approval of the Administrator, provided test cell calibration records show the pertinent instrument information.

(i) Recorder Charts: Identify zero, span, exhaust gas, and dilution air sample traces.

(j) Test cell barometric pressure, ambient temperature and humidity.

NOTE: A central laboratory barometer may be used; Provided, that individual test cell barometric pressures are shown to be within ±0.1 percent of the barometric pressure at the central barometer location.

(k) [Reserved]

(l) Pressure of the mixture of exhaust and dilution air entering the CVS metering device, the pressure increase across the device, and the temperature at the inlet. The temperature may be recorded continuously or digitally to determine temperature variations.

(m) The number of revolutions of the positive displacement pump accumulated during each test phase while exhaust samples are being collected. The number of standard cubic meters metered by a critical flow venturi during each test phase would be the equivalent record for a CFV-CVS.

(n) The humidity of the dilution air. NOTE: If conditioning columns are not used (see §§ 86.522 and 86.544) this measurement can be deleted. If the conditioning columns are used and the dilution air is taken from the test cell, the ambient humidity can be used for this measurement.

(o) The driving distance for each of the three phases of test, calculated from the measured roll or shaft revolutions.

(p) Additional required records for methanol-fueled vehicles:

1. Specification of the methanol fuel, or fuel mixtures, used during testing.
2. Volume of sample passed through the methanol sampling system and the volume of deionized water in each impinger.
3. The methanol calibration information from the GC standards.
4. The concentration of the GC analyses of the test samples (methanol).
5. Volume of sample passed through the formaldehyde sampling system.
6. The formaldehyde calibration information from the HPLC standards.

(q) Additional required records for natural gas-fueled vehicles. Composition, including all carbon containing compounds; e.g., CO₂, of the natural gas-fuel used during the test. C₁ and C₂ compounds shall be individually reported. C₃ and heavier hydrocarbons and C₄ and heavier compounds may be reported as a group.

(r) Additional required records for liquefied petroleum gas-fueled vehicles. Composition of the liquefied petroleum gas-fuel used during the test. Each hydrocarbon compound present, through C₄ compounds, shall be individually reported. C₅ and heavier hydrocarbons may be reported as a group.

54 FR 14553, Apr. 11, 1989, as amended at 59 FR 48515, Sept. 21, 1994; 60 FR 34357, June 30, 1995

§ 86.544–90 Calculations; exhaust emissions.

The final reported test results, with oxides of nitrogen being optional for model years prior to 2006 and required for 2006 and later model years, shall be computed by use of the following formula: (The results of all emission tests shall be rounded, in accordance with ASTM E29–93a (incorporated by reference in §86.1), to the number of places to the right of the decimal point indicated by expressing the applicable standard to three significant figures.)

\[
Y_{wm} = 0.43 \left( \frac{Y_{ct}}{D_{ct} + D_s} \right) + 0.57 \left( \frac{Y_{ht}}{D_{ht} + D_s} \right)
\]

Where:
1. \( Y_{wm} \) = Weighted mass emissions of CO₂ or of each pollutant (i.e., HC, CO, or NOₓ) in grams per vehicle kilometer.
2. \( Y_{ct} \) = Mass emissions as calculated from the “transient” phase of the cold-start test, in grams per test phase.
3. \( Y_{ht} \) = Mass emissions as calculated from the “transient” phase of the hot-start test, in grams per test phase.
4. \( Y_s \) = Mass emissions as calculated from the “stabilized” phase of the cold-start test, in grams per test phase.
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(5) \(D_s\) = The measured driving distance from the “transient” phase of the cold-start test, in kilometers.

(6) \(D_h\) = The measured driving distance from the “transient” phase of the hot-start test, in kilometers.

(7) \(D_c\) = The measured driving distance from the “stabilized” phase of the cold-start test, in kilometers.

