Environmental Protection Agency

§ 86.544–90 Approval of the Administrator, provided test cell calibration records show the pertinent instrument information.

(i) Recorder Charts: Identify zero, span, exhaust gas, and dilution air sample traces.

(j) Test cell barometric pressure, ambient temperature and humidity.

NOTE: A central laboratory barometer may be used; Provided, that individual test cell barometric pressures are shown to be within ±0.1 percent of the barometric pressure at the central barometer location.

(k) [Reserved]

(l) Pressure of the mixture of exhaust and dilution air entering the CVS metering device, the pressure increase across the device, and the temperature at the inlet. The temperature may be recorded continuously or digitally to determine temperature variations.

(m) The number of revolutions of the positive displacement pump accumulated during each test phase while exhaust samples are being collected. The number of standard cubic meters metered by a critical flow venturi during each test phase would be the equivalent record for a CFV-CVS.

(n) The number of revolutions of the positive displacement pump accumulated during each test phase while exhaust samples are being collected. The number of standard cubic meters metered by a critical flow venturi during each test phase would be the equivalent record for a CFV-CVS.

(o) The driving distance for each of the three phases of test, calculated from the measured roll or shaft revolutions.

(p) Additional required records for methanol-fueled vehicles:

(1) Specification of the methanol fuel, or fuel mixtures, used during testing.

(2) Volume of sample passed through the methanol sampling system and the volume of deionized water in each impinger.

(3) The methanol calibration information from the GC standards.

(4) The concentration of the GC analyses of the test samples (methanol).

(5) Volume of sample passed through the formaldehyde sampling system.

(6) The formaldehyde calibration information from the HPLC standards.

(7) The concentration of the HPLC analysis of the test sample (formaldehyde).

(q) Additional required records for natural gas-fueled vehicles. Composition, including all carbon containing compounds; e.g., CO₂, of the natural gas-fuel used during the test. C₁ and C₂ compounds shall be individually reported. C₃ and heavier hydrocarbons and C₄ and heavier compounds may be reported as a group.

(r) Additional required records for liquefied petroleum gas-fueled vehicles. Composition of the liquefied petroleum gas-fuel used during the test. Each hydrocarbon compound present, through C₄ compounds, shall be individually reported. C₅ and heavier hydrocarbons may be reported as a group.

[54 FR 14553, Apr. 11, 1989, as amended at 59 FR 48515, Sept. 21, 1994; 60 FR 34357, June 30, 1995]

§ 86.544–90 Calculations; exhaust emissions.

The final reported test results, with oxides of nitrogen being optional for model years prior to 2006 and required for 2006 and later model years, shall be computed by use of the following formula: (The results of all emission tests shall be rounded, in accordance with ASTM E29–93a (incorporated by reference in §86.1), to the number of places to the right of the decimal point indicated by expressing the applicable standard to three significant figures.)

\[ Y_{wm} = 0.43 \left( \frac{Y_{ct} + Y_{ht}}{D_{ct} + D_{ht}} \right) + 0.57 \left( \frac{Y_{st} + Y_{ht}}{D_{st} + D_{ht}} \right) \]

Where:

(a) \( Y_{wm} \) = Weighted mass emissions of CO₂ or each pollutant (i.e., HC, CO, or NOₓ) in grams per vehicle kilometer and if appropriate, the weighted carbon mass equivalent of total hydrocarbon equivalent, in grams per vehicle kilometer.

(b) \( Y_{ct} \) = Mass emissions as calculated from the “transient” phase of the cold-start test, in grams per test phase.

(c) \( Y_{ht} \) = Mass emissions as calculated from the “transient” phase of the hot-start test, in grams per test phase.

(d) \( Y_{st} \) = Mass emissions as calculated from the “stabilized” phase of the cold-start test, in grams per test phase.
(5) \( D_{c} \) = The measured driving distance from the "transient" phase of the cold-start test, in kilometers.

(6) \( D_{h} \) = The measured driving distance from the "transient" phase of the hot-start test, in kilometers.

(7) \( D_{p} \) = The measured driving distance from the "stabilized" phase of the hot-start test, in kilometers.

