The regulations of the Commission and the preliminary annual rate being adopted today are effective for calendar year 2002. Therefore, all gaming operations within the jurisdiction of the Commission are required to self-administer the provisions of these regulations and report and pay any fees that are due to the Commission by March 31, 2002.


David L. Meyer,
Director, Office of Administration, and
Bobby Gordon, National Indian Gaming
Management.

FOR FURTHER INFORMATION CONTACT:
Bobby Gordon, National Indian Gaming
Commission.

SUMMARY: Notice is hereby given, pursuant to 25 CFR 514.1(a)(3), that the National Indian Gaming Commission has adopted preliminarily annual fee rates of 0.00% for tier 1 and 0.075% (.00075) for tier 2 for calendar year 2002. These rates shall apply to all assessable gross revenues from each gaming operation under the jurisdiction of the Commission. If a tribe has a gaming operation under the jurisdiction of the Commission, 1441 L Street, NW., Suite 9100, Washington, DC 20005; telephone 202/632-7003; fax 202/632-7066 (these are not to toll-free numbers).

The requested exemption would allow use of ASME Code Case N–588 to determine stress intensity factors for postulated flaws and postulated flaw orientation for circumferential welds.

10 CFR part 50, Appendix G requires that Article G–2120 of ASME Code, Section XI, Appendix G, be used to determine the maximum postulated defects in reactor pressure vessels (RPV) for the P–T limits. These limits are determined for normal operation and test conditions. Article G–2120 specifies in part, that the postulated defect be perpendicular to the RPV material and normal (i.e., perpendicular) to the direction of maximum stress. ASME Code, Section XI, Appendix G, also provides a methodology for determining the stress intensity factors for a maximum postulated defect normal to the maximum stress. The purpose of this article is, in part, to ensure the prevention of non-ductile fractures by providing procedures to identify the most limiting postulated fractures to be considered in the development of P–T limits. Code Case N–588 provides relief from the Appendix G requirements, in terms of calculating P–T limits, by determining stress intensity factors for a maximum postulated defect perpendicular to the direction of maximum stress.
revising the Article G–2120 reference flaw orientation for circumferential welds in RPVs. The reference flaw is a postulated flaw that accounts for the possibility of a prior existing defect that may have gone undetected during the fabrication process. Thus, the intended application of a reference flaw is to account for defects that could physically exist within the geometry of the weldment. The current ASME Section XI, Appendix G approach mandates the consideration of an axial reference flaw in circumferential welds for purposes of calculating the P–T limits. Postulating the Appendix G reference flaw in a circumferential weld is physically unrealistic and overly conservative, because the length of the flaw is 1.5 times the RPV wall thickness, which is much longer than the width of circumferential welds. The possibility that an axial flaw may extend from a circumferential weld into a plate or axial weld is already adequately covered by the requirement that defects be postulated in plates/forgings and axial welds. The fabrication of RPVs for nuclear power plant operation involved precise welding procedures and controls designed to optimize the resulting weld microstructure and to provide the required material properties. These controls were also designed to minimize defects that could be introduced into the weld during the fabrication process. Industry experience with the repair of weld indications found during pre-service inspection, in-service non-destructive examinations, and data taken from destructive examination of actual RPV welds, confirms that any remaining defects are small and do not cross transverse to the weld bead. Therefore, any postulated defects introduced during the fabrication process, and not detected during subsequent non-destructive examinations, would only be expected to be oriented in the direction of weld fabrication. For circumferential welds this indicates a postulated defect with a circumferential orientation. ASME Code Case N–588 addresses this issue by allowing consideration of maximum postulated defects oriented circumferentially in circumferential welds. ASME Code Case N–588 also provides appropriate procedures for determining the stress intensity factors for use in developing RPV P–T limits per ASME Code, Section XI, Appendix G procedures. The procedures allowed by ASME Code Case N–588 are conservative and provide a margin of safety in the development of RPV P–T operating and pressure test limits that will prevent non-ductile fracture of the RPV.

The proposed P–T limits include restrictions on allowable operating conditions and equipment operability requirements to ensure that operating conditions are consistent with the assumptions of the accident analysis. Specifically, reactor coolant system pressure and temperature must be maintained within the heatup and cooldown rate dependent P–T limits specified in TS Section 3.1.B, “Heatup and Cooldown.”

2.2 Code Case N–640

The requested exemption would allow use of ASME Code Case N–640 in conjunction with ASME Code Section XI, Appendix G to determine the P–T limits for the RPV. Code Case N–640 permits the use of an alternate reference fracture toughness (Kc, fracture toughness curve instead of Kr, fracture toughness curve) for reactor vessel materials in determining the P–T limits. Because use of the Kr fracture toughness curve results in the calculation of less conservative P–T limits than the methodology currently required by 10 CFR part 50, Appendix G, an exemption to apply the Code Case would be required by 10 CFR 50.60. The licensee proposed to revise the P–T limits for IP2, using the Kr fracture toughness curve, in lieu of the Kc fracture toughness curve, as the lower bound for fracture toughness.

