.25998 \lambda^{2}}{\lambda^{2} - (0.158)^{2}} + \frac{0.08796 \lambda^{2}}{\lambda^{2} - (40.50)^{2}} + \frac{3.17064 \lambda^{2}}{\lambda^{2} - (60.98)^{2}} + \frac{0.30038 \lambda^{2}}{\lambda^{2} - (120.34)^{2}}, \quad (5.17)$$

where  $\lambda$  is in units of  $\mu$ m.

Recommended values calculated from eqs 5.16 and 5.17 are shown in figures 5.2 and 5.3 and are tabulated in table 5.1. It should be noted that values tabulated in table 5.1 are for a pure crystal. Unfortunately, there are no systematic measurements on the refractive index of impure and defective crystal of NaCl reported. However, the refractive indices of an impure crystal are likely to be higher than the values in table 5.1.

Investigations of the absorption coefficient are generally classified into three broad wavelength regions: the ultraviolet, the infrared, and the transparent region. In the ultraviolet region, the investigations are concerned with the exciton states in the crystal and the determination of the Urbach-rule parameters. Roessler and Walker [7] determined the absorption index of NaCl in the spectral range from 0.047 to 0.248  $\mu$ m by a Kramers-Kronig analysis of the reflectance spectrum. The surfaces of the specimen examined were near perfect as evidenced by the strong temperature dependence of reflectance in the exciton region and the appearance of spin-orbit split doublets. Kobayashi and Tomiki [47] studied the effects of impurities on the absorption coefficient and found significant differences between crystals in the spectral range from 0.171 to  $0.231 \,\mu\text{m}$ . The main sources of such discrepancies were the presence of hydroxyl ions and dislocations in the crystals. The inclusion of the OH<sup>-</sup> is also reflected by the presence of an absorption band at 2.8  $\mu$ m in the near infrared region. Miyata and Tomiki [8,9] and Tomiki, Miyata and Tsukamoto [48] studied the absorption of NaCl in the region of 0.156 to 0.205  $\mu$ m for the purpose of determining the Urbach-rule parameters and finding the features characteristic of the intrinsic tail. Systematic observation and analysis gave the empirical relations of the parameters:

$$E_0 = 8.025 \text{ eV}$$

$$A_0 = 1.2 \times 10^{10} \text{ cm}^{-1}$$

$$\overline{h}\omega = 0.0095 \text{ eV}$$

$$\sigma_{s_0} = 0.741$$

and led to the expression of the absorption coefficient for the intrinsic tail as:

A(E,1) = A<sub>0</sub>exp [ 
$$-\sigma_s$$
 (1) (E<sub>0</sub>-E)/k1] (5.18)  
where  $\sigma_s$  (T) =  $\sigma_{s_0} \frac{2 kT}{h\omega} tan h \frac{h\omega}{2 kT}$ .

Measurements of an absorption coefficient for the infrared region were made for the purpose of studying the optically active lattice vibrations. On the short wavelength side of the reststrahlen band, multiphonon



WAVELENGTH,  $\lambda$ ,  $\mu$ m

Figure 5.2. Temperature Coefficient of Refractive Index of Rock Salt



Figure 5.3. Recommended Refractive Index of Rock Salt

λ μm	n	dn/dT 10 <sup>-5</sup> K <sup>-1</sup>	λ µm	n	dn/dT 10 <sup>-5</sup> K <sup>-1</sup>
0.200 0.204 0.208 0.212 0.216	1.789 1.770 1.754 1.739 1.726	4.6 3.4 2.5 1.8 1.2	3.500 4.000 4.500 5.000 6.000	1.5230 1.5217 1.5203 1.5188 1.5153	-3.3 -3.3 -3.2 -3.2 -3.2 -3.2
0.220	1.714	0.7	$\begin{array}{c} 7.000 \\ 8.000 \\ 9.000 \\ 10.000 \\ 10.200 \end{array}$	1.5112	-3.1
0.224	1.704	0.3		1.5064	-3.1
0.228	1.694	-0.0		1.5009	-3.0
0.232	1.686	-0.3		1.4947	-2.9
0.236	1.678	-0.6		1.4934	-2.9
0.240	1.671	-0.8	10.400	1.4920	-2.9
0.244	1.664	-1.0	10.600	1.4906	-2.9
0.248	1.658	-1.2	10.800	1.4892	-2.9
0.252	1.6525	-1.3	11.000	1.4877	-2.8
0.258	1.6447	-1.5	11.200	1.4862	-2.8
0.264	1.6376	-1.7	$ \begin{array}{r} 12.000\\ 13.000\\ 14.000\\ 15.000\\ 16.000\\ \end{array} $	1.4800	-2.7
0.270	1.6312	-1.8		1.4713	-2.6
0.276	1.6254	-2.0		1.4618	-2.5
0.282	1.6201	-2.1		1.451	-2.3
0.290	1.6137	-2.2		1.439	-2.1
0.300	1.6066	-2.3	$17.000 \\ 18.000 \\ 19.000 \\ 20.000 \\ 22.000$	1.427	-1.8
0.320	1.5950	-2.5		1.413	-1.5
0.340	1.5859	-2.7		1.398	-1.2
0.360	1.5785	-2.8		1.382	-0.8
0.380	1.5724	-2.8		1.344	0.1
0.400	1.5674	-2.9	23.000	1.323	0.8
0.450	1.5580	-3.0	24.000	1.299	1.5
0.500	1.5515	-3.1	25.000	1.273	2.5
0.550	1.5469	-3.1	26.000	1.24	3.5
0.600	1.5434	-3.2	27.000	1.21	4.9
0.700 0.800 0.900 1.000 1.250	1.5386 1.5356 1.5335 1.5320 1.5296	-3.2 -3.2 -3.2 -3.3 -3.3	28.000 29.000 30.000	1.17 1.13 1.09	6.4 8.4 10.8
1.500 1.750 2.000 2.500 3.000	1.5282 1.5272 1.5265 1.5253 1.5241	-3.3 -3.3 -3.3 -3.3 -3.3 -3.3	206 in maine 0.20	0.25.1-1.+0	0005 to 0.25

Table 5.1. Recommended Values on the Refractive Index and Its Temperature Derivative for Pure Rock Salt at 293 K\*

\* Estimated uncertainties for n;  $\pm 0.006$  in region 0.20-0.25 µm;  $\pm 0.0005$  in 0.25-0.35 µm;  $\pm 0.0001$  in 0.35-10.0 µm;  $\pm 0.003$  in 10.0-15.0 µm;  $\pm 0.006$  in 15.0-25.0 µm;  $\pm 0.02$  in 25.0-30.0 µm. Estimated uncertainties for dn/dT in units of  $10^{-5} \text{K}^{-1}$ :  $\pm 0.8$  in 0.20-0.24 µm;  $\pm 0.2$  in 0.24-4.0 µm;  $\pm 0.4$  in 4.0-15.0 µm;  $\pm 0.6$  in 15.0-20.0 µm;  $\pm 0.9$  in 20.0-30.0 µm.

absorption, in which a photon is absorbed and two or more phonons are generated, can occur and lead to absorption coefficients that range from 10<sup>-4</sup> cm<sup>-1</sup> to 100 cm<sup>-1</sup>, depending on the number of phonons generated. Recent measurements [49] on NaCl have shown that the absorption coefficient can be represented in the multiphonon absorption region by the expression:

$$A = A_0 \exp(-\nu/\nu_0)$$
 (5.19)

where  $\nu_0 = 56.0 \text{ cm}^{-1}$ , and  $A_0 = 24273 \text{ cm}^{-1}$ .

It is not known if the two exponential relations (eqs 5.18 and 5.19) hold for the visible and near infrared regions. If they do, the absorption in the transparent

region will be negligible. In a real situation, however, there are always traces of residual impurities and imperfections in the available crystal, consequently the absorption is noticeable though it is negligibly low as a rule.

Absorption data in the transparent region are very scanty. The reason is that absorption in this region is very low and its effects are thus unnoticeable in most applications. However, at high energy levels many unfavorable effects due to absorption take place. Unfortunately, investigations of absorption coefficient at the high energy level were made only at a few wavelengths of interest to laser applications. Harrington and Hass [50] studied the temperature dependence of multiphonon absorption at wavelength 10.6 µm from room temperature to near the melting point by a calorimetric method. His results are higher than those in the intrinsic tail. Deutsch [49] using a differential technique with a dual beam spectrometer measured an absorption coefficient for the wavelength region from 11.7 to 20  $\mu$ m at room temperature. The predicted value at wavelength 10.6  $\mu$ m obtained by fitting the measured values is  $1.1 \times 10^{-3}$  cm<sup>-1</sup> which agrees well with the measured value of  $1.3 \times 10^{-3}$  cm<sup>-1</sup> reported by Horrigan and Rudko [51]. This value was believed to conform to the values in the intrinsic tail. No noticeable improvement in the values could be obtained by improvements in purity and growth techniques. Califano and Czerny [52] examined the region,  $11-14 \mu m$ , at room temperature. Barker [53] measured the region, 11-20 µm, at temperature from 300 K up to 1105 K, 31 degrees beyond the melting temperature of NaCl. Their room temperature values agreed with those predicted by eq (5.4).

Owens [54] measured the room temperature absorption index at three wavelengths, 2.50, 8.02, and 32.3  $\mu$ m. By combining his measurement with others reported in the literature [11,12,14,55,56] in the wavelength range from 10 to 10<sup>7</sup>  $\mu$ m, he found a constant background loss corresponding to a residual value in absorption coefficient of  $1 \times 10^{-4}$ . The origin of this loss, which appeared to be independent of temperature is unknown. It is most probably due to imperfections in the crystals. A summary of the knowledge to date on the absorption index of rock salt is shown in figure 5.4.

Based on the above review of available data, the most probable values of intrinsic bulk absorption coefficients of a pure NaCl crystal at 293 K are derived as follows:

Wavelength range	Absorption coefficient, cm <sup>-1</sup>
$\begin{array}{rrrr} 0.165 & - & 0.173 \ \mu m \\ 0.25 & - & 9.00 \ \mu m \\ 9.0 & - & 30 \ \mu m \end{array}$	Use eq (5.3) Usually negligibly small Use eq (5.4)

Values derived and recommended in this way are also given in table 5.2. It should be noted that recommended values in table 5.2 are for a pure crystal. Crystals with impurities, other defects, and unfavorable surface conditions yield absorption coefficients in the transparent region which are expected to be noticeable. At the absorption center wavelengths, such absorption coefficients become extraordinarily large and unpredictable, depending upon the amount of foreign substances and the extent of defects.

While rock salt in the form of a pure chemical compound is clear and colorless, rock salts with impurities and defects reveal a variety of colors; gray to black, red, brown, yellow, green, blue, and violet. In table 5.3, a few typical natural colored rock salts are displayed together with the corresponding causes [57]. Most of the colors are caused by impurities, while some of the yellow, blue and violet colors owe their origin to radiation. Effects of radiation on the optical properties of rock salt will be discussed in a later section.

## 5.4. Effect of Nuclear Irradiation on the Optical Properties

Nuclear radiations either corpuscalar or electromagnetic are known to alter the properties of materials. The results of the interaction of energetic radiation with matter are to create microscopically many types of defects which lead to the observable changes of macroscopic properties. These involve such stable primary defects as vacancies, interstitials and dislocations which may be detected optically in a variety of colored absorption bands. These bands are located primarily in the visible region and therefore are easily recognized by the induced color. Generally the effect of nuclear radiation on the optical properties of rock salt is the coloration produced in the crystal. The strongest absorption band occurs at 0.465  $\mu$ m where the crystal turns yellow after being irradiated.

Color centers can be generated in a crystal in a variety of ways. The most important ones are: (1) exposure to ionizing radiation, (2) addition of impurities to produce coloration, and (3) imposition of electrolytic action to produce coloration. All of these processes occur in nature. However, the first process is primarily concerned with the effect of nuclear radiation on the properties. The term, ionizing radiation, includes all sources that can generate free electrons and holes in the crystal. The energies range from photons of a few eV, through x-rays and  $\gamma$ -rays up to high energy protons of 400 MeV. However, so far as the effect on the optical properties is concerned, studies showed that radiations of high energies produce similar results as those by lowenergy radiations. They both cause color centers of the same nature. The problem of "the effects of nuclear irradiation on the optical properties of rock salt" is therefore reduced to the studies of the F-center and Faggregate centers of rock salt. Detailed discussion of the subject of color centers is beyond the scope of the present work. For a comprehensive and concise review of the color centers, the interested readers are referred to the excellent articles by Seitz [60], Compton and Robin [61], Schulman and Compton [62], and Crawford and Slifkin [63]. Only a few typical examples pertinent to rock salt will be presented.

Irradiation with any type of ionizing radiation including ultraviolet light will produce an F-center



Table 5.2.	Calculated	Values on	the Intrinsic	Absorption
	Coefficient	for Pure	Rock Salt at	293 K

λ, μm	$\alpha$ , cm <sup>-1</sup>
0.165	4525
0.166	1217
0.167	332
0.168	92
0.169	26
0.170	7.4
0.171	2.2
0.172	0.63
0.173	0.19
5.3	$6 \times 10^{-10}$
10.6	1.1 x 10

TABLE 5.3. COLOR AND CAUSE OF NATURAL ROCK SALT

Color Family	Cause
Black	38.64% NaCl
	55.35% insoluble matter
Grey	Clay inclusions in either large aggregates or microscopical particles
Red	Iron compounds
Yellow	Due to radiation or iron compounds
Brown	Bituminous inclusions often arranged in regular layers
Green	Copper
Blue	Due to radiation
Violet	Due to radiation

together with a number of other centers, mostly the Faggregate centers. Figure 5.5 shows a typical absorption spectrum of an irradiated NaCl crystal in the wavelength region from 0.2 to 1.2  $\mu$ m where absorption is otherwise negligibly low. The absorption peaks at 0.210, 0.465, 0.545, 0.595, 0.720, and 0.823 are, respectively, identified as V<sub>3</sub>, F, R<sub>1</sub>, R<sub>2</sub>, M, and N centers.

The above centers are usually created at a low level of irradiation. At a high level of irradiation, a strong absorption band appears at  $0.57 \,\mu m$  corresponding to the absorption of colloidal sodium particles. The appearance of this adsorption band is generally accompanied by the diminution of F-absorption. The radiation-induced formation of colloidal sodium particles can amount to 0.001 to 0.1 atomic weight percent range. In one case of study [69], it was noted that the hydroxyl ions in the crystal may play some role in the formation of colloidal particles.

F-center production is the result of the capture of an electron by a negative ion vacancy. The F-absorption at 0.465  $\mu$ m corresponds to an electron transition from the ground state to a *p* excited state. The half-width of the F-absorption is temperature dependent, it is smallest at low

temperatures and the peak of the band shifts toward shorter wavelengths with decreasing temperature. The M-center is the simplest among the F-aggregate centers. It consists of two adjacent F-centers with its main axis oriented in the <110> plane. Because of anisotropic distribution of the axis of the center, the M-absorption shows dichroism. An R-center consists of three adjacent F-centers occupying an equilateral triangular array in a <111> plane of the NaCl structure. The N-center consists of four neighboring F-centers occupying a parallelogram array or a tetrahedral array. The V-center is due to the halogen molecular ion occupying two adjacent negative ion vacancies.