(b) The mass of each pollutant for each phase of both the cold-start test and the hot-start test is determined from the following:

(1) Hydrocarbon mass:
\[
HC_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{HC} \times (HC_{\text{conc}}/1,000,000)
\]

(2) Oxides of nitrogen mass:
\[
NOx_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{NOx} \times K_{\text{pH}} \times (NOx_{\text{conc}}/1,000,000)
\]

(3) Carbon monoxide mass:
\[
CO_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{CO} \times (CO_{\text{conc}}/1,000,000)
\]

(4) Carbon dioxide mass:
\[
CO_{2\text{mass}} = V_{\text{mix}} \times \text{Density}_{CO2} \times (CO_{2\text{conc}}/100)
\]

(5) Methanol mass:
\[
CH_{3}OH_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{CH_{3}OH} \times (CH_{3}OH_{\text{conc}}/1,000,000)
\]

(6) Formaldehyde mass:
\[
HCHO_{\text{mass}} = V_{\text{mix}} \times \text{Density}_{HCHO} \times (HCHO_{\text{conc}}/1,000,000)
\]

(7) Total hydrocarbon equivalent:
\[
\text{Total HC equiv} = HC_{\text{mass}} + 13.8756 \times (CH_{3}OH_{\text{mass}} + 13.8756 \times (CH_{3}OH_{\text{conc}}/1,000,000)
\]

(8) Nitrous Oxide Mass:
\[
V_{\text{mix}} \times \text{Density}_{N_{2}O} \times (N_{2}O_{\text{conc}}/1,000,000)
\]

(c) Meaning of symbols:

(i) \( HC_{\text{conc}} \) = Hydrocarbon concentration, in ppm.

(ii) \( HC_{\text{mix}} \) = Hydrocarbon emissions, in grams per test phase.

(iii) \( HC_{\text{conc}} \) = Hydrocarbon concentration of the dilute exhaust sample corrected for background, in ppm carbon equivalent, i.e., equivalent propane.

(iii)(A) \( HC_{\text{conc}} \) = Hydrocarbon concentration of the dilute exhaust sample corrected for background, in ppm carbon equivalent, i.e., equivalent propane.

(B) \( HC_{\text{conc}} = HC_{e} - HC_{d}(1 - (1/DF)) \)
Where:

(iv)(A) \( HC_{e} \) = Hydrocarbon concentrations of the dilute exhaust sample as measured, in ppm carbon equivalent (propane ppm=3).

(B) \( HC_{d} = FIDHC_{e} - (r)CCH_{3}OH_{d} \)

(v) \( FIDHC_{e} \) = Concentration of hydrocarbon (plus methanol if methanol-fueled motorcycle is tested) in dilute exhaust as measured by the FID ppm carbon equivalent.

(vi) \( r = \) FID response to methanol.

(vii) \( CCH_{3}OH_{d} = \) Concentration of methanol in dilute exhaust as determined from the dilute exhaust methanol sample, ppm carbon.

(viii)(A) \( HC_{d} \) = Hydrocarbon concentration of the dilution air as measured, ppm carbon equivalent.

(B) \( HC_{d} = FIDHC_{e} - (r)CCH_{3}OH_{d} \)

(ix) \( FIDHC_{e} = \) Concentration of hydrocarbon (plus methanol if methanol-fueled motorcycle is tested) in dilution air as measured by the FID, ppm carbon equivalent.

(x) \( CCH_{3}OH_{d} = \) Concentration of methanol in dilution air as determined from dilution air methanol sample, ppm carbon.

(2)(i) \( NOx_{\text{mass}} \) = Oxides of nitrogen emissions, grams per test phase.

(ii) \( NOx_{\text{conc}} \) = Oxides of nitrogen concentration of the dilute exhaust sample corrected for background, ppm.

(B) \( NOx_{\text{conc}} = NOx_{e} - NOx_{d}(1 - (1/DF)) \)
Where:

(iv) \( NOx_{e} \) = Oxides of nitrogen concentration of the dilute exhaust sample as measured, ppm.

(v) \( NOx_{d} \) = Oxides of nitrogen concentration of the dilution air as measured, ppm.

(3)(i) \( CO_{\text{mass}} \) = Carbon monoxide emissions, in grams per test phase.

(ii) \( CO_{\text{conc}} \) = Density of carbon monoxide, 1164 g/m³ (32.97 g/ft³), at 20 °C
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(68 °F) and 101.3 kPa (760 mm Hg) pressure.