Use of the Kr curve in determining the lower bound fracture toughness in the development of P–T operating limit curves is more technically correct than the Kc curve because the rate of loading during a heatup or cooldown is slow and is more representative of a static condition than a dynamic condition. The Kr curve appropriately implements the use of static initiation fracture toughness behavior to evaluate the controlled heatup and cooldown process of a reactor vessel. The staff has required use of the initial conservatism of the Kr curve since 1974 when the curve was codified. This initial conservatism was necessary due to the limited knowledge of RPV materials. Since 1974, additional knowledge has been gained about RPV materials, which demonstrates that the lower bound on fracture toughness provided by the Kr curve is well beyond the margin of safety required to protect the public health and safety from potential RPV failure. Additionally, P–T curves based on the Kc curve will enhance overall plant safety by opening the operating window, with the greatest safety benefit in the region of low-temperature operations.

In summary, the ASME Section XI, Appendix G, procedure was conservatively developed based on the level of knowledge existing in 1974 concerning RPV materials and the estimated effects of operation. Since 1974, the level of knowledge about these topics has been greatly expanded.

3.0 Discussion

Pursuant to 10 CFR 50.12, the Commission may, upon application by any interested person or upon its own initiative, grant exemptions from the requirements of 10 CFR part 50, when (1) the exemptions are authorized by law, will not present an undue risk to public health or safety, and are consistent with the common defense and security; and (2) when special circumstances are present. Special circumstances are present whenever, according to 10 CFR 50.12(a)(2)(i), “Application of the regulation in the particular circumstances would not serve the underlying purpose of the rule or is not necessary to achieve the underlying purpose of the rule.”

Code Case N–588

The first of these exemption requests would allow ENO to apply ASME Code Case N–588 as the basis for determining the most limiting material in the IP2 RPV. Code Case N–588 is applicable only for reactor vessels that have a circumferential weld as the most limiting material in the beltline region of the RPV. The Code Case methods allow licensees to apply the lower tensile stresses associated with a circumferential crack postulated in the circumferential weld, and thus allow the licensee to use the next most limiting base metal or axial weld material in the RPV as the basis for evaluating the vessel. Since the IP2 RPV is currently limited by circumferential shell weld for the 1/4T location, this Code Case is applicable to the evaluation of the IP2 RPV.

The staff has determined that Entergy has provided sufficient technical bases for using the methods of Code Case N–588 for the calculation of the P–T limits for the IP2 reactor coolant pressure boundary (RCPB). The staff has also determined that application of Code Case N–588 to the P–T limit calculations will continue to serve the purpose in 10 CFR part 50, Appendix G, for protecting the structural integrity of the IP2 RPV and RCPB. In this case, since strict compliance with the requirements of 10 CFR part 50, Appendix G, is not necessary to serve the underlying purpose of the regulation, the staff concludes that application of Code Case...
N–588 to the P–T limit calculations meets the special circumstance provisions stated in 10 CFR 50.12(a)(2)(iii), for granting this exemption to the regulation.

**Code Case N–640**

Entergy has requested, pursuant to 10 CFR 50.60(b), an exemption to use ASME Code Case N–640 as the basis for establishing the P–T limit curves. Appendix G to 10 CFR part 50 has required use of the initial conservatism of the $K_t$ equation since 1974 when the equation was codified. This initial conservatism was necessary due to the limited knowledge of RPV materials. Since 1974, the industry has gained additional knowledge about RPV materials, which demonstrates that the lower bound on fracture toughness provided by the $K_t$ equation is well beyond the margin of safety required to protect the public health and safety from potential RPV failure. In addition, the RPV P–T operating window is defined by the P–T operating and test limit curves developed in accordance with the ASME Code, Section XI, Appendix G, procedure.

The ASME Working Group on Operating Plant Criteria (WGOPC) has concluded that application of Code Case N–640 to plant P–T limits is still sufficient to ensure the structural integrity of RPVs during plant operations. The staff has concurred with ASME’s determination. The staff has concluded that application of Code Case N–640 would not significantly reduce the safety margins required by 10 CFR part 50, Appendix G. The staff also concluded that relaxation of the requirements of Appendix G to the Code by application of Code Case N–640 is acceptable and would maintain, pursuant to 10 CFR 50.12(a)(2)(iii), the underlying purpose of the NRC regulations to ensure an acceptable margin of safety for the IP2 RPV and RCPB. Therefore, the staff concludes that Code Case N–640 is acceptable for application to the IP2 P–T limits.