(b) The mass of each pollutant for each phase of both the cold-start test and the hot-start test is determined from the following:

(1) Hydrocarbon mass:
\[
\text{HC}_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{\text{HC}} \times (\text{HC}_{\text{conc}}/1,000,000)
\]

(2) Oxides of nitrogen mass:
\[
\text{NOX}_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{\text{NOx}} \times K_{\text{H}} \times (\text{NOX}_{\text{conc}}/1,000,000)
\]

(3) Carbon monoxide mass:
\[
\text{CO}_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{\text{CO}} \times (\text{CO}_{\text{conc}}/1,000,000)
\]

(4) Carbon dioxide mass:
\[
\text{CO}_{2\text{mass}} = V_{\text{mix}} \times \text{Density}_{\text{CO2}} \times (\text{CO}_{2\text{conc}}/100)
\]

(5) Methanol mass:
\[
\text{CH}_3\text{OH}_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{\text{CH}3\text{OH}} \times (\text{CH}_3\text{OH}_{\text{conc}}/1,000,000)
\]

(6) Formaldehyde mass:
\[
\text{HCHO}_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{\text{HCHO}} \times (\text{HCHO}_{\text{conc}}/1,000,000)
\]

(7) Total hydrocarbon equivalent:
\[
\text{THCE} = \text{HC}_{\text{mass}} + 13.8756/30.0262 \times (\text{CH}_3\text{OH}_{\text{mass}} + 13.8756/32.042 \times (\text{HCHO}_{\text{mass}})
\]

(8) Nitrous Oxide Mass:
\[
V_{\text{mix}} \times \text{Density}_{\text{N2O}} \times (\text{N2O}_{\text{conc}}/1,000,000)
\]

(c) Meaning of symbols:

(1) \(\text{HC}_{\text{mass}}\) = Hydrocarbon emissions, in grams per test phase.

(ii) \(\text{Density}_{\text{HC}}\) = Density of HC in exhaust gas.

(A) For gasoline-fuel: \(\text{Density}_{\text{HC}} = 576.8\) g/m³-carbon atom (16.33 g/ft³-carbon atom), assuming an average carbon to hydrogen ratio of 1:1.85, at 20 °C (68 °F) and 101.3 kPa (760 mm Hg) pressure.

(B) For natural gas and liquefied petroleum gas-fuel: \(\text{Density}_{\text{HC}} = 41.57/(12.011 + H/C(1.008))\) g/m³-carbon atom (1.177/(12.011 + H/C(1.008)) g/ft³-carbon atom) where H/C is the hydrogen to carbon ratio of the hydrocarbon components of test fuel, at 20 °C (68 °F) and 101.3 kPa (760 mm Hg) pressure.

\(\text{NOX}_{\text{conc}}\) = Oxides of nitrogen concentration of the dilute exhaust sample corrected for background, in ppm carbon equivalent, i.e., equivalent propane.

(B) \(\text{HC}_{\text{conc}} = \text{HC}_e - \text{HC}_d(1 - (1/DF))\)

Where:

(iv) \(\text{HC}_e\) = Hydrocarbon concentrations of the dilute exhaust sample as measured, in ppm carbon equivalent (propane ppm=3).

(B) \(\text{HC}_d = \text{FIDHC}_e - (r)\text{CH3OH}\)

(v) FID HC = Concentration of hydrocarbon (plus methanol if methanol-fueled motorcycle is tested) in dilute exhaust as measured by the FID ppm carbon equivalent.

(vi) \(r = \text{FID response to methanol}\).

(vii) \(\text{CH3OH}\) = Concentration of methanol in dilute exhaust as determined from the dilute exhaust methanol sample, ppm carbon.

(viii) \(\text{HC}_d = \text{HC}_{\text{conc}}\) = Oxidation of the dilution air as measured, ppm carbon equivalent.

(x) \(\text{CH3OH}\) = Concentration of methanol in dilute exhaust as determined from dilute exhaust methanol sample, ppm carbon.

(2)(i) \(\text{NOX}_{\text{mass}}\) = Oxides of nitrogen emissions, grams per test phase.

(ii) \(\text{Density}_{\text{NOx2}}\) = Density of oxides of nitrogen in the exhaust gas, assuming they are in the form of nitrogen dioxide, 1913 g/m³ (54.16 g/ft³), at 20 °C (68 °F) and 101.3 kPa (760 mm Hg) pressure.

(3)(i) \(\text{NOX}_{\text{conc}}\) = Oxides of nitrogen concentration of the dilute exhaust sample corrected for background, ppm.