(iii)(A) \( \text{CO}_{\text{conc}} = \text{Carbon monoxide concentration of the dilute exhaust sample corrected for background, water vapor, and CO}_2 \) extraction, ppm.  
(B) \( \text{CO}_{\text{conc}} = \text{CO}_x - \text{CO}_x(1 - (1/DF)) \)

Where:

(iv)(A) \( \text{CO}_x = \text{Carbon monoxide concentration of the dilute exhaust sample volume corrected for water vapor and carbon dioxide extraction, in ppm.} \)

(B) \( \text{CO}_x = (1 - 0.01925\text{CO}_2 - 0.000323R)\text{CO}_{\text{em}} \) for gasoline-fueled vehicles with hydrogen to carbon ratio of 1.85:1

(C) \( \text{CO}_x = (1 - 0.01 + 0.005\text{HCR})\text{CO}_2 - 0.000323R)\text{CO}_{\text{em}} \) for methanol-fueled, natural gas-fueled or liquefied petroleum gas-fueled motorcycles, where HCR is hydrogen to carbon ratio as measured for the fuel used.

(v) \( \text{CO}_{\text{em}} = \text{Carbon monoxide concentration of the dilute exhaust sample as measured, ppm.} \)

(vi) \( \text{CO}_d = \text{Carbon dioxide concentration of the dilution air corrected for water vapor extraction, ppm.} \)

(B) \( \text{CO}_d = (1 - 0.000323R)\text{CO}_{\text{dm}} \)

Where:

(ix) \( \text{CO}_{\text{dm}} = \text{Carbon monoxide concentration of the dilution air sample as measured, ppm.} \)

Note: If a CO instrument which meets the criteria specified in §86.511 is used and the conditioning column has been deleted, \( \text{CO}_{\text{em}} \) can be substituted directly for \( \text{CO}_{\text{conc}} \) and \( \text{CO}_{\text{dm}} \) must be substituted directly for \( \text{CO}_d \).

(4)(i) \( \text{CO}_2\text{mass} = \text{Carbon dioxide emissions, grams per test phase.} \)

(ii) \( \text{Density}_\text{CO}_2 = \text{Density of carbon dioxide,} \ 1830 \text{ g/m}^3 (51.81 \text{ g/ft}^3), \ \text{at} \ 20 \^{\circ}C (68 \^{\circ}F) \) and 101.3 kPa (760 mm Hg) pressure.

(iii)(A) \( \text{CO}_2\text{conc} = \text{Carbon dioxide concentration of the dilute exhaust sample corrected for background, in percent.} \)

(B) \( \text{CO}_2\text{conc} = \text{CO}_2 - \text{CO}_2(1 - (1/DF)) \)

Where:

(iv)(A) \( \text{CO}_2 = \text{Carbon dioxide concentration of the dilution air as measured, in percent.} \)

(v) \( \text{CH}_3\text{OH}\text{mass} = \text{Methanol emissions corrected for background, grams per test phase.} \)

(ii) \( \text{Density}_\text{CH}_3\text{OH} = \text{Density of methanol is} \ 1332 \text{ g/m}^3 (37.71 \text{ g/ft}^3), \ \text{at} \ 20 \^{\circ}C (68 \^{\circ}F) \) and 101.3 kPa (760 mm Hg) pressure.

(iii)(A) \( \text{CH}_3\text{OHconc} = \text{Methanol concentration of the dilute exhaust sample corrected for background, ppm.} \)

(B) \( \text{CH}_3\text{OHconc} = \text{CH}_3\text{OH} - \text{CH}_3\text{OH}(1 - (1/DF)) \)

Where:

(iv)(A) \( \text{CH}_3\text{OH} = \text{Methanol concentration in the dilution air, ppm.} \)

(B) \( \text{CH}_3\text{OH} = \text{CH}_3\text{OH} - \text{CH}_3\text{OH}(1 - (1/DF)) \)

Where:

(v) \( \text{T}_\text{EM} = \text{Temperature of methanol sample withdrawn from dilute exhaust, °R.} \)

(vi) \( \text{T}_\text{DM} = \text{Temperature of methanol sample withdrawn from dilution air, °R.} \)

\[
\text{C}_{\text{CH}_3\text{OH}(\text{EM})} = \frac{3.813 \times 10^{-2} \times T_{\text{EM}} \left[ (C_{\text{SI}} \times AV_{\text{SI}}) + (C_{\text{S2}} \times AV_{\text{S2}}) \right]}{P_H \times V_{\text{EM}}}
\]