The staff examined the licensee’s rationale to support the exemption requests and concluded that ENO has provided sufficient technical bases for using the methods of Code Cases N–588 and N–640 in the calculation of the P–T limits for IP2. The staff has also concluded that application of Code Case N–588 and Code Case N–640 to the P–T limit calculations will continue to serve the purpose in 10 CFR part 50, Appendix G, for protecting the structural integrity of the IP2 RPV and reactor coolant pressure boundary. In this case, since strict compliance with requirements of 10 CFR 50.60(a) and 10 CFR part 50, Appendix G, is not necessary to serve the overall intent of the regulations, the staff concludes that application of the Code Cases N–588 and N–640 to the P–T limit calculations meets the special circumstance provisions in 10 CFR 50.12(a)(2)(iii), for granting exemptions to the regulations, and that, pursuant to 10 CFR 50.12(a)(1), the granting of these exemptions is authorized by law, will not present undue risk to the public health and safety, and is consistent with the common defense and security. The staff, therefore, considers granting exemptions to 10 CFR 50.60(a) and 10 CFR part 50, Appendix G, to allow ENO to use Code Cases N–588 and N–640 as the part of the bases for generating the P–T limit curves for IP2 is appropriate.

**4.0 Conclusion**

Accordingly, the Commission has determined that, pursuant to 10 CFR 50.12(a), the exemption is authorized by law, will not present an undue risk to the public health and safety, and is consistent with the common defense and security. Also, special circumstances are present. Therefore, the Commission hereby grants ENO an exemption from the requirements of 10 CFR 50.60(a) and 10 CFR part 50, Appendix G, for the calculation of P–T limits for IP2. The licensee shall use the methods Code Cases N–588 and N–640 in calculation of the P–T limits for IP2. Pursuant to 10 CFR 51.32, the Commission has determined that the granting of this exemption will not have a significant effect on the quality of the human environment (67 FR 7206).

This exemption is effective upon issuance.

Dated at Rockville, Maryland, this 15th day of February 2002.

For the Nuclear Regulatory Commission.

John A. Zwolinski,
Director, Division of Licensing Project Management, Office of Nuclear Reactor Regulation.

[FR Doc. 02–4242 Filed 2–21–02; 8:45 am]

BILLING CODE 7590–01–P

**OFFICE OF PERSONNEL MANAGEMENT**

**Federal Prevailing Rate Advisory Committee; Open Committee Meetings**

According to the provisions of section 10 of the Federal Advisory Committee Act (Pub. L. 92–463) and 5 U.S.C. 552(c)(9)(B). These caucuses may, depending on the issues involved, constitute a substantial portion of a meeting.

Annually, the Chair compiles a report of pay issues discussed and concluded recommendations. These reports are available to the public, upon written request to the Committee’s Secretary.

The public is invited to submit material in writing to the Chair on Federal Wage System pay matters felt to be deserving of the Committee’s attention. Additional information on this meeting may be obtained by contacting the Committee’s Secretary, Office of Personnel Management, Federal Prevailing Rate Advisory Committee, Room 5338, 1900 E Street, NW., Washington, DC 20415 (202) 606–1500.

**Thursday, March 14, 2002**

**Thursday, March 28, 2002**

**Thursday, April 11, 2002**

**Thursday, April 25, 2002**

**Thursday, May 9, 2002**

**Thursday, May 23, 2002**

**Thursday, June 6, 2002**

**Thursday, June 27, 2002**

The meeting will start at 10:00 a.m. and will be held in Room 5H09, Office of Personnel Management Building, 1900 E Street, NW., Washington, DC.

The Federal Prevailing Rate Advisory Committee is composed of a Chair, five representatives from labor unions holding exclusive bargaining rights for Federal blue-collar employees, and five representatives from Federal agencies.

Entitlement to membership on the Committee is provided for in 5 U.S.C. 5347.

The Committee’s primary responsibility is to review the Prevailing Rate System and other matters pertinent to establishing prevailing rates under subchapter IV, chapter 53, 5 U.S.C., as amended, and from time to time advise the Office of Personnel Management.

This scheduled meeting will start in open session with both labor and management representatives attending. During the meeting either the labor members or the management members may caucus separately with the Chair to devise strategy and formulate positions. Premature disclosure of the matters discussed in these caucuses would unacceptably impair the ability of the Committee to reach a consensus on the matters being considered and would disrupt substantially the disposition of its business. Therefore, these caucuses will be closed to the public because of a determination made by the Director of the Office of Personnel Management under the provisions of section 10(d) of the Federal Advisory Committee Act (Pub. L. 92–463) and 5 U.S.C. 552(c)(9)(B). These caucuses may, depending on the issues involved, constitute a substantial portion of a meeting.

The Federal Prevailing Rate Advisory Committee has the responsibility to review the Prevailing Rate System and other matters pertinent to establishing prevailing rates under subchapter IV, chapter 53, 5 U.S.C., as amended, and from time to time advise the Office of Personnel Management.

According to the provisions of section 10 of the Federal Advisory Committee Act (Pub. L. 92–463), notice is hereby given that meetings of the Federal Prevailing Rate Advisory Committee will be held on—

**Thursday, February 28, 2002**