(B) \(\text{NOX}_{\text{conc}} = \text{NOX}_e - \text{NOX}_d(1 - (1/DF))\)

Where:

(iv) \(\text{NOX}_e\) = Oxides of nitrogen concentration of the dilute exhaust sample as measured, ppm.

(v) \(\text{NOX}_d\) = Oxides of nitrogen concentration of the dilution air as measured, ppm.
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(68 °F) and 101.3 kPa (760 mm Hg) pressure.

(iii)(A) CO$_{\text{conc}}$ = Carbon monoxide concentration of the dilute exhaust sample corrected for background, water vapor, and CO$_2$ extraction, ppm.

(B) CO$_{\text{conc}}$ = CO$_e$ - CO$_d$(1 - (1/DF))

Where:

(iv)(A) CO$_e$ = Carbon monoxide concentration of the dilute exhaust sample volume corrected for water vapor and carbon dioxide extraction, in ppm.

(B) CO$_e$ = (1 + 0.0006CO$_{\text{2em}}$ - 0.000323R)CO$_{\text{em}}$ for gasoline-fueled vehicles with hydrogen to carbon ratio of 1.85:1.

(C) CO$_e$ = [1 - (0.01+0.005HCR) CO$_{\text{2em}}$ - 0.000323R]CO$_{\text{em}}$ for methanol-fueled, natural gas-fueled or liquefied petroleum gas-fueled motorcycles, where HCR is hydrogen to carbon ratio as measured for the fuel used.

(v) CO$_{\text{em}}$ = Carbon monoxide concentration of the dilute exhaust sample as measured, ppm.

(vi) CO$_{\text{dm}}$ = Carbon dioxide concentration of the dilute exhaust sample as measured, ppm.

(vii) R = Relative humidity of the dilution air, pct (see § 86.542(n)).

(viii)(A) CO$_d$ = Carbon monoxide concentration of the dilution air corrected for water vapor extraction, ppm.

(B) CO$_d$ = (1 - 0.000323R)CO$_{\text{dm}}$

Where:

(ix) CO$_{\text{dm}}$ = Carbon monoxide concentration of the dilution air sample as measured, ppm.

$$C_{\text{CH3OH}_e} = \frac{3.813 \times 10^{-2} \times T_{EM}}{P_r \times V_{EM}} \left[ (C_{S1} \times AV_{S1}) + (C_{S2} \times AV_{S2}) \right]$$

(v) (A) $C_{\text{CH3OH}_e}$ = Methanol concentration in the dilution air, ppm.

$$C_{\text{CH3OH}_d} = \frac{3.813 \times 10^{-2} \times T_{DM}}{P_r \times V_{DM}} \left[ (C_{D1} \times AV_{D1}) + (C_{D2} \times AV_{D2}) \right]$$

(vi) $T_{DM}$ = Temperature of methanol sample withdrawn from dilute exhaust, °R.

(vii) $T_{DM}$ = Temperature of methanol sample withdrawn from dilution air, °R.
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(viii) \( P_B \) = Barometric pressure during test, mm Hg.

(ix) \( V_{DM} \) = Volume of methanol sample withdrawn from dilute exhaust, \( \text{ft}^3 \).

(x) \( V_{DM} \) = Volume of methanol sample withdrawn from dilution air, \( \text{ft}^3 \).

(xi) \( C_{p} \) = GC concentration of sample drawn from dilute exhaust, \( \mu \text{g/ml} \).

(xii) \( C_{D} \) = GC concentration of sample drawn from dilution air, \( \mu \text{g/ml} \).

(xiii) \( AV_s \) = Volume of absorbing reagent (deionized water) in impinger through which methanol sample from dilute exhaust is drawn, \( \text{ml} \).

(xiv) \( AV_D \) = Volume of absorbing reagent (deionized water) in impinger through which methanol sample from dilution air is drawn, \( \text{ml} \).

(xv) \( HCHO_{mass} \) = Formaldehyde emissions corrected for background, grams per test phase.

(xvi) \( 1 \) = first impinger.

(xvii) \( 2 \) = second impinger.

(6)(i) \( HCHO_{em} \) = Formaldehyde emissions corrected for background, grams per test phase.