(vii) \( \text{T}_\text{DM} = \text{Temperature of methanol sample withdrawn from dilution air, °R.} \)

\[
\text{C}_{\text{CH}_3\text{OH}(\text{DM})} = \frac{3.813 \times 10^{-2} \times T_{\text{DM}} \left[ (C_{\text{DI}} \times AV_{\text{DI}}) + (C_{\text{D2}} \times AV_{\text{D2}}) \right]}{P_H \times V_{\text{DM}}}
\]
(viii) \( P_B \) = Barometric pressure during test, mm Hg.
(ix) \( V_{EM} \) = Volume of methanol sample withdrawn from dilute exhaust, ft\(^3\).
(x) \( V_{DM} \) = Volume of methanol sample withdrawn from dilution air, ft\(^3\).
(xi) \( C_p \) = GC concentration of sample drawn from dilute exhaust, \( \mu g/ml \).
(xii) \( C_D \) = GC concentration of sample drawn from dilution air, \( \mu g/ml \).
(xiii) \( AV_s \) = Volume of absorbing reagent (deionized water) in impinger through which methanol sample from dilute exhaust is drawn, ml.
(xiv) \( AV_d \) = Volume of absorbing reagent (deionized water) in impinger through which methanol sample from dilution air is drawn, ml.
(xv) \( HCHO_{mass} \) = Formaldehyde emissions corrected for background, grams per test phase.
(xvi) \( HCHO_{conc} \) = Formaldehyde concentration of the dilute exhaust corrected for background, ppm.

\[
C_{HCHOe} = \frac{4.069 \times 10^{-2} \times C_{FDE} \times V_{AE} \times Q \times T_{EF}}{V_{SE} \times P_B}
\]

(vii)(A) \( C_{HCHOe} \) = Formaldehyde concentration in dilute exhaust, ppm.
(B) \( Q = \frac{C_{FDE}}{C_{FDE} + C_{FDE} \times 10^{4}} \) for gasoline-fueled vehicles.

\[
C_{HCHOM} = \frac{4.069 \times 10^{-2} \times C_{FDA} \times V_{AA} \times Q \times T_{DF}}{V_{SA} \times P_B}
\]

(vi) \( C_{FDE} \) = Concentration of DNPH derivative of formaldehyde from dilute exhaust sample in sampling solution, \( \mu g/ml \).
(vii) \( V_{AE} \) = Volume of sampling solution for dilute exhaust formaldehyde sample, ml.
(viii)(A) \( Q = \frac{C_{FDE}}{C_{FDE} + C_{FDE} \times 10^{4}} \) for gasoline-fueled vehicles.
(ix) \( T_{EF} \) = Temperature of formaldehyde sample withdrawn from dilute exhaust, °R.
(x) \( V_{SE} \) = Volume of formaldehyde sample withdrawn from dilute exhaust, ft\(^3\).
(xi) \( P_B \) = Barometric pressure during test, mm Hg.
(xii) \( C_{FDA} \) = Concentration of DNPH derivative of formaldehyde from dilu-
tion air sample in sampling solution, \( \mu g/ml \).
(xiii) \( V_{AA} \) = Volume of sampling solution for dilution air formaldehyde sample, ml.
(xiv) \( T_{DF} \) = Temperature of formaldehyde sample withdrawn from dilution air, °R.
(xv) \( P_B \) = Barometric pressure during test, mm Hg.
are being collected, 

ment pump during test while samples 

temperature entering positive displace-

in kPa at the ambient dry bulb tem-

ment pump during the 

cative across the positive displace-

ume is dependent on the pressure dif-

this volume, in cubic meters per revolution. This volume 

is dependent on the barometric pressure, kPa.

atmospheric measured at the inlet to 

the positive displacement pump, kPa. 

verage temperature of the positive 

dilute exhaust entering positive displace-

ment pump during test while samples are being 

clected.

positive displacement 

the test phase while samples are being 

ized by the positive displacement pump, in 

cubic meters per revolution. This volume 

is dependent on the pressure differential across the positive displacement pump. (See calibration tech-

iques in §86.519.)

Number of revolutions of the 

positive displacement pump during the 

test phase while samples are being 

clected.

barometric pressure, kPa.

 Pressure depression below 

atmospheric measured at the inlet to 

the positive displacement pump, kPa.

ave temperature of dilute exhaust 

entering positive displacement 

ment pump during test while samples are being 

clected, °K.

humidity correction factor.