Kobayashi [64,65] studied the relationship between the behavior of the color centers and the density change during thermal annealing for sodium chloride crystals irradiated with 350 MeV protons with a total flux of  $1 \times$  $10^{16}$  protons/cm<sup>2</sup>. Figure 5.6 shows the changes of concentration of color centers and the change of density,  $\Delta$  n, of the crystal as a function of annealing temperature. It can be noted that, while below 475 K the density of the irradiated crystal remains constant, significant changes in the intensity of respective



Figure 5.5. Typical Absorption Spectrum of Irradiated Rock Salt

absorption bands are observed. It implies that in this region no noticeable annealing of vacancies takes place, while the continuous decreases of F and V<sub>3</sub> bands and the growths of the F-aggregate absorption bands are the results of thermal agitation which leads to the redistribution of the vacancies to form more clusters. It appears that the final products of such redistribution of vacancies are the R centers and other stable clusters.

When all of the color centers are converted to R centers and clusters, a further increase of temperature will anneal the vacancies out as indicated by the simultaneous drop of  $\Delta p$  and intensity of R-absorption band. At a temperature of 515 K, where all color centers have disappeared, the remaining  $\Delta p$  is due to the existence of other types of stable vacancy clusters. Beyond this point,  $\Delta p$  decreases almost linearly with increasing temperature and the crystal is completely recovered at 673 K.

It can be said that the nuclear radiation effect on the optical properties is to increase the absorption coefficient particularly at the color centers. A well known method to study the formation of defects induced by radiation in rock salt is to obtain the so-called F-coloring curve, which shows the variation of the F-center concentration with irradiation dose. Hodgson, Delgado and Rivas [66] investigated the gamma-ray produced Fcoloring curve for NaCl at and above room temperatures. The dose rate was approximately 350 R/min, produced by bombarding 1.8 MeV electrons on a gold target. The results are shown in figure 5.7. The curves corresponding to temperatures 293, 323, and 373 K show the increasing F-center concentrations and the approaching saturations at the respective temperatures. At temperatures above 373 K, the respective curves have a broad maximum which decreases as the temperature increases. This change is due to the formation of F-aggregate centers in accordance with the data shown in figure 5.6. Jain and Lidiard [67], in the study of the growth of colloidal centers in irradiated alkali halides, calculated the growth of F-center concentration as a function of dose as given in figure 5.8. It can be seen that the F-center concentration reaches its saturation at quite a low dose and is very temperature dependent. It should be noted that in all cases the saturated F-center concentration decreases with increased temperature. There are two contributing factors, the thermal



bleaching and the optical bleaching. The thermal bleaching is actually the thermal annealing caused by energy absorption. The optical bleaching can be obtained either from radiation of appropriate frequency or from luminescence caused by the excitation of the electrons. Both of the bleaching effects are present at any operational condition.

Nowick [68] investigated the growth of the F band in NaCl crystals with 1.2 MeV gamma-ray irradiation using a CO<sup>60</sup> source. Crystals of different origins, heat treatments, and states of deformation were measured. While deformation has a small effect on the concentration of F-centers in the early stage of F band growth, the effect on the later stage is large. The growth of F band in the undeformed and annealed crystals appears to saturate rapidly at about 1017 F-center/cm<sup>3</sup> and continue to grow slowly and linearly with time. The deformed crystals, however, continue to grow at a considerably higher rate in the later stage of irradiation time as shown in figures 5.9 and 5.10. Furthermore, the deformed crystals cannot be completely bleached; the R band remains. Based on the available information on the F-center investigation, it was concluded that F-center coloration at room temperature proceeds in two distinct stages:

(1) The first stage consists of a rapid filling of the vacancies and vacancy clusters present in the crystal prior to irradiation.

(2) The second stage consists of the creation of new vacancies at a slow rate and their transformation into F-centers.

The effect of deformations is to create new dislocations and possibly to help disperse the precipitated impurities with the consequence of more F-centers creation.

Compton [69] observed the coloration of synthetic and natural NaCl crystals with CO<sup>60</sup> gamma-ray and 1.3 MeV electron irradiations. It was found that these



Figure 5.7. F-center color curves obtained for NaCl sample temperatures between 20 and 300 °C at a dose rate of approximately 350 R/min [66].

irradiations produced the colloid band, at 0.565  $\mu$ m, in the synthetic crystals but not in natural crystal. This colloid band became much stronger than F-center absorption at high doses. Through various thermal treatments given the natural crystal prior to their coloration, it was found that the hydroxyl ions played an important role in the conversion of F-centers into colloids.

Observations of Nowick [68] and Compton [69] may provide clues regarding the nature of blue rock salt. In the deformed rock salt, the optically unbleachable R-



Figure 5.8. The predicted dose dependence of F-center concentration in NaCl at temperatures of 398, 423 and 448 K [67].



Figure 5.9. Early stage of F-band growth for irradiated NaCl crystals [68].

band covers a broad spectral range centered at about 0.6  $\mu$ m. The presence of hydroxyl ions in the crystal seem to be essential in the formation of the colloid band, at 0.565  $\mu$ m, by irradiation. As both absorption bands contribute to the blue appearance of the crystal, it may be possible to conclude that the blue rock salt is the consequence of nuclear irradiation on a rock salt crystal which contains hydroxyl ion substituted lattice defects which was plastically deformed in the geological past.

Not only does the F-center concentration depend on temperature and radiation dose, but it also varies with the incident energy of radiation. Figure 5.11 is a plot of the number of F-centers produced per proton versus the energy of the protons [70]. It was also observed in the case of intense irradiation that the peak of F-center absorption was slightly shifted toward shorter wavelength. This may be due to the high concentration of lattice defects and an associated interaction between them [71]. Data on the effect of neutron exposure on the optical properties on rock salt is rather scanty. Available information [72] indicates that neutron bombardment is more effective in producing defects.

From the available information on the color center investigations, it is noted that neither F-center nor Faggregate center absorption bands have been found to extend into the 10.6  $\mu$ m region when observed by the usual spectrometric methods. However, Lipson, Ligor, and Martin [73], measured the absorption coefficient at 10.6  $\mu$ m by CO<sub>2</sub> laser calorimetry for NaCl crystals irradiated with CO<sup>60</sup> gamma-rays. It was found that the absorption at 10.6  $\mu$ m increased upon irradiation.



Figure 5.10. The same F-band growth curves as in Figure 5.9 carried out to a much longer irradiation time [68].



Figure 5.11. Number of F-centers produced by one proton per cm path in NaCl irradiated with 10<sup>16</sup> protons/cm<sup>2</sup> [70].

Through a careful analysis, they concluded that the increase in absorption at 10.6  $\mu$ m after irradiation is associated with the F-aggregate centers.

In general, it can be safely said that the effect of nuclear radiation on the optical property of rock salt is to increase the absorption coefficient across the spectrum, with much greater absorption at the color centers. The effects resulting from crystal irradiation are, however, influenced by many factors:

- a. The thermal history of the crystal,
- b. The irradiation history of the crystal,
- c. The origin of the crystal,
- d. The energy of the radiation,
- e. The dose rate of the radiation,
- f. The length of exposure (the total dose),
- g. The physical environment (temperature, pressure, radiation), and
- h. The impurity contents of the crystal.

Whatever the factors are, the result is the coloration of the crystal. Although the colored crystal may be bleached optically or thermally, some of the defects will remain as permanent damage to the crystal. The most important of such defects is the creation of additional impurities which result from the primary bombardment of particles and/or when their products are stopped by the crystal.

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## Symbols and Units

Symbol	Name	Units
A	Absorption coefficient	cm <sup>-1</sup>
d	Sample thickness	cm
Ε	Energy	eV
Ea	Absorbed energy	eV
hw	Energy of light quantum	eV
k	Absorption index or extinction	
	coefficient	dimensionless
LO, TO	Longitudinal and transverse	
	optical phonon modes	
п	Refractive index	dimensionless
R	Reflectivity	dimensionless
Т	Temperature	K
Т	Transmission	dimensionless
α	Intrinsic absorption coefficient	cm <sup>-1</sup>
$\Delta  ho$	Density change	cm <sup>-3</sup>
€o	Static dielectric constant	dimensionless
e	Dielectric constant	dimensionless
λ	Wavelength	μm
θ	Phase angle	radius
λ	Light frequency	s <sup>-1</sup>

Wavelength		
To convert jrom	to S	Multiply by

240

# Chapter 6 Electrical and Magnetic Properties

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### 6.1. Introduction

There have been extensive measurements made on the electrical properties. In most cases an effort was made to critically evaluate the available data and come forth with recommended reference values. When this was not possible, selected sets of data are presented as typical cases with the state presented in both tabular and graphical form for ease of use. The difficulty in developing recommended values arises from the uncharacterized nature of the samples reported and the large changes in the properties due to impurities. Because of these difficulties, data for pure and doped sodium chloride have been included.

The very meaning of "rock salt" gives an indication of the variation in composition to be expected. The percentage of NaCl in "rock salt" ranges from 17% to 99+% with a range around 96% being a typical value; typical values of impurities are water 0.17-0.5%, anhydrite 0.1-80%, other salts 0.08-0.5%, carbonates 0.01-0.2%, and sulfate 0.1-10% [128]. In addition, numerous liquid and gaseous inclusions are known to be in rock salt.

Preceding the presentation and discussion of the data, a brief discussion is given of methods of measurement for the purpose of pointing out the basic idea of the methods and giving references for additional information for the interested reader.

## 6.2. Methods of Measuring Electrical and Magnetic Properties

#### 6.2.1. Methods of Measuring Electrical Conductivity

The electrical conductivity in the solid state is determined by measuring the resistance of a slab of material of known dimensions. The resistance is found by placing the material between metallic electrodes and finding the current flowing for a given known electric potential. To aid in obtaining good contacts Aquadag, a colloidal dispersion of graphite, is sometimes put on the faces of the material on which the metallic contacts are to be placed. Details of measuring the conductivity in the solid state can be found in references [112, pp. 26–35; 5, p. 1005; and 2, p. 1497]. A discussion of electrode behavior in the determination of ionic conductivity is given in reference [113]. The error inherent in the measurement of the electrical conductivities with the 4probe method can be of the order of  $\pm 0.1\%$ .

In the liquid state there are three main types of cells used to measure the electrical conductivity. With the Ushaped capillary type the liquid material is contained entirely within the cell. With the dip-type cell the capillaries are immersed in the liquid material. The third type uses electrodes immersed in the liquid material. Additional details are in references [46, pp. 875-6; 114, p. 3; and 115, pp. 583-6]. The errors inherent in the measurement of the electrical conductivities in the liquid state can be as high as several percent for the dip-type cell because of the problem of parasitic conduction, but for the U-type cell, where this problem is not present, it can be of the order of 0.1%.

#### 6.2.2. Methods of Measuring Dielectric Constant

The general idea behind the determination of the real and imaginary parts of the dielectric constant is the measurement and comparison of a capacitor containing the dielectric material and the same capacitor without the dielectric. In different frequency regions, different experimental methods are used. At lower frequencies, typically 10<sup>2</sup> to 10<sup>7</sup> Hz, bridge methods are applicable. At higher frequencies resonant circuit methods can be used while at frequencies greater than the order of 100 MHz transmission line methods are used while at higher frequencies, waveguide and cavity resonator methods can be used. Details can be found in references [69, pp. 315-6; 116, chapter 3, pp. 109-68; 117, chapter 2, pp. 21-38; 118, p. 1; 119, pp. 47-122; 72; and 120, pp. 364-390]. The inherent inaccuracy in the measurement of the dielectric constant can be of the order of 0.1% or better.

#### 6.2.3. Methods of Measuring Dielectric Strength

The dielectric strength is the maximum electric field strength a material can withstand before the onset of a rapid increase in electrical conduction. The dielectric strength is measured by increasing the voltage applied to a specimen and noting when conducting paths form. Additional details can be found in references [121, pp. 6-7; and 81, pp. 2, 3, 6, and 7]. One writer [98, p. 103] points out that the variation in the breakdown voltage can be held to within  $\pm 5\%$  as well as for the sample thickness thus giving an uncertainty in these quantities alone that should not exceed  $\pm 10\%$ .

#### 6.2.4. Methods of Measuring Magnetic Susceptibility

The magnetic susceptibility of sodium chloride has been measured using the Faraday method which is also known as the non-uniform field method. The principle behind this method is the measurement of a force, using a sensitive balance, on a small specimen suspended between pole pieces in which the magnetic field and its spatial derivative do not vary very much. The sensitivity using this method is high with an accuracy that can be attained of  $\pm 0.1\%$ . Additional details can be found in references [122, pp. 428–30; 123, pp. 11–8; and 124, pp. 458–9].

In the Gouy method or uniform field method, a long sample is suspended between pole pieces such that one end of the sample is in the region of maximum field strength and the other end in a region where the field is minimal. The force is measured by a balance and the force is proportioned to the square of the maximum field strength. Generally the accuracy using this method can be  $\pm 1\%$  which can be improved to an accuracy of  $\pm 0.1\%$ [124, p. 454]. Additional details can be found in references [122, pp. 429–30; 123, pp. 3–10; and 124, pp. 456–7].

### 6.3. Electrical Conductivity

#### 6.3.1. Solid State, Temperature Dependence

Evaluated data are given for the intrinsic electrical conductivity of pure sodium chloride in the solid state. The evaluated data are given in table 6.1 and shown on figure 6.1. Table 6.2 gives the experimental data for data sets used specifically to develop the evaluated data as well as other selected data in order to illustrate the behavior for pure sodium chloride, sodium chloride with known amounts of dopants, and naturally occurring rock salt. A discussion of some features of the data follows before describing how the evaluated data were arrived at.

There are several characteristics of the conductivity data as a function of temperature that bear mentioning. The conductivity increases as the temperature increases and, moreover, does so by orders of magnitude from room temperature of 293 K (or  $10^3/T=3.41$ ) to the melting point of 1074 K (or  $10^3/T=0.931$ ). This large change suggests plotting the conductivity on a logarithmic scale.

Another feature of the data is that there are distinct regions where log  $(\sigma T)$  is linear when plotted as a function of  $T^{-1}$  (curve 15). This is further illustrated in the literature both for pure and doped sodium chloride [7, fig. 1; 15, fig. 1; and 16, fig. 1]. In addition, theoretical considerations lead to the conclusion that in three conductivity regions, one of which is the intrinsic, log  $(\sigma T)$  versus  $T^{-1}$  is linear [4]. Based on the consideration that much of the data in the literature are presented as log  $(\sigma T)$  as a function of  $10^3/T$ , it was decided to plot figure 6.1 similarly.