(6)(ii) \( Density_{HCHO} \) = Density of formaldehyde is 1249 g/m\(^3\) (35.36 g/ft\(^3\)), at 20 °C (68 °F) and 101.3 kPa (760 mm Hg) pressure.

(6)(iii)(A) \( HCHO_{conc} \) = Formaldehyde concentration of the dilute exhaust corrected for background, ppm.

(B) \( HCHO_{conc} = C_{HCHOe} - C_{HCHOD} (1 - (1/DF)) \)

Where:

(iv)(A) \( C_{HCHOe} \) = Formaldehyde concentration in dilute exhaust, ppm.

(B)

\[
C_{HCHOe} = \frac{4.069 \times 10^{-2} \times C_{FDE} \times V_{AE} \times Q \times T_{EF}}{V_{SE} \times P_B}
\]

(v)(A) \( C_{CHOMD} \) = Formaldehyde concentration in dilution air, ppm.

(B)

\[
C_{CHOMD} = \frac{4.069 \times 10^{-2} \times C_{FDA} \times V_{AA} \times Q \times T_{DF}}{V_{SA} \times P_B}
\]

(vi) \( C_{FDE} \) = Concentration of DNPH derivative of formaldehyde from dilute exhaust sample in sampling solution, \( \mu \text{g/ml} \).

(vii) \( V_{AE} \) = Volume of sampling solution for dilute exhaust formaldehyde sample, ml.

(viii)(A) \( Q \) = Ratio of molecular weights of formaldehyde to its DNPH derivative.

(B) \( Q = 0.1429 \)

(ix) \( T_{EF} \) = Temperature of formaldehyde sample withdrawn from dilute exhaust, °R.

(x) \( V_{SE} \) = Volume of formaldehyde sample withdrawn from dilute exhaust, \( \text{ft}^3 \).

(xi) \( P_B \) = Barometric pressure during test, mm Hg.

(xii) \( C_{FDA} \) = Concentration of DNPH derivative of formaldehyde from dilution air sample in sampling solution, \( \mu \text{g/ml} \).

(xiii) \( V_{AA} \) = Volume of sampling solution for dilution air formaldehyde sample, ml.

(xiv) \( T_{DF} \) = Temperature of formaldehyde sample withdrawn from dilution air, °R.

(xv) \( V_{SA} \) = Volume of formaldehyde sample withdrawn from dilution air, \( \text{ft}^3 \).

(7)(i) \( DF = 13.4[CO_e + (HC_e = CO_e)10^{-4}] \) for gasoline-fueled vehicles.

(ii) For methanol-fueled, natural gas-fueled or liquefied petroleum gas-fueled motorcycles, where fuel composition is \( C, H, O \), as measured, or calculated, for the fuel used (for natural gas and liquefied petroleum gas-fuel, \( Z=0 \)):
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(iii)(A) \( V_{\text{mix}} \) = Total dilute exhaust volume in cubic meters per test phase corrected to standard conditions (293 K (528 °R) and 101.3 kPa (760 mm Hg)).

(B) \[
V_{\text{mix}} = \frac{V_o \times N \times (P_b - P_i) \times 293}{101.3 \times T_p}
\]

Where:

(iv) \( V_o \) = Volume of gas pumped by the positive displacement pump, in cubic meters per revolution. This volume is dependent on the pressure differential across the positive displacement pump. (See calibration techniques in §86.519.)

(v) \( N \) = Number of revolutions of the positive displacement pump during the test phase while samples are being collected.

(vi) \( P_b \) = Barometric pressure, kPa.

(vii) \( P_i \) = Pressure depression below atmospheric measured at the inlet to the positive displacement pump, kPa.

(viii) \( T_p \) = Average temperature of dilute exhaust entering positive displacement pump during test while samples are being collected, °K.

(ix)(A) \( K_h \) = Humidity correction factor.

(B) \( K_h = 1/[1 - 0.0329(H - 10.71)] \]

Where:

(x) \( H \) = Absolute humidity in grams of water per kilogram of dry air.

(B) \( H = [(6.211)R_a \times P_d]/[P_b - (P_d \times R_a/100)] \]

(xi) \( R_a \) = Relative humidity of the ambient air, pct.