Where:

(iii) \( V_{\text{mix}} = \frac{x}{\text{DF}} \) \( = \frac{(100(x+y/2+3.76)(x+y/2-z/2))}{\text{CO}_2 + (\text{HC} + \text{CO} + \text{CH}_3\text{OH} = \text{HCHO} e) \times 10^{-4}} \)

(iii) \( \text{NO}_x = \text{Nitrous oxide concentration of the dilute exhaust sample corrected for background, in ppm.} \)

(iii) \( \text{NO}_x = \text{Nitrous oxide concentration of the dilute exhaust as measured, in ppm.} \)

Sample calculation of mass emission rates for gasoline-fueled vehicles 

with engine displacements equal to or greater than 170 cc (10.4 cu. in.).

(1) For the “transient” phase of the cold-start test, assume \( V_o = 0.077934 \) m³ per rev; \( R = 12.115; R_c = 20.5 \) pct; \( \text{bar} = 99.05 \) kPa; \( P_b = 9.851 \) kPa; \( T_c = 309.8 \) °K; \( \text{HC}_{\text{conc}} = 249.75 \) ppm carbon equivalent; \( \text{NO}_{x} = 38.30 \) ppm; \( \text{CO}_{\text{em}} = 311.23 \) ppm; \( \text{CO}_{\text{ed}} = 0.415 \) percent; \( \text{H}_{\text{tot}} = 4.90 \) ppm; \( \text{NO}_{\text{ed}} = 0.30 \) ppm; \( \text{CO}_{\text{em}} = 8.13 \) ppm; \( \text{CO}_{\text{ed}} = 0.037 \) pct; \( D_{ct} = 5.650 \) km.

Then:

(i) \( V_{o} = \frac{(0.077934)(0.12.115)(99.05-9.851)}{(298.88)(309.8)} = 78.651 \) m³ per test phase.

(ii) \( H = \frac{(0.077934)(0.12.115)(20.5)}{(99.05-3.382)} = 4.378 \) ppm.

(x) \( \text{NO}_{\text{em}} = 38.30 - 0.30(1 - 0.128472) = 38.01 \) ppm.

(x) \( \text{NO}_{\text{em}} = 78.651(1913)(38.01)(0.8276) \times 10^{-6} = 4.733 \) grams per test phase.

(x) \( \text{CO}_{\text{em}} = 306.68 - 8.08(1 - 0.128472) = 298.88 \) ppm.
(xii) CO\textsubscript{mass} = (78.651) (1164) (298.88) \times 10^{-6} = 27.362 grams per test phase.

(xiii) CO\textsubscript{2conc} = 0.415 \times 0.037 (1 - 1/28.472) = 0.3793 percent.

(xiv) CO\textsubscript{2mass} = (78.651)(1843)(0.3793)/100 = 549.81 grams per test phase.

(2) For the “stabilized” portion of the cold-start test, assume that similar calculations resulted in HC\textsubscript{mass} = 7.184 grams per test phase; NOx\textsubscript{mass} = 2.154 grams per test phase; CO\textsubscript{mass} = 64.541 grams per test phase; and CO\textsubscript{2mass} = 529.52 grams per test phase. D\textsubscript{s} = 6.070 km.

(3) For the “transient” portion of the hot-start test, assume that similar calculations resulted in HC\textsubscript{mass} = 6.122 grams per test phase; NOx\textsubscript{mass} = 7.056 grams per test phase; CO\textsubscript{mass} = 34.964 grams per test phase; and CO\textsubscript{2mass} = 480.93 grams per test phase. D\textsubscript{ht} = 5.660 km.

(4) For a 1978 motorcycle with an engine displacement equal to or greater than 170 cc (10.4 cu. in):

(i) HC\textsubscript{wm} = 0.43 [(11.114 + 7.184)/(5.650 + 6.070)] + 0.57 [(6.122 + 7.184)/(5.660 + 6.070)] = 1.318 grams per vehicle kilometer.

(ii) NOx\textsubscript{wm} = 0.43 [(4.733 = 2.154)/(5.650 = 6.070)] + 0.57 [(7.056 = 2.154)/(5.660 = 6.070)] = 0.700 gram per vehicle kilometer.

(iii) CO\textsubscript{wm} = 0.43 [(27.362 + 64.541)/(5.650 + 6.070)] + 0.57 [(34.964 + 64.541)/(5.660 + 6.070)] = 8.207 grams per vehicle kilometer.

(iv) CO\textsubscript{2wm} = 0.43 [(549.81 + 529.52)/(5.650 + 6.070)] + 0.57 [(480.93 + 529.52)/(5.660 + 6.070)] = 88.701 grams per vehicle kilometer.