On figure 6.1, it is observed that below the melting point to perhaps  $10^3/T \sim 1.3$ , there is a limiting line below which data do not extend. This is the intrinsic region applicable to the pure material (parts of data sets 4, 5, 7, 8, 9, and 15). Several of these data sets are for pure sodium chloride. Jain and Dahake [4] (curve 7) presented data on spectroscopically pure material, Etzel and Maurer [5] (curve 9) presented results from measurements on pure sodium chloride, and Trnovcova et al. [8] (curve 15) also gave measurements on pure material. It should be noted that very close to the melting point, a behavior different from the extension of linearity of the intrinsic-region behavior is evident (curve 5 for  $10^3/T < 1.0$ ).

Other features are also evident in figure 6.1. Specimens doped with impurities exhibit differences in the value of the conductivity (curves 3, 6, 10, 11, 12, and 14). Specimens that come from natural crystals show a wide variation (curves 4 and 16). Other conditions are for a single crystal (curve 1), pellet (curve 2), disk specimen made under pressure (curve 5), a single crystal with low background impurity (curve 8), and a specimen called "rock salt" by the author (curve 13). For the same impurity, the conductivity increases as the impurity content increases (curves 11 and 12).

Recent measurements of the DC resistivity by Olhoeft [127] (curves 17-20), made at 295 K on halite cored from a Carlsbad, New Mexico corehole, show a variation between subsamples. In addition, data for the real part of the complex resistivity as a function of frequency are also presented and range from  $5.16 \times 10^6 \Omega m$  to  $1.86 \times 10^6 \Omega m$  at a frequency of  $10^2$  Hz. This can be compared to the estimate based on dielectric measurements of the Laboratory for Insulation Research [60] at 298K. Using a frequency of  $10^2$  Hz, a value for the real part of the dielectric constant of 5.90 (see data set 1 in table 6.7), a value of tan  $\delta$  of  $< 1 \times 10^{-4}$  [60, p. 302], and the relation between this resistivity and the dielectric properties (and

TABLE 6.1.	EVALUATED DATA FOR	THE INTRINSIC	ELECTRICAL	CONDUCTIVITY	01
	SOLID, PURE SODIUM	CHLORIDE			

[Temperature, T, K; Electrical Conductivity, J, S m<sup>-1</sup>]

Т	<sup>0</sup> intrinsic
25	$2.06 \times 10^{-4}$
50	$4.27 \times 10^{-4}$
75	$8.47 \times 10^{-4}$
00	$1.62 \times 10^{-3}$
25	$2.98 \times 10^{-3}$
50	$5.31 \times 10^{-3}$
75	9.19 x 10 <sup>-3</sup>
00	$1.54 \times 10^{-2}$

8

10



FIGURE 6.1. Electrical conductivity of solid sodium chloride (temperature dependence).
# TABLE 6.2. EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF SOLID SODIUM CHLORIDE (Temperature Dependence)

[Temperature, T,	,K;	Electrical	Conductivity,	σ,	S	m	1	]
------------------	-----	------------	---------------	----	---	---	---	---

Data Set	Author(s), Year [Ref.]	10 <sup>3</sup> /T	log(JT)	Remarks
1	Torkar, K., 1965 [1]	1.250 1.301 1.304 1.451 1.626 1.818 2.202 2.265 2.448 2.862 3.153	-0.952 -1.137 -1.242 -1.668 -2.082 -3.124 -4.849 -5.177 -6.069 -7.944 -9.221	NaCl single crystal; measured in air using isothermal method; data points extracted from figure; analytically, temperature de- pendence, $\sigma = 2.5 \exp(-20,700/\text{RT})$
2	Torkar, K., 1965 [1]	1.650 1.979 2.302 2.739 3.116	-2.625 -4.248 -5.902 -7.872 -9.264	NaCl pellet; measured in air using isothermal method; data points extracted from figure; analytically, temperature dependence $\sigma$ = 1.0 exp(-20,700/RT).
3	Radhakrishna, S. and Karguppikar, A.M., 1973 [2]	1.287 1.354 1.354 1.397 1.439 1.464 1.489 1.532 1.549 1.574 1.591 1.624 1.641 1.667 1.709 1.726 1.759 1.793 1.827 1.869 1.920 1.970 1.996 2.030 2.072 2.105 2.156 2.215 2.257 2.308 2.359 2.426 2.544 2.612 2.679	0.267 -0.150 -0.283 -0.400 -0.467 -0.567 -0.600 -0.683 -0.800 -0.867 -0.933 -0.983 -1.067 -1.150 -1.217 -1.300 -1.367 -1.483 -1.617 -1.483 -1.617 -1.483 -2.017 -2.183 -2.017 -2.183 -2.017 -2.183 -2.367 -2.500 -2.650 -2.800 -3.033 -3.250 -3.483 -3.700 -3.983 -4.233 -4.517 -4.800 -5.033 -5.233	NaCl crystals Sb-doped to 0.0080 (80 ppm); crystals grown from melt by Kyropoulos tech- nique starting with BDH-AR grade salt, Sb then diffused by heating the crystal in Sb vapor at 973 ± 5 K for about 6 days, the NaCl and Sb metal sealed together in quartz tube after evacuating to approx 10 <sup>-3</sup> torr; impurity content estimated by mass spectro- scopic analysis; data points of log(0T) versus 10 <sup>3</sup> /T extracted from figure; conduc- tivity measurements incorporated a GR 1644-A M <sub>2</sub> bridge; specimens prepared for measure- ments by coating two opposite faces of crystal with thin coating of aquadag and crystal placed between two platinum plates.

Data Set	Author(s), Year [Ref.]	10 <sup>3</sup> /T	log(OT)	Remarks
4	Phipps, T.E., Lansing,	0.947	1.984	NaCl natural crystal (Navarre), rock salt;
	W.D., and Cooke, T.G.,	0.953	1.871	resistances from 0 to 0.5 M $\Omega$ measured using
	1926 [3]	0.950	1.774	telephone and drum-wound conductivity bridge
		0.970	1.686	with a Leeds and Northrup 1000 Hz microphone
		0.980	1.430	nummer as source of ac, from 0.5 to 100 MM
		0.993	L.3/3	wheatstone bridge method used with 8 V dc
		1.010	1.121	V de wood for the highest resistances and 110
		1 060	0 589	certainty in temperature 1 or 2 K. composite
		1.093	0.448	data of 3 experiments with different crystals
		1,107	0.336	extracted from table: at $10^3/T = 1.28$ (T =
		1,110	0.115	781 K) slope changes in log $\sigma$ versus $10^3/T$
		1,148	-0.068	plot.
		1.160	-0.304	F====
		1.175	-0.255	
		1.209	-0.589	
		1.210	-0.645	
		1.210	-0.808	
		1.226	-0.759	
		1.235	-0.780	
		1.237	-0.848	
		1.260	-1.022	
		1.265	-1.225	
		1.260	-1.192	
		1.282	-1.184	
		1.321	-1.484	
		1.330	-1.597	
		1.363	-1.631	
		1.410	-1.934	
		1,431	-2.008	
		1.401	-2.230	
		1.550	-2.425	
		1 670	-3 008	
		1.682	-3.228	
		1.747	-3.496	
		1.795	-3,635	
		1.796	-3.706	
5	Phipps., T.E., et al.	0.948	1.866	NaCl; material obtained from S.A. Braley of
	1926 [3]	0.950	1.724	the Analytical Division of Chemical Lab. of
		0.950	1.729	the University of Illinois and had been
		0.970	1.623	twice crystallized, twice centrifuged, and
		0.980	1.405	dried at temperatures near the melting point;
		0.980	1.415*	specimen prepared by pressing the powdered
		1.000	1 129*	dicks were suite transparent, dick specimen
		1 000	1 130	1.5 mm thick: resistances from 0 to 0.5 MO
		1 030	1 009	measured using telephone and drum-wound con-
		1,060	0.638	ductivity bridge with a Leeds and Northrup
		1,110	0.209	1000 Hz microphone hummer as source of ac
		1,110	0,193	from 0.5 to 100 M $\Omega$ Wheatstone bridge method
		1,116	0,192	used with 8 V dc used in range of lower re-
		1.160	-0.166	sistances and 110 V dc used for the highest
		1.160	-0.200	resistances; uncertainty in temperature 1 or

\* Not shown in figure.

Data Set	Author(s), Year [Ref.]	10 <sup>3</sup> /T	log(oT)	Remarks
5 (cont.)	Phipps, T.E., Lansing, W.D., and Cooke, T.G., 1926 [3]	$\begin{array}{c} 1.200\\ 1.210\\ 1.289\\ 1.310\\ 1.310\\ 1.360\\ 1.399\\ 1.410\\ 1.447\\ 1.447\\ 1.447\\ 1.447\\ 1.460\\ 1.530\\ 1.561\\ 1.600\\ 1.670\\ 1.691\\ 1.740\\ 1.810\\ 1.810\\ 1.810\end{array}$	$\begin{array}{c} -0.447 \\ -0.546 \\ -0.975 \\ -1.141 \\ -1.238 \\ -1.410 \\ -1.686 \\ -1.655 \\ -1.860 \\ -1.764 \\ -1.902 \\ -2.235 \\ -2.540 \\ -2.561 \\ -2.897 \\ -3.140 \\ -3.240 \\ -3.542 \\ -3.624 \end{array}$	2 K; composite data of three runs with different high-pressure disks extracted from table; at 916 K slope changes in log $\sigma$ versus 10 <sup>3</sup> /T plot; first value of 10 <sup>3</sup> /T = 1.310 taken with ac, second value taken with dc.
6	Jain, S.C. and Dahake, S.L., 1964 [4]	1.205 1.243 1.292 1.343 1.421 1.514 1.592 1.690 1.802	0.458 0.309 0.128 -0.076 -0.382 -0.745 -1.097 -1.528 -2.049	NaCl single crystal; Ba-doped to concentra- tion 0.0045 at.%; grown from melts of BDH analar NaCl using Kyropoulos method; barium impurity added in form of chloride to melt; concentration of barium estimated approx by comparing ionic conductivity (in impurity range) of Ba-doped NaCl with corresponding conductivity of NaCl containing known con- centration of nickel; rapidly quenched; thin coating of aquadog applied to two opposite faces and crystal put between two plates made of a platinum-rhodium alloy; measure- ments performed in an atmosphere of pure nitrogen to avoid oxidation of graphite electrodes; measurements performed using dc pulse and ballistic galvanometer; data points of log( $\sigma$ T) versus 10 <sup>3</sup> /T extracted from a figure; accuracy of conductivity 5% at lowest temperature used and 1% at higher temperatures.
7	Jain, S.C. and Dahake, S.L., 1964 [4]	$1.018 \\ 1.034 \\ 1.050 \\ 1.070 \\ 1.081 \\ 1.091 \\ 1.154 \\ 1.160 \\ 1.191 \\ 1.222 \\ 1.233 \\ 1.248 \\ 1.264 \\ 1.316 $	$\begin{array}{c} 1.262\\ 1.000\\ 0.870\\ 0.765\\ 0.608\\ 0.504\\ -0.097\\ -0.202*\\ -0.437\\ -0.751\\ -0.803\\ -0.986\\ -1.117\\ -1.535\end{array}$	Spectroscopically pure NaCl; impurity con- centration 0.00015 at.%; grown from melt at Johnson Matthey spectroscopically pure NaCl using Kyropoulos method; rapidly quenched from 973 K at about 200 K min <sup>-1</sup> ; thin coat- ing of aquadog applied to opposite faces and then specimen put between two plates made of a platinum-rhodium alloy; measure- ments performed in an atmosphere of pure nitrogen to avoid oxidation of graphite electrodes; measurements performed using dc pulse and ballistic galvanometer; data points of log( $\sigma$ T) versus 10 <sup>3</sup> /T extracted from a figure; accuracy of conductivity 5% at

TABLE 6.2. EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF SOLID SODIUM CHLORIDE (Temperature Dependence) (continued)

\* Not shown in figure.

Data Set	Author(s), Year [Ref.]	10 <sup>3</sup> /T	log(σT)	Remarks
7 (cont.)	Jain, S.C. and Dahake, S.L., 1964 [4]	1.358 1.421 1.520 1.645 1.755 1.870	-1.770 -2.057 -2.396 -2.840 -3.257 -3.753	lowest temperature used and 1% at higher temperatures.
8	Jain, S.C. and Dahake, S.L., 1964 [4]	1.175 1.207 1.255 1.307 1.360 1.434 1.498 1.656 1.741 1.820	-0.226 -0.382 -0.591 -0.825 -1.033 -1.267 -1.527 -2.125 -2.464 -2.854	NaCl single crystal; background impurity content 0.0010 at.%; grown from melt of BDH analar NaCl using Kyropoulos method; rapidly quenched from 973 K at about 200 K min <sup>-1</sup> ; thin coating of aquadag applied to opposite faces and then specimen put between two plates made of a platinum-rhodium alloy; measurements performed in an atmosphere of pure nitrogen to avoid oxidation of graphite electrodes; measurements performed using dc pulse and ballistic galvanometer; data points of log( $\sigma$ T) versus 10 <sup>3</sup> /T extracted from a figure; accuracy of conductivity 5% at lowest temperature used and 1% at higher temperatures.
9	Etzel, H.W. and Maurer, R.J., 1950 [5]	1.01 1.04 1.09 1.15 1.18 1.22 1.25 1.32 1.41 1.48 1.55 1.63 1.67 1.75	1.120* 0.783 0.362 -0.136 -0.519 -0.736* -0.921 -1.208 -1.587 -1.846 -2.115 -2.437 -2.623 -2.955	Sample designation N; pure NaCl; impurities <0.00001 B, <0.00001 Be, <0.00001 Cr, <0.00001 Cu, <0.00001 Fe, <0.00001 Li, <0.00001 Si, <0.0001 Ag, <0.0001 Al, <0.0001 As, <0.0001 Ba, <0.0001 Ca, <0.0001 Cd, <0.0001 Co, <0.0001 Hg, <0.0001 K, <0.0001 Mg, <0.0001 Mn, <0.0001 Ni, <0.0001 P, <0.0001 Ti, <0.0001 Zn, <0.0001 Zr, and Mo V, and W not detected; Eimer and Amend Tested Purity NaCl source of material; singl crystal grown from melt by Kyropoulos method using platinum crucible; cleaved into cubes approx 1 cm on an edge and annealed in an atmosphere of helium at 1043 K (heating rate 6 K min <sup>-1</sup> ) for 1 h, slowly cooled to room temperature at 1 K min <sup>-1</sup> (for pure crystal and one containing 0.0002 mole frac- tion Cd conductivity not altered when cool- ing rate changed to either 3 K min <sup>-1</sup> or 0.3 K min <sup>-1</sup> , conductivity of a quenched pure crystal rapidly cooled in air by removing it from oven at 1043 K was same as that of crystal cooled at 1 K min <sup>-1</sup> ); then cleaved into plates approx 1 mm thick; electrodes used were either platinum evaporated on crystal surfaces in a vacuum or colloidal graphite painted on in alcohol solution (both materials yielded identical results); during measurements crystals mounted between platinum clad nickel electrodes in a quartz tube; measurement method used a ballistic

TABLE 6.2.	EXPERIMENTAL	DATA	ON	THE	ELECTRICAL	CONDUCTIVITY	OF	SOLID	SODIUM	CHLORIDE
	(Temperature	Deper	nder	ice)	(continued	i)				

\* Not shown in figure.