(xii) \( P_d \) = Saturated vapor pressure, in kPa at the ambient dry bulb temperature.

(xiii) \( P_b \) = Barometric pressure, kPa.

(ii) \( N_{2O} \) = Nitrous oxide emissions, in grams per test phase.

(ii) Density \( N_{2O} \) = Density of nitrous oxide is 51.81 g/m³ (1.93 kg/m³), at 68 °F (20 °C) and 760 mm Hg (101.3kPa) pressure.

(ii) \( N_{2O} = \frac{\text{Density} \times \text{Volume}}{\text{Pressure}} \)

(iv) \( N_{2O} = \frac{(51.81) \times (12,115) \times 99.05}{(101.325) \times (309.8)} = 78.651 \text{ m}^3/\text{per test phase} \)

(v) \( HC e = 249.75 \text{ ppm carbon equivalent} \)

(vi) \( HC d = 4.90 \text{ ppm} \)

(iii)(A) \( N_{2O_{\text{conc}}} \) = Nitrous oxide concentration of the dilute exhaust sample corrected for background, in ppm.

(B) \( N_{2O_{\text{conc}}} = N_{2O_e} - N_{2O_d}(1 - (1/DF)) \)

Where:

(1) For the “transient” phase of the cold-start test, assume \( V_o = 0.0077934 \text{ m}^3/\text{per rev} ; N = 12,115; R = 20.5 \text{ pct} ; R_a = 20.5 \text{ pct} ; P_b = 99.05 \text{ kPa} ; P_d = 3.382 \text{ kPa} ; P_i = 9.851 \text{ kPa} ; T_p = 309.8 \text{ °K} ; HC e = 249.75 \text{ ppm carbon equivalent} ; NOx e = 30.30 \text{ ppm} ; CO em = 311.23 \text{ ppm} ; CO_2 e = 0.415 \text{ percent} ; HCd = 4.90 \text{ ppm} ; NOx d = 0.30 \text{ ppm} ; CO dm = 8.13 \text{ ppm} ; CO_2 d = 0.037 \text{ pct} ; D_{\text{test}} = 5.650 \text{ km}.

Then:

(i) \( V_{\text{mix}} = \frac{[(0.0077934)\times(12,115)\times(99.05-9.851)\times(293.15)]}{[(101.325)\times(309.8)\times(3.382)\times(20.5/100)]} = 78.651 \text{ m}^3/\text{per test phase} \)

(ii) \( H = [((6.211)\times20.5\times3.382)\times(99.05 - 3.382)\times(20.5/100)] = 4.378 \text{ grams H}_2\text{O per kg dry air} \)

(iii) \( K_h = 1/[1 - 0.0329(H - 10.71)] = 0.8276 \)

(iv) \( CO e = \frac{1 - 0.01925(0.415) - 0.000323(20.5)(311.23)}{1 - 0.000323(20.5)(8.13)} = 8.08 \text{ ppm} \)

(v) \( CO d = \frac{1 - 0.000323(20.5)(8.13)}{1 - 0.000323(20.5)(8.13)} = 0.08 \text{ ppm} \)

(vi) \( DF = 13.4/[0.415 + (249.75 + 306.68)\times(20.5/100)] = 28.472 \)

(vii) \( HC_{\text{conc}} = 249.75 - 4.90(1 - 1/28.472) = 245.02 \text{ ppm} \)

(viii) \( HC_{\text{conc}} = (78.651)(576.8) = 44,782 \text{ grams per test phase} \)

(i) \( NOx_{\text{conc}} = 38.30 - 0.30(1 - 1/28.472) = 38.01 \text{ ppm} \)

(x) \( NOx_{\text{conc}} = (78.651)(1913)(0.8276) \times 10^{-6} = 4.733 \text{ grams per test phase} \)

(xi) \( CO_{\text{conc}} = 306.68 - 8.08 (1 - 1/28.472) = 298.88 \text{ ppm} \)

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(xii) \( \text{CO}_{\text{mass}} = (78.651)(1164)(298.88) \times 10^{-6} = 27.362 \) grams per test phase.
(xiii) \( \text{CO}_{2 \text{conc}} = 0.415 \times 0.037 \times (1/28.472) = 0.3793 \) percent.
(xiv) \( \text{CO}_{2 \text{mass}} = (78.651)(1843)(0.3793)/100 = 549.81 \) grams per test phase.