TABLE 6.2.EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF SOLID SODIUM CHLORIDE<br/>(Temperature Dependence) (continued)

Data Set	Author(s), Year [Ref.]	10 <sup>3</sup> /T	log(σT)	Remarks
9 (cont.)	Etzel, H.W. and Maurer, R.J., 1950 [5]			galvanometer which measured charge passing through crystal on application of square pulse of voltage of known magnitude and duration; accuracy of conductivity estimated as ±5%.
10	Etzel, H.W. and Maurer, R.J., 1950 [5]	1.48 1.55 1.62 1.70	-1.658 -1.940 -2.260 -2.580	Sample designation K; crystal grown from melt containing 0.01 at.% KCl, expected con- centration of KCl in crystal was about 0.1 of its concentration in melt.
11	Etzel, H.W. and Maurer, R.J., 1950 [5]	1.48 1.55 1.62 1.69 1.76 1.83 1.90	-1.157 -1.445 -1.743 -2.079 -2.426 -2.771 -3.046	Sample designation H; mole ratio Cd/Na 1 x $10^{-5}$ ; single crystal grown from melt by Kyropoulos method using platinum crucible; source materials were Eimer and Amend Tested Purity NaCl and Baker and Adamson CdCl ; cleaved into cube approx 1 cm on an edge and annealed in an atmosphere of helium at 1043 K (heating rate 6 K min <sup>-1</sup> ) for 1 h, slowly cooled to room temperature at 1 K min <sup>-1</sup> , then cleaved into plates approx 1 mm thick; electrodes used were either platinum evaporated on crystal surfaces in a vacuum or colloidal graphite painted on in alcohol solution (both materials yielded identical results); during measurements crystals mounted between platinum clad nickel electrodes in a quartz tube; measurement method used a ballistic galvanometer which measured charge passing through crystal on application of square pulse of voltage of known magnitude and duration; accuracy of conductivity estimated as $\pm 5\%$ .
12	Etzel, H.W. and Maurer, R.J., 1950 [5]	1.48 1.55 1.62 1.69 1.76 1.84 1.90	0.208 -0.100 -0.428 -0.785 -1.064 -1.471 -1.803	Similar to the above specimen and conditions except sample designated as A and mole ratio Cd/Na 68.6 x $10^{-5}$ with duplicate analysis giving 64.0 x $10^{-5}$ .
13	Seelen, D., 1924 [6]	1.293 1.486 1.745 2.113 2.680 3.413	-1.456 -3.088 -4.479 -6.001 -8.568 -12.197	Rock salt; compilation of results reported by this author in this paper; data extracted from table.
14	Dreyfus, R.W. and Nowick, A.S., 1962 [7]	1.49 1.61 1.72 1.81 1.92 2.00 2.08 2.13	-0.64 -1.20 -1.71 -2.21 -2.82 -3.12 -3.48 -3.78	Sample number L20A; specimen with CaCl <sub>2</sub> added; metallic impurity concentration 0.0100 ± 0.0030 and determined by semiquanti- tative spectroscopic analysis; specimen size 1 cm by 1 cm by 0.04 cm; specimen prepared by adding CaCl <sub>2</sub> to reagent grade NaCl and grown by Bridgman technique; cooled from range of 343 to 573 K down to 203 K at

Data Set	Author(s), Year [Ref.]	10 <sup>3</sup> /T	log(σT)	Remarks
14	Dreyfus, R.W. and	2.22	-4.24	cooling rate of 0.3 K min <sup>-1</sup> ; data taken with
(cont.)	Nowick, A.S., 1962 [7]	2.27	-4.59	increasing temperature; data points extracted
		2.41	-5.20	from figure; accuracy of temperature ±0.1
		2.47	-5.71	$\pm$ 0.005 T with T in °C.
		2.51	-5.96	
		2.60	-6.52	
		2.71	-7.02	
		2.76	-/.33	
		2.91	-8.14	
		3.34	-10.37*	
		* Not s	hown in figu	ire.
15	Trnovcova, V., Mariani,	1.030	0.930	Pure; contains 2 x 10 <sup>-5</sup> molar percent biva-
	E., and Polak, K.,	1.049	0.692	lent metals; thermal treatment of annealing
	1974 [8]	1.074	0.560	for 2 h at 1023 K and quenching employed in
		1.099	0.242	most measurements; sample equipped with
		1.112	0.151	graphite contacts and a dc voltage of 10 V
		1.149	-0.179	applied for measurements; measured in an
		1.187	-0.537	inert atmosphere of dry argon; data extracted
		1.212	-0.892	from smooth curve.
		1.231	-0.955	
		1.237	-1.014	
		1.262	-1.167	
		1.306	-1.382	
		1.381	-1.664	
		1.443	-1.940	
		1.512	-2.219	
		1.58/	-2.520	
		1 737	-2.002	
		1 818	-3.444	
		1.912	-3 838	
		1,994	-4.199	
		2.069	-4.559	
		2,156	-4.949	
		2,219	-5.277	
		2.300	-5.607	
		2.362	-5.934	
		2.438	-6.263	
		2.500	-6.560	
		2.575	-6.859	
		2.625	-7.125	
16	Lehfeldt, W., 1933 [9]	1.088	0.454	Naturally occurring rock salt; estimated
		1.107	0.301*	inaccuracy ±10%; data points extracted from
		1.144	0.189*	figure.
		1.181	0.077	
		1.228	-0.136*	
		1.246	-0.240*	
		1.302	-0.406	
		1.321	-0.461*	
		1.339	-0.613*	
		1.300	-0.720*	
		* Not s	hown in figu	170

Data Set	Author(s), Year [Ref.]	10 <sup>3</sup> /T	log(σT)	Remarks
16 (cont.)	Lehfeldt, W., 1933 [9]	1.414 1.451 1.488 1.525 1.553 1.572 1.609 1.646 1.702 1.748 1.776 1.804 1.841 1.869	-0.832* -0.990 -1.196* -1.304 -1.507* -1.561* -1.718* -1.718* -2.073* -2.073* -2.340* -2.541 -2.645* -2.801* -2.905	
		*Not sh	own in figur	e.
17	Olhoeft, G.R., 1978 [127]	3.39	-5.73	Subsample 1; halite salt cored from 786 m deep in ERDA #9 corehole at Carlsbad, New Mexico; core cut into 4 subsamples; salt crystals in core had undetectable impurity levels but cracks and grain boundaries con- tained large amounts of impurities; disc geometry 1.7 cm thick and 10.6 cm diam; sample holder was 3-terminal brass configura- tion with 3.8 cm diam guarded electrode under 8.5 kPa uniaxial load; measured in 3% rela- tive humidity; accuracy $\pm 5\%$ in resistivity; accuracy in dielectric permittivity $\pm 0.65\%$ ; $\rho = 1.57 \times 10^8 \Omega$ m for DC conditions.
18	Olhoeft, G.R., 1978 [127]	3.39	-5.08	Similar to the above specimen and conditions except subsample 2 and $\rho$ = 3.58 x $10^7~\Omega\text{m}$ .
19	Olhoeft, G.R., 1978 [127]	3.39	-5.57	Similar to the above specimen and conditions except subsample 3 and $\rho$ = 1.09 x 10 <sup>8</sup> $\Omega$ m.
20	Olhoeft, G.R., 1978 [127]	3.39	-5.43	Similar to the above specimen and conditions except subsample 4 and $\rho$ = 7.92 x 10 <sup>7</sup> $\Omega$ m.

TABLE 6.2.EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF SOLID SODIUM CHLORIDE<br/>(Temperature Dependence) (continued)

frequency) [60, p. 294], a value of  $3.05 \times 10^{11} \Omega$ m is obtained for fresh sodium chloride crystals from Harshaw.

The evaluated data for the intrinsic conductivity of pure sodium chloride were based on the data from data set 15. The result of a least-squares fit gave

$$\sigma_{\text{intrinsic}} = \frac{2.637 \times 10^{10}}{T} e^{-\frac{21,258}{T}}$$
(6.1)

(T in K,  $\sigma$  intrinsic in S m<sup>-1</sup>) which is applicable over the temperature range of 825 K to 1000 K. The values given in table 6.1 were calculated from equation (6.1). The Least Square Polynomial Equation Curve Fit (LSPE) program at the Purdue University Computing Center was utilized to obtain equation (6.1). This program utilizes the F-statistic to optimize the order of a polynomial fit to

data. The order of the polynomial is successively increased until a maximum is found in the F-statistic. LSPE was applied to the intrinsic conductivity data for the data applying to pure sodium chloride (data sets 7,9,15); the best fit to  $\log(\sigma T)$  versus  $10^3/T$  data resulted in a linear relation for each of these data sets. Of these three, data set 15 was selected as the one on which to base the evaluated data; the standard deviation of the data about the regression line is  $3.27 \times 10^{-2}$  for the fit to the linear form  $\log(\sigma T)$  versus  $10^3/T$ . Data set 7 was not used since it is higher than the other two sets and has more scatter. Of the remaining two sets, data set 15 has slightly less scatter and was, therefore, selected. The difference between the evaluated data and the conductivity data for curve 15 can be as high as 10%. Furthermore, even though the data in table 6.1 can be regarded as

evaluated data, it should be recognized that systematic variations from sample to sample can be large for pure sodium chloride. The difference between the evaluated data for conductivity and curve 9 can be as high as 15% while for curve 7 it is typically 45%.

Additional data for the electrical conductivity of solid sodium chloride appear in references [15-30]. A review article of ionic conductivity in solids [31] reports both general references as well as references pertaining to sodium chloride.

#### 6.3.2. Liquid State, Temperature Dependence

Evaluated data are given for the electrical conductivity of liquid sodium chloride. The evaluated data are given in table 6.3 and are shown in figure 6.2 which shows the general trend of the data. Data from references [32 and 33] formed the general base on which the evaluated data were developed and table 6.4 gives the experimental data from these references. A discussion of how the evaluation was arrived at follows.

The evaluated data for the electrical conductivity of liquid sodium chloride were specifically based on the data of Ketelaar and Maenaut [33] (curve 2) because their use of the capillary U-type cell in air did not involve parasitic conduction. On figure 6.2, it is noted that the data of Van Artsdalen and Yaffe [32] (curve 1) is higher than the data of Ketelaar and Maenaut [33] (curve 2) in the higher temperature region. Also shown are data of Ketelaar and Maenaut [33] (curves 3 and 4) taken with a dip cell with these data higher than their data taken with the U-type cell in air. These higher data have been demonstrated to be due to parasitic conduction, i.e., the cell walls conduct when using the dip-type design for the measurements, which leads to a higher conductivity [33 and 46, pp. 875-6]. The result of a least-squares fit to the data of Ketelaar and Maenaut (data set 2) was

$$\sigma = -3.9323 \times 10^2 + 11.269 \times 10^{-1}T$$
  
-3.9452 × 10<sup>-4</sup>T<sup>2</sup> (6.2)

(T in K and  $\sigma$  in S m<sup>-1</sup>) which is valid over the temperature range of 1090 K to 1300 K. The computer program LSPE, which was previously described in the discussion of the temperature dependence of the electrical conductivity of solid sodium chloride, was used for the least-squares fit. The standard deviation of the



FIGURE 6.2. Electrical conductivity of liquid sodium chloride.

TABLE 6.3. EVALUATED DATA FOR THE ELECTRICAL CONDUCTIVITY OF LIQUID SODIUM CHLORIDE

[Temperature, T, K; Electrical Conductivity,  $\sigma$ , S m<sup>-1</sup>]

Т	σ
1090	366.4
1100	369.0
1200	390.9
1300	405.0

TABLE 6.4. EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF LIQUID SODIUM CHLORIDE

[Temperature, T,K; Electrical Conductivity,  $\sigma$ , S m<sup>-1</sup>]

Data Set	Author(s), Year [Ref.]	Т	σ	Remarks
1	Van Artsdalen, E.R. and Yaffe, I.S., 1955 [32]	1075.4 1077.8 1079.6 1079.6 1081.2 1081.4 1091.0 1091.0 1100.6 1113.0 1131.0 1144.6 1165.8 1172.6 1184.6 1186.4 1195.6 1206.4 1207.0 1220.4 1244.6 1245.2 1245.4 1280.0 1283.2 1294.6	308.87 344.97 358.04 358.21 360.57 360.60 364.31 364.41 366.01 371.45 376.62 380.41 385.02 386.37 391.54 391.29 394.16 396.80 397.01 401.51 406.53 406.16 407.19 415.95 417.01 418.01	100 NaCl; liquid state; quartz dip-type cap- illary conductance cell used for measurements; resistance measured using Leeds and Northrup precision "Jones" bridge with frequencies of 200 to 20,000 Hz and a variation in resistance $\langle 0.5\%$ ; linear extrapolation to infinite fre- quency made of measured resistance versus frequency <sup>-2</sup> to obtain inductance-free resis- tance; cell constant order of 300-500 cm <sup>-1</sup> and recalibration after 2 or 3 days use showed constant did not change by more than 0.3% and on average about 0.1%; cell calibrated in demal aqueous potassium chloride solution at 298 K; temperature could be maintained to better than ±0.1 K up to 1273 K with a thermal gradient of no more than 0.2 K over height of melt, usually about 6.35 cm (2.5 in); data taken going up and down in temperature scale, no difference observed in measurements; data extracted from table; authors presented equa- tion for conducting as $\sigma = -0.1697 + 0.6259t -$ $1.953t^2$ , $\sigma \text{ in } \Omega^{-1} \text{ cm}^{-1}$ , t in °C, std dev = $0.006 \ \Omega^{-1} \text{ cm}^{-1}$ , and valid within 1083-1303 K.
2	Ketelaar, J.A.A. and Maenaut, P.P.E., 1972 [33]	1093 1093 1103 1103 1113 1123 1123 1123 1123 1125.6 1133 1143 1143 1148 1148 1173.6 1198 1223 1273 1273 1273 1298	367.2 367.65 371.1 369.4 370.25 373.7 372.9 373.77 372.9 374.0 376.5 376.2 378.4 382.5 379.6 385.3 387.1 391.4 394.1 395.1 395.6 398.5 402.2 401.1 402.6 404.5	Each impurity does not exceed 0.003%; Baker analyzed reagent; liquid state; capillary U- type cell in air used; cell constant 2500 cm <sup>-1</sup> and determined using a normal solution of po- tassium chloride at 298 K; cell constant checked after every series of measurements, variation never exceeded 3%; resistances mea- sured at a frequency of 10 hHz; higher values of measurements using dip-cell explained as due to parasitic conduction; data extracted from table.

Data Set	Author(s), Year [Ref.]	Т	σ	Remarks
3	Ketelaar, J.A.A. and Maenaut, P.P.E., 1972 [33]	1223.3 1272.9	446.5 469.8	Similar to the above specimen and conditions except dip-cell used, cell constant 2520 cm <sup>-1</sup> , and data extracted from figure.
4	Ketelaar, J.A.A. and Maenaut, P.P.E., 1972 [33]	1113.3 1173.5	376.9 400.2	Similar to the above specimen and conditions except cell constant 1520 cm <sup>-1</sup> .

TABLE 6.4. EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF LIQUID SODIUM CHLORIDE (continued)

data about the regression line is  $1.01 \times 10^{-2}$ . The uncertainty assigned to the evaluated data is  $\pm 3\%$  because Ketelaar and Maenaut found a variation of the cell constants within that value.

Additional data for the electrical conductivity of liquid sodium chloride appears in references [34-44]. Two documents which give a compilation of information and an assessment of the data are references [45 and 46].

#### 6.3.3. Solid State, Pressure Dependence

Selected experimental data are given for the pressure dependence of the electrical conductivity of solid sodium chloride. These selected data are given in table 6.5 and are shown in figure 6.3.

Pierce [47] (curves 1-6) reported extensive data for doped sodium chloride. Shimizu [13] (curves 7-10) reported data over a lesser range of pressure for a single crystal. Observation of these data on figure 6.3 which are plotted as log  $\sigma$  as a function of pressure shows that above 550 K there is a single straight line that would be applicable to the data at each temperature.

Other investigators have contributed information to the pressure dependence of the electrical conductivity. Beyeler and Lazarus [14] presented data for single crystal sodium chloride at 923 K and at 953 K for log  $(\sigma T)$  as a function of pressure. Cleaver et al. [48] reported data at 1093 K but the data were presented on the log  $\sigma$  axis such that absolute values cannot be determined. Biermann [21] presented data for the resistance ratio as a function of pressure and, in addition, data for the pressure coefficient of electrical conductivity as a function of temperature. Another data source for the pressure dependence of the electrical conductivity is reference [49]. Murri and Doran [59] studied the effects of shock waves on the electrical conductivity of sodium chloride. Homan et al. [125] reported the conductivity ratio as a function of pressure.

Evaluated data are not given for the pressure dependence of the electrical conductivity because of the

lack of confirmatory data on well-characterized materials.

#### 6.3.4. Aqueous Solutions

Data for the electrical conductivity of aqueous solutions of sodium chloride for various concentrations and temperatures appear in references [50-56]. Two early compilations appear in references [57 and 58].

## 6.4. Dielectric Constant

#### 6.4.1. Real Part of the Dielectric Constant

Evaluated data are given for the real part of the dielectric constant of pure sodium chloride in table 6.6 and are shown on figure 6.5. Figure 6.4 shows the frequency dependence over a range of  $1 \times 10^2$  Hz to  $2.5 \times 10^{10}$  Hz and figure 6.5 shows the temperature dependence. The curves shown on these two figures come from references [60–67] and have been selected to show various characteristics including the variation at room temperature for pure sodium chloride and for naturally occurring samples. The numerical data, together with information on sample characterization, for the curves shown on the two figures are given in table 6.7.

The data in figure 6.4 show interesting features. The measurements of the Laboratory for Insulation Research [60] (curve 1) made at room temperature on a commercial crystal from Harshaw show that the data are constant. The data of the Laboratory for Insulation Research [60] (curve 2) and of Breckenridge [61] (curve 3) are also for Harshaw crystals with the measurement temperature 358 K. The data for both curves are close to each other and show an upturn as the frequency is decreased below 104 Hz. Above that frequency the data are constant to 10<sup>10</sup> Hz. This rise at low frequencies is due to interfacial polarizability which is not included in the real part of the dielectric constant [69, pp. 316-7]. Data for halite cored from a Carlsbad, New Mexico corehole are given in ref. [127] for four subsamples and show a variation of 106 Hz from 7.012 to 8.705.



FIGURE 6.3. Electrical conductivity of solid sodium chloride (pressure dependence).

## TABLE 6.5. EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF SOLID SODIUM CHLORIDE (Pressure Dependence)

[Pressure, P,MPa; Electrical Conductivity,  $\sigma$ , S m<sup>-1</sup>]

Data Set	Author(s), Year [Ref.]	Ρσ	Remarks
1	Pierce, C.B., 1961 [47]	(T=473 K) 0.0 -5.949 199.6 -6.347 394.8 -6.545 598.6 -6.759 810.8 -6.957	0.02 mole percent CaCl <sub>2</sub> ; crystal grown by Kyropoulos method; measurements made using ac bridge technique with 1 hHz input to a General Radio 706 capacitance bridge; measurement tem- perature 473 K.
2	Pierce, C.B., 1961 [47]	(T=513 K) 4.2 -5.196 250.5 -5.523 458.5 -5.793 636.8 -5.977 891.5 -6.233	The above specimen and conditions except mea- surement temperature 513 K.
3	Pierce, C.B., 1961 [47]	(T=594 K) 297.1 -4.259 598.6 -4.500 908.5 -4.756	The above specimen and conditions except mea- surement temperature 594 K.
4	Pierce, C.B., 1961 [47]	(T=773 K) 573.1 -2.767 755.7 -2.866	The above specimen and conditions except mea- surement temperature 773 K.
5	Pierce, C.B., 1961 [47]	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	0.09 mole percent CaCl <sub>2</sub> ; crystal grown by Kyropoulos method; measurements made using ac bridge technique with 1 hHz input to a General Radio 706 capacitance bridge; measurement tem- perature 481 K.
6	Pierce, C.B., 1961 [47]	(T=773 K) 302.7 -2.011 588.5 -2.167 844.5 -2.337	The above specimen and conditions except mea- surement temperature 773 K.
7	Shimizu, K., 1962 [13]	(T=473 K) 0.4 -7.962 19.5 -7.988 38.6 -8.003 58.9 -8.017	Single crystal prepared by Kyropoulos method; specimen 1 mm by 5 mm by 8 mm; annealed in NaCl powder at 873 K for 6 h and slowly coded to room temperature; electrodes applied with silver paint; conductivity measurements made for increasing and decreasing pressures by means of a capacitance bridge at 1 hKz at con- stant temperature; specimen compressed in a silicone oil by an oil injector and pressure measured with a calibrated Bourdon-type gauge; data points extracted from figure; measurement temperature 473 K.

Data Set	Author(s), Year [Ref.]	Р	σ	Remarks
8	Shimizu, K., 1962 [13]	(T=) 0.9 19.9 39.5 59.2	533 K) -5.680 -5.702 -5.720 -5.738	The above specimen and conditions except measurement temperature 533 K.
9	Shimizu, K., 1962 [13]	(T=) 0.9 20.2 39.5 59.5	553 K) -5.371 -5.388 -5.406 -5.425	The above specimen and conditions except measurement temperature 553 K.
10	Shimizu, K., 1962 [13]	(T=5 0.6 20.4 40.1 59.5	573 K) -5.120 -5.136 -5.158 -5.172	The above specimen and conditions except measurement temperature 573 K.

TABLE 6.5. EXPERIMENTAL DATA ON THE ELECTRICAL CONDUCTIVITY OF SOLID SODIUM CHLORIDE (Pressure Dependence) (continued)



FIGURE 6.4 Real part of the dielectric constant of sodium chloride (frequency dependence).



FIGURE 6.5. Real part of the dielectric constant of sodium chloride (temperature dependence).

## TABLE 6.6. EVALUATED DATA FOR THE REAL PART OF THE DIELECTRIC CONSTANT OF PUKE SODIUM CHLORIDE

[Frequency,  $\nu,$  Hz; Temperature, T, K; Real Part of the Dielectric Constant,  $\epsilon^{\,\prime}]$ 

ν	ε	1
	T = 298K	T = 358K
$1 \times 10^{2}$	5.90	6.01
1 x 10 <sup>3</sup>	5.90	6.01
$1 \times 10^{4}$	5.90	6.01
$1 \times 10^{5}$	5.90	6.01
$1 \times 10^{6}$	5.90	6.01
$1 \times 10^{7}$	5.90	6.01
$1 \times 10^{8}$	5.90	6.01
1 x 10 <sup>9</sup>	5.90	6.01
$1 \times 10^{10}$	5.90	6.01

## TABLE 6.7. EXPERIMENTAL DATA FOR THE REAL PART OF THE DIELECTRIC CONSTANT OF SODIUM CHLORIDE

[Frequency, v,Hz; Temperature, T,K; Real Part of the Dielectric Constant,  $\epsilon'$ ]

Data Set	Author(s), Year [Ref.]	ν	ε'	Remarks
1	Laboratory for Insulation Research, 1954 [60]	(T=298 K 1 x 10 <sup>2</sup> 1 x 10 <sup>3</sup> 1 x 10 <sup>4</sup> 1 x 10 <sup>5</sup> 1 x 10 <sup>6</sup> 1 x 10 <sup>7</sup> 2.5 x 10 <sup>10</sup>	) 5.90 5.90 5.90 5.90 5.90 5.90 5.90	Fresh crystals from Harshaw; dried over phosphorus pentoxide; data extracted from table.
2	Laboratory for Insulation Research, 1954 [60]	(T=358 K) $1 \times 10^{2}$ $1 \times 10^{3}$ $1 \times 10^{4}$ $1 \times 10^{5}$ $1 \times 10^{6}$ $1 \times 10^{7}$ $2.5 \times 10^{10}$ * Not shown i	) 6.35 6.11 6.00 5.98* 5.98* 5.98* 5.97* n figure.	Fresh crystals from Harshaw; dried over phosphorus pentoxide; data extracted from table.
3	Breckenridge, R.G., 1948 [61]	(T=358  K) 9.86 x 10 9.54 x 10 <sup>2</sup> 1.17 x 10 <sup>4</sup> 1.14 x 10 <sup>5</sup> 9.81 x 10 <sup>5</sup> 9.53 x 10 <sup>6</sup> 8.21 x 10 <sup>7</sup> 8.71 x 10 <sup>9</sup>	6.36* 6.09 5.98 5.98 5.92* 5.97 5.96 5.95	Commercial crystal from Harshaw Chemical Co., Cleveland, Ohio; specimen approx 0.5 in square and about 0.020 in thick; electrodes applied by painting crystal faces with duPont Silver Paste No. 4351; probable error about 2%; data extracted from figure.
		* Not shown in T	figure. ε'	
4	DeGiura, V. and Spinolo, G., 1968 [62]	(v=5x10 <sup>3</sup> ) 293	Hz) 5.92	Measurement method used a three-terminal system kept under vacuum, General Radio 1615A bridge used; data extracted from table; data reported is average on sev- eral specimens with maximum variance within $\pm 0.02$ ; temperature specified as room temperature, 293 K assigned.
5	Lowndes, S., 1966 [63]	(v=10 <sup>2</sup> −10 <sup>6</sup> 1.5 90 290	Hz) 5.43 5.57 5.90	Optically flat single crystal discs with vacuum-deposited gold electrodes on the faces; measurements made in a three-terminal cell system with frequency at $10^2$ to $10^6$ Hz; crystals showed no impurity polarization mechanisms; uncertainty $\pm 0.02$ at the three temperatures; data extracted from table.
6	Haussühl, S., 1957 [64]	(v=10 <sup>5</sup> -2x10 293	<sup>7</sup> Hz) 5.87	Single crystal; measurements conducted in a frequency range of $10^5$ to 2 x $10^7$ Hz and in a temperature range of 293 to 383 K; measurement temperature applying

Data Set	Author(s), Year [Ref.]	Т	ε'	Remarks
6 (cont.)	Haussühl, S., 1957 [64]			to tabular data not explicitly stated, 293 K assumed.
7	Jones, B.W., 1967 [65]	(v=1x10 <sup>3</sup> ) 296	Hz) 5.86	Naturally occurring sample; 0.7 ppm divalent ions; single crystal; flat plate specimen of about 1.0 cm x 1.0 cm x 0.1 cm with metallic electrodes put on; dielectric constant measured using a geo- metrical technique in association with a three terminal transformer bridge system; pressures up to 7 kbars used; low fre- quency dielectric constant at zero pressure reported; data extracted from table; uncertainty 1% or less.
8	Eucken, A. and Buchner, A., 1935 [66]	293	5.62	Slab specimen; from natural crystal; data extracted from table; uncertainty ±0.01.
9	Matsonashvile, B.N., 1958 [67]	$(v=8.50 \times 10^{5})$ 304 307 313 318 327 339 348 357 367 374 383 392 399 407 416 432 446 462 474 482 500 514	Hz) 5.72 5.73 5.73 5.75 5.76 5.79 5.80 5.81 5.83 5.84 5.83 5.84 5.87 5.88 5.89 5.90 5.94 5.95 5.99 6.00 6.02 6.08 6.10	Single crystal; grown by Kyropoulos tech- nique; slabs sawed from crystals by using water-wetted wire saw; ground and polished using dehydrated alcohol to disk shape; plane parallel to within 1-2 µm; trans- parent and crossed polaroids showed no perceptible internal stresses; measured in vacuum; data extracted from smooth curve.

The data in figure 6.5 show several features. There is a spread in the data at room temperature for pure material (curves 4, 5, 6, and 9). The data of Lowndes [63] (curve 5) show the variation with temperature for temperatures below room temperature. Above room temperature the data of Matsonashvili [67] (curve 9) appear to show a variation that increases faster than linearly at the higher temperatures. Naturally occurring specimens also have a spread (curves 7 and 8).

The evaluated data for the real part of the dielectric constant at room temperature were based on data set 1 in figure 6.4 and confirmatory evidence given in reference [74, table IV-1] for the room temperature values at 8.9, 35.4, and 116 GHz which were all 5.90. The values up to 358 K were based on data set 2 together with information on the slope from data sets 5 and 9 as well as information on the temperature coefficient quoted in reference [74, table IV-3]. The evaluated data for pure sodium chloride are given in table 6.6 and between 298 K and 358 K are represented by

$$\epsilon' = 5.354 + 0.001833 T \tag{6.3}$$

with T in K. Considering the difference between equation (6.3) and the data of curve 9, an uncertainty of 3.5% is assigned to  $\epsilon'$ .

Additional data for the real part of the dielectric constant appear in references [68, 70-74, 76, and 80], with reference [12] containing data for doped sodium

chloride, halite, granulated purified salt, and fine flake salt. Data over a frequency range of 2.96×1012 Hz to 1.17  $\times 10^{13}$  Hz appear in reference [79] and were calculated from the magnitude and phase angle of the reflectance which was measured at 300 K. Data for a 10% solution are reported in reference [78]. Data for the temperature coefficient of the real part of the dielectric constant appear in references [66, 74, 75, and 80] and data on the rate of change with temperature appear in reference [76]. Data for pressure coefficient appear in references [77 and 80], on the rate of change with pressure in references [76], and the variation with pressure in reference [65]. In reference [80] measurements of the real part of the dielectric constant, its pressure and temperature coefficients, were performed on the same samples.

#### 6.4.2. Tangent of the Loss Angle

Selected experimental data are given for the tangent of the loss angle, tan  $\delta$ , of sodium chloride. These selected data are tabulated in table 6.8 with the frequency dependence shown in figure 6.6 and the temperature dependence shown in figure 6.7.