(2) For the “stabilized” portion of the cold-start test, assume that similar calculations resulted in \( \text{HC}_{\text{mass}} = 7.184 \) grams per test phase; \( \text{NOx}_{\text{mass}} = 2.154 \) grams per test phase; \( \text{CO}_{\text{mass}} = 64.541 \) grams per test phase; and \( \text{CO}_{2\text{mass}} = 529.52 \) grams per test phase. \( D_s = 6.070 \) km.

(3) For the “transient” portion of the hot-start test, assume that similar calculations resulted in \( \text{HC}_{\text{mass}} = 6.122 \) grams per test phase; \( \text{NOx}_{\text{mass}} = 7.056 \) grams per test phase; \( \text{CO}_{\text{mass}} = 34.964 \) grams per test phase; and \( \text{CO}_{2\text{mass}} = 480.93 \) grams per test phase. \( D_h = 5.660 \) km.

(4) For a 1978 motorcycle with an engine displacement equal to or greater than 170 cc (10.4 cu. in):
(i) \( \text{HC}_{\text{wm}} = 0.43 \times [(11.114 + 7.184)/(5.650 + 6.070)] + 0.57 \times [(6.122 + 7.184)/(5.660 + 6.070)] = 1.318 \) grams per vehicle kilometer.
(ii) \( \text{NOx}_{\text{wm}} = 0.43 \times [(4.733 + 2.154)/(5.650 + 6.070)] = 0.700 \) gram per vehicle kilometer.
(iii) \( \text{CO}_{\text{wm}} = 0.43 \times [(27.362 + 64.541)/(5.650 + 6.070)] + 0.57 \times [(34.964 + 64.541)/(5.660 + 6.070)] = 8.207 \) grams per vehicle kilometer.
(iv) \( \text{CO}_{2\text{wm}} = 0.43 \times [(549.81 + 529.52)/(5.650 + 6.070)] + 0.57 \times [(480.93 + 529.52)/(5.660 + 6.070)] = 88.701 \) grams per vehicle kilometer.


§§ 86.545–86.599 [Reserved]

Subpart G—Selective Enforcement Auditing of New Light-Duty Vehicles, Light-Duty Trucks, and Heavy-Duty Vehicles

SOURCE: 41 FR 31483, July 28, 1976, unless otherwise noted.

§§ 86.601–86.601–83 [Reserved]

§ 86.601–84 Applicability.

The provisions of this subpart apply to light-duty vehicles, light-duty trucks, and heavy-duty vehicles. However, manufacturers that optionally certify heavy-duty vehicles based on chassis testing under §86.1863–07 may choose instead to perform selective enforcement audits using the procedures specified in 40 CFR part 1068, subpart E. References to “light-duty vehicle” or “LDT” in this subpart G shall be deemed to include light-duty trucks and heavy-duty vehicles as appropriate.

(a) Section numbering; construction. (1) The model year of initial applicability is indicated by the two digits following the hyphen of the section number. A section remains in effect for subsequent model years until it is superseded.

(2) A section reference without a model year suffix shall be interpreted to be a reference to the section applicable to the appropriate model year.

(b) References in this subpart to engine families and emission control systems shall be deemed to refer to durability groups and test groups as applicable for manufacturers certifying new light-duty vehicles and light-duty trucks under the provisions of subpart S of this part.

(Secs. 206, 208(a) and 301(a), Clean Air Act, as amended, 42 U.S.C. 7525, 7542(a) and 7601(a))


§ 86.602–84 Definitions.

(a) The definitions in this section apply to this subpart.

(b) As used in this subpart, all terms not defined herein have the meaning given them in the Act.

(1) Acceptable Quality Level (AQL) means the maximum percentage of failing vehicles that, for purposes of sampling inspection, can be considered satisfactory as a process average.

(2) Axle Ratio means all ratios within ±5% of the axle ratio specified in the configuration in the test order.