The frequency dependence, figure 6.6, contains some general features for various conditions. There are several curves for the pure material. The results reported by Haven [82 and 83] (curve 5) were for a very pure single crystal measured at a temperature of 383 K with the data decreasing from  $1.55 \times 10^{-4}$  at 52.3 Hz to  $4.44 \times 10^{-5}$  at  $1.04 \times 10^{5}$  Hz. Nearby at  $1 \times 10^{6}$  Hz is the data point reported by Vodop'ianov and Galibina [85] (curve 8) which applies to a pure specimen at 293 K. In a higher frequency range, the data also of Vodop'ianov and Galibina [85] (curve 9) show data for pure material generally decreasing and going from  $1.36 \times 10^{-4}$  at  $1.718 \times 10^5$  Hz to  $2.3 \times 10^{-5}$  at  $1 \times 10^7$  Hz. Similarly, a decrease in tan  $\delta$  with an increase in frequency is evident for the data of Bayley [84] (curve 7) which apply to pure rock salt; the values are higher than for the pure material. The data of Nevald [86] (curve 1) and of Breckenridge [61] (curve 6) both show an increase in tan  $\delta$  at the upper end of their respective frequency intervals; the former data apply to an unstrained specimen of sodium chloride with the upturn starting at  $1 \times 10^{6}$  Hz and the latter data apply to a commercial crystal from Harshaw with the increase applying to the last point at  $7.64 \times 10^9$  Hz. The data for the Harshaw crystal are higher than the data for the unstrained crystal.

Specimens with doping or dislocations show some interesting features. The data of Radhakrishna and Karguppikar [2] (curves 3 and 4) apply to Sb-doped sodium chloride crystal with curve 3 for a temperature of 393 K and curve 4 for a temperature of 493 K. The magnitude of tan  $\delta$  is higher than for previous curves discussed. Nevald [81] (curve 2) reported data for a specimen having a dislocation density of  $5 \times 10^9$  cm<sup>-2</sup> and the shape of the curve is concave downward. Data for halite cored from a Carlsbad, New Mexico corehole is given in ref. [127] for four subsamples and show a variation in tan  $\delta$  of:

Hz	Variation	$\mathbf{i}\mathbf{n}$	$\tan\delta$

10	1.1411 to 3.3953
$10^{3}$	0.2909 to 0.4997
$10^{4}$	0.4239 to 0.6510
106	0.2175 to 0.3639

The temperature dependence, figure 6.7, shows the general trend of the data and illustrates the point that data for pure specimens have lower values of tan  $\delta$  compared to specimens with impurities (compare curves 10, 15-17 with curves 11 and 12), and illustrates the effect of frequency (curves 13 and 14) with the higher frequency giving higher values of tan  $\delta$ 

Evaluated data are not given for tan  $\delta$  because of the large change in tan  $\delta$  caused by impurities and the lack of confirmatory evidence on well-characterized materials.

Documents containing additional data of tan  $\delta$  in addition to the particular data sets discussed above are references [2,11,12,60,67,74,81-9].

## 6.5. Dielectric Strength

Evaluated data for the dielectric strength of bulk, pure, unstrained sodium chloride are given in table 6.9. Figure 6.8 shows the temperature dependence of the dielectric strength and figure 6.9 shows the thickness dependence. Table 6.10 contains the numerical data, together with information on sample characterization, for the curves shown on the two figures. Before stating the basis of the evaluated data, a discussion of some features of the data is given.

There are several noteworthy characteristics of the temperature dependence of the dielectric strength. The dielectric strength increases in value from low temperatures to reach a maximum slightly above room temperature and then decreases (curves 1, 4, 11, and 12).

The data at room temperature show quite a variation. Nevald [81] (data set 1) reported a value of  $139 \text{ MV m}^{-1}$ at 302 K for a sodium chloride single crystal. von Hippel and Lee [90] (data set 4) gave 164.7 MV m<sup>-1</sup> at 295.5 K for pure sodium chloride. Caspari [91] (data set 8) reported a value of 146 MV m<sup>-1</sup> at 296 K for a single crystal from Harshaw Chemical Co. with the applied field in the [100] direction; in contrast, he reported 142 MV m<sup>-1</sup> for the field in the [110] direction (data set 9). The



FIGURE 6.6. Tangent of the loss angle of sodium chloride (frequency dependence).



FIGURE 6.7. Tangent of the loss angle of sodium chloride (temperature dependence).

TABLE	6.8.	EXPERI	IMENTAL	DATA	FOR	THE	TANG	ENT	OF	THE	LOSS	ANGL	E OF	F S(	DIUM	CHLORID	E
	[Frequ	iency,	v,Hz;	Temper	atur	e, 1	Г,К;	Tang	ent	of	the	Loss	Angl	Le,	tan d	5]	

Data Set	Author(s), Year [Ref.]	ν	tan ó	Remarks
1	Nevald, R., 1964 [81]	$(T = 2.36 \times 10^{2})$ $2.70 \times 10^{2}$ $3.31 \times 10^{2}$ $4.06 \times 10^{2}$ $4.97 \times 10^{2}$ $6.09 \times 10^{2}$ $9.14 \times 10^{2}$ $1.12 \times 10^{3}$ $1.37 \times 10^{3}$ $1.47 \times 10^{3}$ $1.47 \times 10^{3}$ $1.92 \times 10^{3}$ $2.52 \times 10^{3}$ $3.30 \times 10^{3}$ $4.33 \times 10^{3}$ $5.67 \times 10^{3}$ $7.95 \times 10^{3}$ $8.50 \times 10^{3}$ $1.27 \times 10^{4}$ $2.05 \times 10^{4}$ $3.51 \times 10^{4}$ $4.92 \times 10^{4}$ $7.37 \times 10^{4}$ $1.45 \times 10^{5}$ $2.66 \times 10^{5}$ $1.02 \times 10^{6}$ $3.22 \times 10^{6}$ $5.92 \times 10^{6}$ $1.09 \times 10^{7}$ $1.86 \times 10^{7}$	293 K) $3.45 \times 10^{-4}$ $3.19 \times 10^{-4}$ $2.99 \times 10^{-4}$ $2.99 \times 10^{-4}$ $2.73 \times 10^{-4}$ $2.44 \times 10^{-4}$ $2.18 \times 10^{-4}$ $1.86 \times 10^{-4}$ $1.73 \times 10^{-4}$ $1.60 \times 10^{-4}$ $1.50 \times 10^{-4}$ $1.50 \times 10^{-4}$ $1.34 \times 10^{-4}$ $1.04 \times 10^{-4}$ $0.915 \times 10^{-4}$ $0.850 \times 10^{-4}$ $0.720 \times 10^{-4}$ $0.687 \times 10^{-4}$ $0.363 \times 10^{-4}$ $0.364 \times 10^{-4}$ $0.364 \times 10^{-4}$ $0.332 \times 10^{-4}$ $0.332 \times 10^{-4}$ $0.333 \times 10^{-4}$ $0.369 \times 10^{-4}$ $0.332 \times 10^{-4}$ $0.333 \times 10^{-4}$ $0.464 \times 10^{-4}$ $0.599 \times 10^{-4}$ $0.599 \times 10^{-4}$ $0.599 \times 10^{-4}$ $0.369 \times 10^{-4}$ $0.369 \times 10^{-4}$ $0.332 \times 10^{-4}$ $0.369 \times 10^{-4}$ $0.369 \times 10^{-4}$ $0.599 \times 10^{-4}$ $0.593 \times 10^{-4}$	NaCl unstrained; flat specimen 2.5 x l x 0.1 cm <sup>3</sup> cleaved from blanks, gold electrodes evaporated over both sides, and tin foil pasted to the gold electrodes with low-loss oil; smooth data extracted from figure; measurement temperature specified as room temperature, 293 K assigned.
2	Nevald, R., 1964 [81]	$(T = 1.31 \times 10^{3})^{3}$ $1.71 \times 10^{3}$ $2.55 \times 10^{3}$ $4.34 \times 10^{3}$ $8.45 \times 10^{3}$ $1.10 \times 10^{4}$ $1.14 \times 10^{4}$ $1.76 \times 10^{4}$ $1.76 \times 10^{4}$ $3.00 \times 10^{4}$ $3.67 \times 10^{5}$ $1.14 \times 10^{5}$ $1.95 \times 10^{5}$ $2.23 \times 10^{5}$ $2.91 \times 10^{5}$ $3.81 \times 10^{5}$ $4.35 \times 10^{5}$ $5.69 \times 10^{5}$	293 K) 2.36 $\times 10^{-4}$ 2.62 $\times 10^{-4}$ 3.21 $\times 10^{-4}$ 4.06 $\times 10^{-4}$ 5.04 $\times 10^{-4}$ 5.73 $\times 10^{-4}$ 5.70 $\times 10^{-4}$ 5.76 $\times 10^{-4}$ 5.89 $\times 10^{-4}$ 5.89 $\times 10^{-4}$ 5.89 $\times 10^{-4}$ 5.90 $\times 10^{-4}$ 6.03 $\times 10^{-4}$ 6.03 $\times 10^{-4}$ 6.29 $\times 10^{-4}$ 6.42 $\times 10^{-4}$ 6.36 $\times 10^{-4}$ 6.23 $\times 10^{-4}$	Similar to the above specimen and conditions except dislocation density 5 x 10 <sup>9</sup> cm <sup>-2</sup> and specimen designated as I.

Data Set	Author(s), Year [Ref.]	ν	tan δ	Remarks				
2 (cont.)	Nevald, R., 1964 [81]	$7.44 \times 10^{5}$ $9.09 \times 10^{5}$ $1.78 \times 10^{6}$ $4.26 \times 10^{6}$ $6.81 \times 10^{6}$ $1.02 \times 10^{7}$ $1.74 \times 10^{7}$ $2.44 \times 10^{7}$	$\begin{array}{c} 6.10 \times 10^{-4} \\ 5.97 \times 10^{-4} \\ 5.25 \times 10^{-4} \\ 4.34 \times 10^{-4} \\ 3.89 \times 10^{-4} \\ 3.37 \times 10^{-4} \\ 2.85 \times 10^{-4} \\ 2.52 \times 10^{-4} \end{array}$					
3	Radhakrishna, S. and Karguppikar, A.M., 1973 [2]	$(T = 1.25 \times 10^{2})$ $1.68 \times 10^{2}$ $2.26 \times 10^{2}$ $2.52 \times 10^{2}$ $2.81 \times 10^{2}$ $3.92 \times 10^{2}$ $5.36 \times 10^{2}$ $5.88 \times 10^{2}$ $6.45 \times 10^{2}$ $7.47 \times 10^{2}$ $8.20 \times 10^{2}$ $1.02 \times 10^{3}$ $1.40 \times 10^{3}$ $2.02 \times 10^{3}$ $2.57 \times 10^{3}$	393 K) $1.05 \times 10^{-1}$ $7.30 \times 10^{-2}$ $5.56 \times 10^{-2}$ $5.57 \times 10^{-2}$ $5.78 \times 10^{-2}$ $4.02 \times 10^{-2}$ $2.96 \times 10^{-2}$ $2.96 \times 10^{-2}$ $2.29 \times 10^{-2}$ $1.95 \times 10^{-2}$ $1.63 \times 10^{-2}$ $1.36 \times 10^{-2}$ $9.62 \times 10^{-3}$ $5.80 \times 10^{-3}$	NaCl crystals doped with Sb; crystals grown from melt by Kyropoulos tech- nique starting with BDH-AR grade salt Sb then diffused by heating the crystal in Sb vapor at 973 $\pm$ 5 K for about 6 days, the NaCl and Sb metal sealed together in quartz tube after evacuating to approx 10 <sup>-3</sup> torr; im- purity content estimated by mass spectroscopic analysis; before mea- surements crystals quenched from approx 673 K; for measurements thin coating of aquadog made and crystals held in vacuum of 10 <sup>-2</sup> torr; in mea- surements made by GR 1615-A capaci- tance bridge combined with GR 1311-A Audio Oscillator, for higher fre- quencies a PM 5100 Philips Oscillator used in conjunction with capacitance bridge; data points of log(tan $\delta$ ) versus log(frequency) extracted from figure.				
4	Radhakrishna, S. and Karguppikar, A.M., 1973 [2]	$(T = 6.47 \times 10^{3})$ $7.50 \times 10^{3}$ $8.70 \times 10^{3}$ $9.71 \times 10^{3}$ $1.05 \times 10^{4}$ $2.03 \times 10^{4}$ $2.58 \times 10^{4}$ $5.30 \times 10^{4}$ $1.03 \times 10^{4}$	493 K) 7.26 $\times 10^{-1}$ 5.84 $\times 10^{-1}$ 4.96 $\times 10^{-1}$ 4.37 $\times 10^{-1}$ 3.78 $\times 10^{-1}$ 1.77 $\times 10^{-1}$ 1.71 $\times 10^{-1}$ 7.69 $\times 10^{-2}$ 3.60 $\times 10^{-2}$	Similar to the above specimen and conditions.				
5	Haven, Y., 1953 [82,83]	$(T = 5.23 \times 10)$ $7.56 \times 10$ $1.02 \times 10^{2}$ $1.36 \times 10^{2}$ $1.97 \times 10^{2}$ $2.85 \times 10^{2}$ $4.60 \times 10^{2}$ $6.90 \times 10^{2}$ $9.98 \times 10^{2}$ $1.44 \times 10^{3}$ $1.87 \times 10^{3}$ $2.80 \times 10^{3}$ $4.36 \times 10^{3}$ $7.30 \times 10^{3}$	383 K) $1.55 \times 10^{-4}$ $1.34 \times 10^{-4}$ $1.24 \times 10^{-4}$ $1.11 \times 10^{-4}$ $9.95 \times 10^{-5}$ $8.58 \times 10^{-5}$ $7.98 \times 10^{-5}$ $7.14 \times 10^{-5}$ $6.64 \times 10^{-5}$ $6.17 \times 10^{-5}$ $5.94 \times 10^{-5}$ $5.32 \times 10^{-5}$ $5.32 \times 10^{-5}$ $4.95 \times 10^{-5}$	Very pure; single crystal; smooth data extracted from figure.				

Data Set	Author(s), Year [Ref.]	ν	tan δ	Remarks
5 (cont.)	Haven, Y., 1953 [82,83]	$\begin{array}{c} 1.02 \times 10^{4} \\ 1.70 \times 10^{4} \\ 2.75 \times 10^{4} \\ 5.14 \times 10^{4} \\ 7.71 \times 10^{4} \\ 1.04 \times 10^{5} \end{array}$	$\begin{array}{r} 4.95 \times 10^{-5} \\ 4.77 \times 10^{-5} \\ 4.78 \times 10^{-5} \\ 4.44 \times 10^{-5} \\ 4.44 \times 10^{-5} \\ 4.44 \times 10^{-5} \end{array}$	
6	Breckenridge, R.G., 1948 [61]	$(T = 1.09 \times 10^{2})$ $1.20 \times 10^{3}$ $1.03 \times 10^{4}$ $1.00 \times 10^{5}$ $1.09 \times 10^{6}$ $9.42 \times 10^{6}$ $8.11 \times 10^{7}$ $7.64 \times 10^{9}$	$358 \text{ K})$ $1.11 \times 10^{-2}$ $1.19 \times 10^{-2}$ $8.93 \times 10^{-3}$ $3.58 \times 10^{-3}$ $6.35 \times 10^{-4}$ $3.68 \times 10^{-4}$ $3.68 \times 10^{-4}$ $3.04 \times 10^{-3}$	Commercial crystal from Harshaw Chemical Co., Cleveland, Ohio; spec- imen approx 0.5 in square and about 0.020 in thick; electrodes applied by painting crystal faces with duPont Silver Paste No. 4351; prob- able error $\pm 0.0003$ ; data extracted from figure except max tan $\delta$ at 600 Hz from text.
7	Bayley, P.L., 1933 [84]	$(T = 1.04 \times 10^{3})$ $1.14 \times 10^{3}$ $2.04 \times 10^{3}$ $2.86 \times 10^{3}$ $3.43 \times 10^{3}$ $1.33 \times 10^{5}$ $1.46 \times 10^{5}$ $1.98 \times 10^{5}$ $2.30 \times 10^{5}$	293 K) $3.50 \times 10^{-4}$ $3.41 \times 10^{-4}$ $3.18 \times 10^{-4}$ $3.08 \times 10^{-4}$ $3.02 \times 10^{-4}$ $1.65 \times 10^{-4}$ $1.58 \times 10^{-4}$ $1.49 \times 10^{-4}$ $1.49 \times 10^{-4}$	Pure rock salt; specimen 0.9 mm thick; sawed from larger block almost par- allel to natural cleavage planes; from Ward's Natural Science Estab- lishment; colored amber by 40 min exposure to x-rays; data points, before and after exposure to x-rays, extracted from figure; no difference in data noted due to x-ray exposure; temperature assumed to be 293 K.
8	Vodop'ianov, K.A. and Galibina, G.I., 1958 [85]	$(T = 1 \times 10^{6})$	293 K) 6.4 x 10 <sup>-5</sup>	Pure; grown by Kyropoulos method from melt of chemically pure material; data extracted from table; measure- ment temperature specified as room temperature, 293 K assigned.
9	Vodop'ianov, K.A. and Galibina, G.I., 1958 [85]	$(T = 1.718 \times 10^{5})$ 3.784 × 10 <sup>5</sup> 6.714 × 10 <sup>5</sup> 2.158 × 10 <sup>6</sup> 7.998 × 10 <sup>6</sup> 1.00 × 10 <sup>7</sup>	293 K) $1.36 \times 10^{-4}$ $9.6 \times 10^{-5}$ $5.5 \times 10^{-5}$ $3.0 \times 10^{-5}$ $3.1 \times 10^{-5}$ $2.3 \times 10^{-5}$	Pure; grown by Kyropoulos method from melt of chemically pure material; data extracted from figure; measure- ment temperature presumably room temperature, 293 K assigned.
		<u>T</u>	<u>tan δ</u>	
10	Breckenridge, R.G., 1950 [86]	(v = 1) 303.9 305.9 310.6 313.0 315.8 318.1 322.1 324.9 329.2 333.5 338.7 347.0 356.4	$ \begin{array}{c} \times 10^{3} \text{ Hz} ) \\ 8.6 \times 10^{-4} \\ 9.4 \times 10^{-4} \\ 1.03 \times 10^{-3} \\ 1.11 \times 10^{-3} \\ 1.11 \times 10^{-3} \\ 1.27 \times 10^{-3} \\ 1.51 \times 10^{-3} \\ 1.67 \times 10^{-3} \\ 2.14 \times 10^{-3} \\ 2.46 \times 10^{-3} \\ 3.01 \times 10^{-3} \\ 3.96 \times 10^{-3} \\ 5.54 \times 10^{-3} \end{array} $	0.18 mole percent CdCl <sub>2</sub> ; concentration of impurity ion determined polaro- graphically using method of standard additions; NaCl from Harshaw Chemical Co., Cleveland, Ohio; c.p. grade of CdCl <sub>2</sub> used; specimen prepared by coating pure crystal of approx 0.02 in by 0.5 in by 0.5 in with thin layer of impurity and heating for several hours at approx 25 K below melting point until impurity evenly distributed; measurements made at l kHz; data points extracted from figure.

TABLE 6.8.	EXPERIMENTAL	DATA	FOR	THE	TANGENT	OF	THE	LOSS	ANGLE	OF	SODIUM	CHLORIDE	(continued)
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Data Set	Author(s), Year [Ref.]	Т	tan d	Remarks
10	Breckenridge, R.G.,	360.3	$6.88 \times 10^{-3}$	
(cont.)	1950 [86]	363.9	$7.51 \times 10^{-3}$	
		366.2	$7.51 \times 10^{-3}$	
		369.0	$9.24 \times 10^{-3}$	
		372.1	$1.066 \times 10^{-2}$	
		374.5	$1.200 \times 10^{-2}$	
		3/0.0 201 0	$1.342 \times 10^{-2}$	
		385 1	$1.378 \times 10^{-2}$	
		385 8	$1.757 \times 10^{-2}$	
		388.2	$2.128 \times 10^{-2}$	
		391.3	$2.302 \times 10^{-2}$	
		394.8	$1.9 \times 10^{-2}$	
		395.2	$2.703 \times 10^{-2}$	
		399.1	$2.7 \times 10^{-2}$	
		403.9	$3.9 \times 10^{-2}$	
		407.0	$4.7 \times 10^{-2}$	
		410.2	$5.9 \times 10^{-2}$	
		416.5	$7.9 \times 10^{-2}$	
		420.8	$1.15 \times 10^{-1}$	
		424.4	$1.46 \times 10^{-1}$	
		423.9	$1.00 \times 10^{-1}$	
		429.5	$2.37 \times 10^{-1}$	
		435.4	$3.07 \times 10^{-1}$	
		439.3	$3.70 \times 10^{-1}$	
		440.9	$4.29 \times 10^{-1}$	
		444.8	5.51 x $10^{-1}$	
		446.7	$5.98 \times 10^{-1}$	
		450.6	$7.00 \times 10^{-1}$	
		452.6	$7.67 \times 10^{+}$	
		454.9	$9.04 \times 10^{-1}$	
		456.8	9.79 x 10	
		458.8	1.053	
		461.9	1.230	
11	Vodop'ianov, K.A. and	(v =	$1 \times 10^{6} \text{ Hz}$ )	Pure; grown by Kyropoulos method from
	[85]	325	$5.9 \times 10^{-5}$	data extracted from figure: data
	[05]	355	$6.1 \times 10^{-5}$	reported for two different specimens
		364	$6.2 \times 10^{-5}$	with data obtained on increasing
		377	$6.2 \times 10^{-5}$	temperature.
		384	4.6 x 10 <sup>-5</sup>	
		397	$5.5 \times 10^{-5}$	
		406	$6.3 \times 10^{-5}$	
		425	$7.2 \times 10^{-5}$	
		435	$5.6 \times 10^{-3}$	
		455	$1.07 \times 10^{-4}$	
		400	$1.25 \times 10^{-4}$	
		402	$1.95 \times 10^{-4}$	
		518	$3.12 \times 10^{-4}$	
		540	$4.64 \times 10^{-4}$	
		547	$4.81 \times 10^{-4}$	
		562	5.75 x 10 <sup>-4</sup>	
		574	$6.34 \times 10^{-4}$	
		5.81	$6.85 \times 10^{-4}$	

Data Set	Author(s), Year [Ref.]	Т	tan ó	Remarks
12	Vodop'ianov, K.A. and Galibina, G.I., 1958 [85]	(v = 464) 476 544	$1 \times 10^{6} \text{ Hz})$ 1.62 x 10 <sup>-4</sup> 2.12 x 10 <sup>-4</sup> 5.19 x 10 <sup>-4</sup>	The above specimens except data taken with decreasing temperature.
13	Matsonashvili, B.N., 1958 [67]	(v = 299) 309 315 327 341 354 357 367 372 379 383 398 410	$1 \times 10^{3} Hz)$ $6.4 \times 10^{-4}$ $7.1 \times 10^{-4}$ $7.5 \times 10^{-4}$ $7.5 \times 10^{-4}$ $7.5 \times 10^{-4}$ $9.3 \times 10^{-4}$ $1.01 \times 10^{-3}$ $1.12 \times 10^{-3}$ $1.12 \times 10^{-3}$ $1.12 \times 10^{-3}$ $1.12 \times 10^{-3}$ $1.25 \times 10^{-3}$ $1.43 \times 10^{-3}$	Single crystal; grown by Kyropoulos technique; slab sawed from crystal by using water-wetted wire saw; ground and polished using dehydrated alcohol to disk shape; plane parallel to within 1-2 µm; transparent and crossed polaroids showed no percep- tible internal stresses; measured in vacuum; data taken on heating; data points extracted from figure.
14	Matsonashvili, B.N., 1958 [67]	(v = 8) 296 306 317 328 334 341 351 368 382 429 443 468 473 481 488 504 512 530 535 540 546 551 558	$3.50 \times 10^{5} Hz)$ $3.5 \times 10^{4}$ $3.6 \times 10^{4}$ $3.5 \times 10^{4}$ $3.5 \times 10^{4}$ $3.5 \times 10^{4}$ $3.5 \times 10^{4}$ $3.7 \times 10^{4}$ $4.0 \times 10^{4}$ $5.4 \times 10^{-4}$ $5.5 \times 10^{-4}$ $6.3 \times 10^{-4}$ $6.3 \times 10^{-4}$ $6.3 \times 10^{-4}$ $6.3 \times 10^{-4}$ $6.5 \times 10^{-4}$ $6.5 \times 10^{-4}$ $7.4 \times 10^{-4}$ $7.6 \times 10^{-4}$ $8.1 \times 10^{-4}$ $8.5 \times 10^{-4}$ $9.0 \times 10^{-4}$	Similar to the above specimen and conditions except different frequency and data taken on heating.
15	Westphal, W.B. and Sils, A., 1972 [12]	(v = 295 347 383 432 478 591	$1 \times 10^{2} \text{ Hz})$ $3 \times 10^{-3}$ $6.7 \times 10^{-2}$ $1.84 \times 10^{-1}$ $3.26 \times 10^{-1}$ $7.61 \times 10^{-1}$ $8.020$	0.075 at.% BeCl3; data points ex- tracted from figure.
16	Westphal, W.B. and Sils, A., 1972 [12]	(v = 298 335 382 426	$1 \times 10^{5} \text{ Hz})$ $4 \times 10^{-4}$ $7 \times 10^{-4}$ $1.6 \times 10^{-3}$ $2.9 \times 10^{-3}$	Similar to the above specimen and conditions.

Data Set	Author(s), Year [Ref.]	Т	tan δ	Remarks
16 (cont.)	Westphal, W.B. and Sils, A., 1972 [12]	492 518 553 586 625	$3.9 \times 10^{-3}  4.4 \times 10^{-3}  1.2 \times 10^{-2}  2.0 \times 10^{-2}  4.9 \times 10^{-2}$	
17	Westphal, W.B. and Sils, A., 1972 [12]	(v = 295 341 380 419 461 500 533	$1 \times 10^{2} \text{ Hz})$ $4.7 \times 10^{-3}$ $5.9 \times 10^{-2}$ $1.76 \times 10^{-1}$ $3.63 \times 10^{-1}$ $5.59 \times 10^{-1}$ $1.030$ $1.730$	1.23 at.% BiCl <sub>3</sub> ; data points ex- tracted from figure.

TABLE 6.8. EXPERIMENTAL DATA FOR THE TANGENT OF THE LOSS ANGLE OF SODIUM CHLORIDE (continued)



FIGURE 6.8. Dielectric strength of sodium chloride (temperature dependence).



FIGURE 6.9. Dielectric strength of sodium chloride (thickness dependence).

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## TABLE 6.10. EXPERIMENTAL DATA FOR THE DIELECTRIC STRENGTH OF SODIUM CHLORIDE

[Temperature, T,K; Thickness, t,µm; Dielectric Strength, MV m<sup>-1</sup>]

Data Set	Author(s), Year [Ref.]	Т	Dielectric Strength	Remarks
1	Nevald, R., 1964 [81]	4 77 133 176 202 229 277 302 345 355	86 92 97 100 107 111 126 139 139 134	NaCl single crystal; from Harshaw Chemical; slabs 5 to 8 mm thick cleaved from crystal blanks of approx 1 cm <sup>2</sup> cross section, an- nealed for several hours at 750 K and slowly cooled; cavity, approx 3 mm in diam and average thickness 90 $\mu$ m, etched into center of one side and chemically polished with ether to a mirrorlike surface free of scratches; after drying and cleaning gold electrodes evaporated in high vacuum on both sides; data extracted from table; 37 samples used: at 4 K spread in breakdown voltage 5 MV m <sup>-1</sup> based on 5 samples, at 77 K 5 MV m <sup>-1</sup> with 6 samples, at 133 K 5 MV m <sup>-1</sup> with 4 samples, at 176 K 6 MV m <sup>-1</sup> with 2 samples, at 202 K 4 MV m <sup>-1</sup> with 3 samples, at 229 K 5 MV m <sup>-1</sup> with 3 samples, at 277 K 4 MV m <sup>-1</sup> with 4 samples, at 302 K 3 MV m <sup>-1</sup> with 3 samples, at 345 K 5 MV m <sup>-1</sup> with 3 samples, and at 355 K 4 MV m <sup>-1</sup> with 4 samples; author reports maximum breakdown strength at 140 MV m <sup>-1</sup> at 337 K; identical data reported in table for specimen annealed no deformation, and counted dislocation density of 2 x 10 <sup>3</sup> cm <sup>-2</sup> .
2	Nevald, R., 1964 [81]	77 185 229 266 298 340 388	97 109 116 124 142 119 94	Similar to the above specimen and conditions except deformed by compression of 2.5% or bent with radius 1 cm, counted dislocation density 1.1 x $10^7$ cm <sup>-2</sup> , at 77 K spread in breakdown voltage 8 MV m <sup>-1</sup> based on 9 sam- ples, at 185 K 5 MV m <sup>-1</sup> with 2 samples, at 229 K 9 MV m <sup>-1</sup> with 3 samples, at 266 K 7 MV m <sup>-1</sup> with 2 samples, at 298 K 7 MV m <sup>-1</sup> with 4 samples, at 340 K 15 MV m <sup>-1</sup> with 6 specimens, and at 388 K 10 MV m <sup>-1</sup> with 5 samples.
3	Nevald, R., 1964 [81]	77 220 298 345	137 129 115 94	Similar to the above specimen and conditions except deformed by compression 10%, counted dislocation density 1.0 x $10^9$ cm <sup>-2</sup> at 77 K spread in breakdown voltage 12 MV m <sup>-1</sup> based on 11 samples, at 220 K 7 MV m <sup>-1</sup> with 7 samples, at 298 K 8 MV m <sup>-1</sup> with 7 samples, and at 345 K 10 MV m <sup>-1</sup> with 4 samples.
4	von Hippel, A. and Lee, G.M., 1941 [90]	100.7 211.8 295.5 328.4 360.0 394.4 420.5	85.0 126.2 164.7 168.8 146.9 96.3 67.6	Pure NaCl (rock salt); data points extracted from figure.
5	von Hippel, A. and Lee, G.M., 1941 [90]	110.2 200.8	119.2 152.2	0.004 at.% AgCl in rock salt; data points extracted from figure.

Data Set	Author(s), Year [Ref.]	Т	Dielectric Strength	Remarks
5 (cont.)	von Hippel, A. and Lee, G.M., 1941 [90]	298.2 351.7 384.8	201.7 167.5 115.5	
6	von Hippel, A. and Lee, G.M., 1941 [90]	117.0 202.1 296.7 353.1 395.8	200.1 233.0 246.9 157.9 67.5	0.017 at.% AgCl in rock salt; data points extracted from figure.
7	von Hippel, A. and Lee, G.M., 1941 [90]	204.7 298.1 346.3 373.8	290.6 272.9 146.9 103.1	0.046 at.% AgCl in rock salt; data points extracted from figure.
8	Caspari, M.E., 1955 [91]	296	146	NaCl single crystal from Harshaw Chemical Co.; crystal plates of <0.25 mm thickness and about 1 cm <sup>2</sup> area cut from same single crystal, ground to proper thickness, and polished on soft silk moistened with NaCl solution; evaporated gold electrodes applied to flat specimens; direction of applied field [100]; data reported is average for 5 specimens; data extracted from table; max 154 MV m <sup>-1</sup> , min 135 MV m <sup>-1</sup> , standard devia- tion 0.064; max deviation about $\pm7.5\%$ , about 2.5% of this may be due to random errors in voltage and thickness determina- tion.
9	Caspari, M.E., 1955 [91]	296	142	Similar to the above specimens and condition except direction of applied field [110], max dielectric strength 151 MV m <sup>-1</sup> , min 138 MV m <sup>-1</sup> , and standard deviation 0.048.
10	Caspari, M.E., 1955 [91]	293	175	Crystal between glass slides; approximate values reported; data extracted from table; measurement temperature specified as room temperature, 293 K assigned.
11	von Hippel, A. and Alger, R.S., 1949 [92]	99 121 138 159 175 191 206 224 239 255 268 280 291 303 311 319 330 334	82 89 96 102 109 116 123 130 137 143 150 156 160 162 164 164 164 164	Pressed-on ball bearing electrodes; dc dielectric strength; data extracted from figure.

TABLE 6.10. EXPERIMENTAL DATA FOR THE DIELECTRIC STRENGTH OF SODIUM CHLORIDE (continued)

Data Set	Author(s), Year [Ref.]	Т	Dielectric Strength	Remarks
11	von Hippel, A. and	340	162	
(cont.)	Alger, R.S., 1949 [92]	344	158	
		352	153	
		362	143	
		372	134	
		382	123	
		390	113	
		396	104	
		402	94	
		410	85	
		418	75	
		422	69	
		428	60	
		432	58	
12	von Hippel, A. and	170	63	Cavity, evaporated metal electrodes; dc
	Alger, R.S., 1949 [92]	183	70	dielectric strength; data extracted from
		203	80	figure.
		222	89	
		238	98	
		255	106	
		265	113	
		273	118	
		284	122	
		292	125	
		300	129	
		304	131	
		311	134	
		321	135	
		331	134	
		341	133	
		356	132	
		370	128	
		384	124	
		396	119	
		411	112	
		429	106	
		455	25	
		467	8/	
		480	01 70	
		500	12	
		5/0	0Z^ 52*	
		550	^CC * / /	
		575	44*	
		505	21*	
		601	24*	
		* Not	shown in figu:	re.
13	von Hippel, A., 1932	293	150	Results of measurements on several natural
	[93]			crystals and a synthetic NaCl specimen; max deviation $\pm 10$ MV m <sup>-1</sup> or $\pm 6.6\%$ ; measure ment temperature not given explicitly, assumed to be 293 K.

Data Set	Author(s), Year [Ref.]	t	Dielectric Strength	Remarks
14	Pikalova, I.S., 1967 [94]	(T= 0.36 0.48 0.54 0.76 1.03 1.21 1.64 2.00 2.42 3.00 3.97	293 K) 10320* 6780* 5470* 3670* 2490* 1860* 1310* 1060* 933* 933* 684	Rock salt; measurement carried out using dc; data extracted from figure; measurement temperature not given explicitly, assumed to be 293 K.
		* Not	shown in fi	gure.
15	Vorob'ev, A.A., Vorob'ev, G.A., and Murashko, L.T., 1963 [95]	(T=2 2.9 5.1 6.9 8.3 10.0 11.7 13.7 16.3 17.4 20.3	93 K) 744 543 464 392 352 319 285 291 268 268 268	Rock salt; electric field in [100] direc- tion; small electrodes used; data extracted from figure; measurement temperature speci- fied as room temperature, 293 K assigned.
16	Vorob'ev, A.A., et al. 1963 [95]	(T=2 5.7 9.7 15.1 20.0	93 K) 386 308 252 241	Similar to the above specimen and conditions except electric field in [111] direction.
17	Vorob'ev, A.A., et al. 1963 [95]	(T=2 10.0 15.1 20.0 35.1 40.3 50.0	93 K) 263 224 213 173 168 151	Similar to the above specimen and conditions except electric field in [110] direction.

work of von Hippel and Alger [92] showed that the electrodes used to measure the dielectric strength have an effect on the numerical values. Data from press-on ball bearings (data set 11) resulted in a value of 160 MV m<sup>-1</sup> at 291 K while cavity, evaporated metal electrodes (data set 12) gave 125 MV m<sup>-1</sup> at 292 K. With a crystal between glass slides, Caspari [91] (data set 10) reported an approximate value of 175 MV m<sup>-1</sup> at 293 K. For results on several natural crystals and a synthetic one, von Hippel [93] (data set 13) reported a value of 150 MV m<sup>-1</sup>.

In contrast to pure material, data for specimens with impurities deliberately added or deformed show other features. In 1941, von Hippel and Lee [90] (data sets 4-7) presented data for the dielectric strength for varying amounts of silver chloride in sodium chloride. For temperatures below room temperature, the dielectric strength increases as the amount of silver chloride increases and the maximum in the dielectric strength shifts to a lower temperature. Above room temperature the slope of the decrease shows a tendency to become more pronounced as the amount of silver chloride increases. Nevald [81] (data sets 1-3) investigated the effect of deformation. A deformation by compression of 10% (data set 3) shows a curve decreasing in value form 77 to 345 K.

Figure 6.9 for the thickness dependence shows the general features of the data. Of particular note is the orientation dependence shown by Vorob'ev et al. [95] (data sets 15–17) demonstrating that the dielectric strength increases as the electric field is in the [100], [111], and [110] directions.

The range of values at room temperature for the dielectric strength given in table 6.9 as the evaluated data is based on the lowest and highest values reported for bulk, pure, and unstrained sodium chloride; evaluated data are not given in addition to room temperature since several effects mentioned above lead to a variation in the dielectric strength and also data on well-characterized materials are lacking.

In addition to the data discussed above, data are contained in references [91,96,97]. A review article in which the author discusses many aspects of dielectric strength in alkali halide crystals is reference [98].

## 6.6. Magnetic Susceptibility

Evaluated data for the temperature dependence of the magnetic mass susceptibility of pure sodium chloride are given in table 6.11 and shown on figure 6.10 together with experimental data. Table 6.12 contains the numerical data, together with information on sample characterization, for the experimental data shown on figure 6.10. A discussion of the data is given before stating the basis of the evaluated data.

The data indicate that at room temperature and below the magnetic susceptibility is constant. In 1914, Ishiwara [99] (curve 1) reported data on a small crystal from Merck over the temperature range 123 to 291 K, with the data showing a constant behavior. The data are negative making sodium chloride a diamagnetic substance. He also reported data on a large crystal of rock salt (curve 2), which are close to the data on the small crystal, and also showed constant behavior. Data on solid material at or near room temperature were reported by Hoare and Brindley [101,102] (curve 4) and by Kido [103] (curve 5) with the data of the latter differing from the data of Ishiwara by no more than 3.5%. Data from measurements on aqueous solutions were given by Ikenmeyer [100] (curve 3). In 1974, Smirnov et al. [104] made the point that the temperature coefficient of the magnetic susceptibility, within the experimental error, was zero for crystals of sodium chloride.

The evaluated data were based on the data of Ishiwara (curve 1) for a solid sample and were arrived at by taking an average of that data. The uncertainty in the data is assigned a value of 3.5% since the data of Kido is within that percentage.

Additional data for the magnetic susceptibility appear in references [105,106, and 126]. A previous compilation of molar magnetic susceptibility values for sodium chloride in aqueous solutions appears in reference [107].

## 6.7. Effect of Nuclear Irradiation on Electrical and Magnetic Properties

### 6.7.1. Effect of Nuclear Irradiation on Electrical Conductivity

Pearlstein [108] studied the effect of proton bombardment on the electrical conductivity of sodium chloride. The material received a 350 MeV fluence of 10<sup>15</sup> protons cm<sup>-2</sup> at room temperature and the conductivity was measured over the range of 398 to 743 K. The conductivity was decreased by the bombardment. Upon heating the material the conductivity anneals in several distinct temperature ranges. At room temperature, the initial conductivity is restored after all the heat treatments; at higher temperatures it is only about 75% restored. Further work on proton bombardment was reported by Pearlstein and Ingham [109] in which sodium chloride was bombarded at 350 MeV and several days later the conductivity was measured as the temperature was increased at a constant rate of 1.25 K min<sup>-1</sup>. Three different proton fluences of  $2.6 \times 10^{14}$ ,  $1 \times$  $10^{15}$ , and  $2.6 \times 10^{15}$  protons cm<sup>-2</sup> were used. The

conductivity decreased to a minimum at 423 K and increased to its pre-bombardment level at just below 623 K.

### 6.7.2. Effect of Nuclear Irradiation on Dielectric Constant and Strength

Ishiguro et al. [110] studied the effect of x-ray irradiation on tan  $\delta$ . If a specimen is either plastically

deformed or quenched, x-rays darken the crystal and the anomalous dispersion peak at 393 K disappears. When the specimen undergoes either heating or illumination, the peak reappears.

Mineav et al. [111] exposed single-crystal sodium chloride whiskers to x-rays and found the dielectric strength decreased with an increase in the concentration of F-centers that were produced by the irradiation.

TABLE 6.11. EVALUATED DATA FOR THE MAGNETIC MASS SUSCEPTIBILITY OF PURE SODIUM CHLORIDE

[Temperature, T, K; Magnetic Mass Susceptibility,  $\chi_{\rm M,mass},~10^{-9}~{\rm m}^3~{\rm kg}^{-1}]$ 

Т	X <sub>M,mass</sub>
1.25	-6.28
150	-6.28
200	-6.28
250	-6.28
291	-6.28



FIGURE 6.10. Magnetic mass susceptibility of sodium chloride.

Data Set	Author(s), Year [Ref.]	T	X <sub>M,mass</sub>	Remarks
1	Ishiwara, T., 1914 [99]	123.2 143.4 165.6 183.8 210.2 229.0 244.2 269.2 291.4	-6.30 -6.26 -6.30 -6.22 -6.28 -6.31 -6.27 -6.35 -6.27	From Merck; small crystal, data extracted from table.
2	Ishiwara, T., 1914 [99]	122.2 142.2 165.0 188.8 207.6 227.8 248.8 263.8 271.2 292.4	-6.32 -6.31 -6.37 -6.31 -6.32 -6.32 -6.30 -6.31 -6.27 -6.26	Rock salt; large crystal; data extracted from table.
3	Ihenmeyer, K., 1929 [100]	293	-6.438	From measurements on aqueous solutions; mea- surement temperature assumed to be 293 K; data extracted from table.
4	Hoare, F.E. and Brindley, G.W., 1934 [101,102]	293	-6.49	Material supplied by British Drug Houses, Ltd., of grade A.R. standard; measurement con- ducted on crystalline material; number of samples used was 4; Gouy method used; temper- ature specified as room temperature, 293 K assigned; data of molecular diamagnetic sus- ceptibility ( $30.2 \pm 0.14 \times 10^{-6}$ ) extracted from table; average deviation from mean of molecular diamagnetic susceptibility $\pm 0.14 \times 10^{-6}$ ; molecular weight of NaCl 58.44277 from 1971 atomic weights of the elements.
5	Kido, K., 1932 [103]	282	-6.36	Solid material; data extracted from table.

TABLE 6.12. EXPERIMENTAL DATA FOR THE MAGNETIC MASS SUSCEPTIBILITY OF SODIUM CHLORIDE [Temperature, T,K; Magnetic Mass Susceptibility, X<sub>M.mass</sub>, 10<sup>-9</sup> m<sup>3</sup> kg<sup>-1</sup>]

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### Symbols and Units

Name

Symbol

tanδ

T

e

ν

о

ρ

0 intrinsic

 $\chi_{\rm M, mass}$ 

Symbols and Units		Conversion Factors			
Name	Unit	Temperature			
Tangent of the loss angle	dimensionless	To convert from	to	Use	
Temperature	К	K	°C	K – 273.15	
Real part of the dielectric constant	nt dimensionless	K	°F	(K - 273.15)9/5+32	
Frequency	Hz	<b>Electrical</b> Conductiv	vity		
Electrical conductivity	S m <sup>-1</sup> S m <sup>-1</sup>	To convert from	to	Multiply by	
Magnetic mass susceptibility	m3 kg-1	S m <sup>-1</sup>	$\Omega^{-1}$ cm <sup>-1</sup>	10-2	
Flootrical resistivity		S m <sup>-1</sup>	$\Omega^{-1}$ in <sup>-1</sup>	$2.54 \times 10^{-2}$	
Lieutical resistivity	22 111	S m <sup>-1</sup>	$\Omega^{-1}$ ft <sup>-1</sup>	$3.048 \times 10^{-1}$	
		S m <sup>-1</sup>	$\Omega^{-1}$ cmil <sup>-1</sup> ft	$1.66243 \times 10^{-9}$	
		S m <sup>-1</sup>	$(\mu \Omega \text{ cm})^{-1}$	$1 \times 10^{-8}$	

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BIBLIOGRAPHIC DATA SHEET	NBS MN 167				
4. TITLE AND SUBTITLE			5. Publication Da	ate	
Physical Propertie	es Data for Rock Salt		January 6. Performing Org	1981 ganization Code	
7. AUTHOR(S)			8. Performing Org	gan. Report No.	
L. H. Gevantman, J	Editor				
9. PERFORMING ORGANIZATIO	ON NAME AND ADDRESS		10. Project/Task/	Work Unit No.	
NATIONAL BUREAU OF DEPARTMENT OF COMM WASHINGTON, DC 20234	STANDARDS ERCE		11. Contract/Gran	it No.	
12. SPONSORING ORGANIZATIO	ON NAME AND COMPLETE ADDRESS (Stre	et, City, State, ZIP)	13. Type of Report	rt & Period Covered	
Same as Item 9 and Office of Nuclear Waste Isolation			N/7	ł	
	505 King Avenue		14. Sponsoring Ag	ency Code	
15. SUPPLEMENTARY NOTES	5-1410-457 01110 45201				
Library of Congres	ss Catalog Card Number: 8	0~607096			
Document describes a con	nputer program; SF-185, FIPS Software Sum	mary, is attached.			
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